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## Catalytic reactions of oxalic acid degradation with Pt/SiO<sub>2</sub> as a catalyst in nitric acid solutions

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Large quantities of solutions containing oxalic acid and nitric acid are produced from nuclear fuel reprocessing, but oxalic acid must be removed before nitric acid and plutonium ions can be recovered in these solutions. The degradation of oxalic acid with Pt/SiO<sub>2</sub> as a catalyst in nitric acid solutions has the characteristics of a fast and stable reaction, recyclable catalyst, and no introduction of impurity ions into the system. This method is one of the preferred alternatives to the currently used reaction of KMnO<sub>4</sub> with oxalic acid but lacks theoretical support. Therefore, this study attempts to clarify the reaction mechanism of the method. First, there was no induction period for this catalytic reaction, and no evidence was found that the nitrous acid produced in the solution could have an effect on oxalic acid degradation. Furthermore, oxidation intermediates (structures of Pt–O) were formed through this reaction between NO<sub>3</sub><sup>–</sup> adsorbed on the active sites and Pt on the catalyst surface, but H<sup>+</sup> greatly promoted the reaction. Additionally, oxalic acid degradation through the oxidative dehydrogenation reaction occurred between oxalic acid molecules (HOOC–COOH) and Pt–O, with ·OOC–COOH, which is easily self-decomposable especially in acidic solution, generated simultaneously, and finally CO<sub>2</sub> was produced.

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### 1 Introduction

In nuclear fuel reprocessing plants, oxalic acid is commonly used as a precipitant or complexing agent to separate actinide ions from other elements through the formation of undissolved actinide oxalic acids in aqueous solution.<sup>1–7</sup> For example, plutonium is recycled through plutonium oxalic acid precipitation from solution during a uranium–plutonium co-decontamination separation process that dates back to the 1940s.<sup>3</sup> However, after the precipitation step, small amounts of plutonium oxalic acid solids remain in the radioactive filtrate, and small amounts of plutonium must be extracted from the filtrate. Untreated filtrates containing an excessive addition of oxalic acid are not favorable for purification and recovery of trace amounts of plutonium. Therefore, oxalic acid must be removed from filtrates as much as possible to reach the limiting oxalic acid concentration (10<sup>–4</sup> to 10<sup>–5</sup> M).<sup>6,7</sup> At present, this method for oxalic acid in filtrates oxidized by KMnO<sub>4</sub> is normally used in nuclear fuel reprocessing plants. This method has the advantages of simple operation and short reaction time, but it results in continuous accumulation of K<sup>+</sup> and Mn<sup>2+</sup> compared to alternative methods,<sup>6–9</sup> and it does not

comply with the principle of nuclear waste minimization. Therefore, alternative methods to replace this method are needed.

Various methods of oxalic acid destruction, such as the addition of oxidizing agents,<sup>10,11</sup> electrolytic oxidation<sup>12,13</sup> and using a catalyst in nitrate solution,<sup>6–8,14–20</sup> have been developed to replace the method for oxalic acid oxidized by KMnO<sub>4</sub>. H<sub>2</sub>O<sub>2</sub> is the most popular reagent for the addition of oxidizing agents in this approach and has the advantage of not importing additional impurity ions into the reaction system, but its drawback is that oxalic acid degradation to limiting oxalic acid concentration is excessively prolonged due to the low reaction rate. Also, in the electrolysis process, the required equipment is complex and can lead to precipitation of metal ions during lengthy operation times. Oxalic acid degradation using catalysts in nitric acid solutions is a research hotspot, and depends on catalysts being soluble in water, and these are classified into heterogeneous and homogeneous catalysts. In homogeneous catalysis, metal ions, such as vanadium ions<sup>14</sup> and manganese ions,<sup>6–8</sup> are used as catalysts or combined with ozone and ultraviolet irradiation, with manganese ions being the most mature and widely studied.

Oxalic acid degradation in nitric acid solution using manganese(II) as a catalyst is straightforward, but this method has an induction period and still requires the import of trace amounts of manganese salts in each treatment. In addition, oxalic acid degradation to limiting oxalic acid concentration by this method is lengthy, and the prolonged reaction process at elevated temperatures causes severe erosion damage to the alloy reactor. In

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heterogeneous catalysis, using supported platinum as a catalyst is common,<sup>15–20</sup> and this method shows the characteristics of rapid and stable oxalic acid degradation without an induction period. Moreover, the catalyst is recyclable without introducing impurity ions. As a result, this method is one of the preferred alternatives to the method currently used for oxalic acid oxidation by  $\text{KMnO}_4$ . Pt/SiO<sub>2</sub> is commonly used as a catalyst for nitrate degradation in solution,<sup>15–21</sup> and the oxalic acid degradation with Pt/SiO<sub>2</sub> as a catalyst only is carried out by a simple exploratory process.<sup>19,20</sup> The catalytic processes and mechanisms of oxalic acid degradation are still poorly understood. Thus, the present study focused on the effects of  $\text{H}^+/\text{NO}_3^-$  and nitrous acid on oxalic acid degradation, in order to provide insight into the interaction of the catalyst with the reactants. The aim of this work was to provide theoretical and technical support for the design of techniques to optimize the conditions for oxalic acid degradation in the spent fuel processing process.

## 2 Experimental

### 2.1 Pretreatment of the catalyst

Pt catalyst supported on SiO<sub>2</sub> (particle size, 16–18 mesh; 1% loaded) was obtained from the Dalian Institute of Chemical Physics.<sup>22</sup> Pt/SiO<sub>2</sub> was pretreated as follows before the test run. First, Pt/SiO<sub>2</sub> was immersed in 3 M nitric acid solution for 10 min in a linear shaking bath. In addition, the Pt/SiO<sub>2</sub> was immersed in ethanol for 2 h in a linear shaking bath. Finally, the Pt/SiO<sub>2</sub> was washed three times with pure water before drying at 90 °C for 24 h.

### 2.2 Experimental procedure for measuring the rate of oxalic acid degradation

A 250 ml three-neck flask equipped with a magnetic stirring rod, thermocouple, and condenser was placed in an oil bath for the experiments to measure the rate of oxalic acid degradation in nitrate solution with Pt/SiO<sub>2</sub> as a catalyst. In order to perform the experiment under different conditions, solutions with different concentrations of nitric/sulfuric and oxalic acids were prepared. In addition, the solution was added to a three-neck flask in an oil bath to keep the temperature stable, while the rotational velocity of the stirring head was set at 250 rpm and the temperature was controlled with a thermocouple in all cases. Finally, a certain amount of Pt/SiO<sub>2</sub> was added to the solution under agitation after the temperature was kept constant for 3 min. Next, 200  $\mu\text{l}$  samples were taken from the solution at fixed time intervals, and the samples were stored at 2–8 °C before analysis. The oxalic acid concentration was determined by measuring the difference in absorbance of Mn(III) in solution before and after oxalic acid addition,<sup>23</sup> and the Griess Reagent System was used to determine the levels of nitrous acid.

### 2.3 Raman spectroscopy

An ATR8300 Raman spectrometer (Xiamen Optosky Photonics INC, China) was used for the Raman spectroscopy experiments, with an automated confocal microscope system, laser power of

about 30 mW, laser excitation wavelength of 532 nm, and telephoto lens with a 20 $\times$  objective for laser focusing on the SERS substrate surface. The spectral resolution was 1.5  $\text{cm}^{-1}$  and the integration time of the spectrum was about 3 s. The peak values of the spectra were averaged over the three integrations after subtracting the dark spectra, and then a baseline calibration was performed.

### 2.4 Electron paramagnetic resonance spectroscopy (EPR)

An A300 electron spin resonance spectrometer (Bruker, Germany) was used for the EPR analysis. The spin trap 5,5-dimethyl-1-pyrroline *N*-oxide (DMPO) is commonly used to identify free radicals and active substances through an adduction reaction to generate DMPO adducts, which are relatively stable and easily detected. In all the EPR experiments, dissolved oxygen in solution was removed after the injection of nitrogen gas (99.99%) for 10 min according to the amounts of reagents required *via* the preparation chamber in a nitrogen atmosphere at room temperature as follows. First, a single Pt/SiO<sub>2</sub> was added to 50  $\mu\text{l}$  of the sample solutions of a given solute concentration before stirring for 120 s. Second, 5  $\mu\text{l}$  DMPO was injected in to each sample solution with stirring for about 90 s for the addition reaction of DMPO with the free radicals and active substances. Third, the sample solutions were transferred directly into a capillary tube (50  $\mu\text{l}$ , Brand Co., Ltd., Germany); moreover the capillary tube was three-quarters filled, and then the top and bottom of the capillary tube was sealed with plasticine. Finally, the capillary tube was inserted into the detection chamber in the EPR spectrometer.

The EPR spectrometer was set up as follows: microwave power, 4.4 mW; frequency, 9.84 GHz; central magnetic field, 3505 G; and modulation width, 0.6 G. Computer spectral simulations were performed with the software 'Bruker WinEPR' for DMPO-N ( $\text{N}=\text{OH}$ ,  $\text{OOC}-\text{COOH}$ ) and DMPOX EPR signals.

### 2.5 X-ray photoelectron spectroscopy (XPS)

An Escalab Xi<sup>+</sup> X-ray photoelectron spectrometer (Thermo Fisher Scientific, USA) was used for the X-ray photoelectron spectroscopy (XPS) analysis using an Al X-ray source ( $h\nu = 1486.6$  eV, total energy resolution  $E = 1$  eV). The XPS experiments were performed in an ultrahigh vacuum (UHV) experimental chamber operating at base pressures of  $<8 \times 10^{-10}$  mbar. Computer spectral simulations were performed with software 'Advantage' for the Pt 4f (Pt<sup>0</sup>, Pt(II), Pt(IV)) XPS spectral signals.

## 3 Results and discussion

### 3.1 Is nitrous acid a primary oxidizing substance involved in the catalytic reactions?

In this section, the effect of different concentrations of nitrous acid on oxalic acid degradation during the catalytic reactions is discussed and shown in Fig. 1–4.

In previous studies into formic degradation using supported platinum as a catalyst in nitric acid solutions, some studies have suggested that nitrous acid is an influential reactant

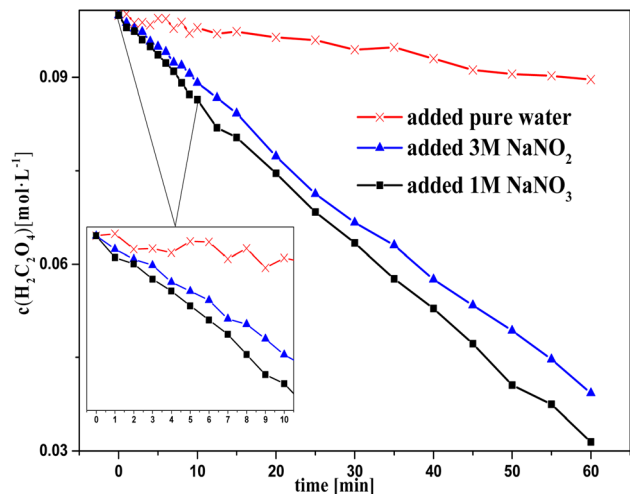


Fig. 1 Oxalic acid concentration in solution versus time with the successive addition of  $\text{NaNO}_2/\text{NaNO}_3$  solution to sulfuric acid solutions at  $T = 90\text{ }^\circ\text{C}$ , where  $c_0(\text{H}_2\text{C}_2\text{O}_4) = 0.1\text{ M}$ ,  $c_0(\text{H}_2\text{SO}_4) = 3\text{ M}$ ,  $S/L$  (solid/liquid ratio) =  $19.5\text{ g L}^{-1}$ , and the speed of adding  $\text{NaNO}_3/\text{NaNO}_2$  solution  $\approx 0.01\text{ ml s}^{-1}$ .

during catalytic reactions.<sup>15,16</sup> However, Bernard believed that the catalytic reactions between  $\text{HNO}_3$  molecules and  $\text{HCO}_2\text{H}$  prevails at the beginning of formic degradation in nitric acid solutions.<sup>17</sup> Miyazaki reported that a large size of  $\text{Pt}/\text{SiO}_2$  (0.6 wt%, 50 nm) does not show any significant catalytic activity for the formation of nitrous acid in solution.<sup>18</sup> These studies indicate that nitrous acid shows an unclear contribution to nitrate degradation in its catalytic process. The oxalic acid degradation proceeds in nitric acid, using supported platinum as a catalyst, similar to that of formic acid. Therefore, in order to obtain the reaction process of oxalic acid degradation with  $\text{Pt}/\text{SiO}_2$  as a catalyst in nitric acid solution, the effect of the nitrous acid concentration on oxalic acid degradation should first be clarified. A series of experiments in different acid media were thus designed.

Fig. 1 and 2 show the change in concentration of oxalic acid and nitrous acid in solution over time during oxalic acid degradation using  $\text{Pt}/\text{SiO}_2$  as a catalyst with the successive addition of  $\text{NaNO}_3/\text{NaNO}_2$  solution into sulfuric acid solution. A decrease in oxalic acid concentration with the addition of  $\text{NaNO}_2/\text{NaNO}_3$  solution was evident compared to the control group, and the decrease in oxalic acid concentration with the addition of  $\text{NaNO}_2$  solution was consistently smaller than that of  $\text{NaNO}_3$  in Fig. 1. The nitrous acid concentration with the addition of  $\text{NaNO}_2$  solution was much greater than that of  $\text{NaNO}_3$  and approached saturation at 4 min, while the nitrous acid concentration with the addition of  $\text{NaNO}_3$  solution reached saturation at 10 min. The higher nitrous acid concentration did not accelerate oxalic acid degradation in this group with the addition of  $\text{NaNO}_2$  compared to  $\text{NaNO}_3$  during the period 4–10 min, indicating that oxalic acid degradation was barely affected by the nitrous acid concentration.

It is important to note in Fig. 1 that the decrease in oxalic acid concentration with the addition of  $\text{NaNO}_2$  solution was

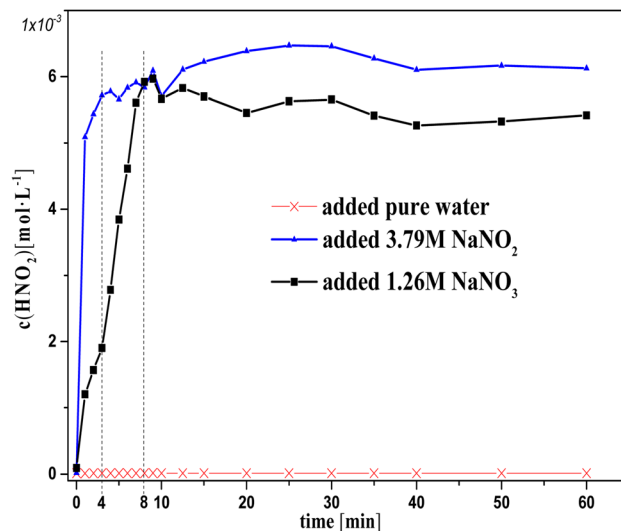


Fig. 2 Nitrous acid concentration in solution versus time with the successive addition of  $\text{NaNO}_2/\text{NaNO}_3$  solution to sulfuric acid solutions at  $T = 90\text{ }^\circ\text{C}$ , where  $c_0(\text{H}_2\text{C}_2\text{O}_4) = 0.1\text{ M}$ ,  $c_0(\text{H}_2\text{SO}_4) = 3\text{ M}$ ,  $S/L = 19.5\text{ g L}^{-1}$ , and the speed of addition of  $\text{NaNO}_3/\text{NaNO}_2$  solution  $\approx 0.01\text{ ml s}^{-1}$ .

consistently smaller than that of  $\text{NaNO}_3$ . In addition, the concentrations  $c(\text{H}^+)$  and  $c(\text{NO}_3^-)$  with the addition of  $\text{NaNO}_2$  solution were always lower than that of  $\text{NaNO}_3$ , resulting from the  $\text{H}^+$  consumed by  $\text{NO}_2^-$  and some  $\text{NO}_2$  gas escaping from solution at the same time, as shown in Fig. 1 ( $2\text{HNO}_2 \rightarrow \text{NO} + \text{NO}_2$ ,  $\text{NO}_2 + \text{HNO}_2 \rightarrow \text{HNO}_3 + \text{NO}$ ). This result suggests  $\text{NO}_3^-/\text{H}^+$  has a positive contribution to oxalic acid degradation to some extent.

Fig. 3 and 4 show the change in oxalic acid concentration and nitrous acid concentration in solution over time during oxalic acid degradation with  $\text{Pt}/\text{SiO}_2$  as a catalyst in the nitrous acid range in the concentration range from 1 M to 5 M. During the first 5 min of oxalic acid degradation, the rate of oxalic acid degradation at different nitric acid concentrations was a stable

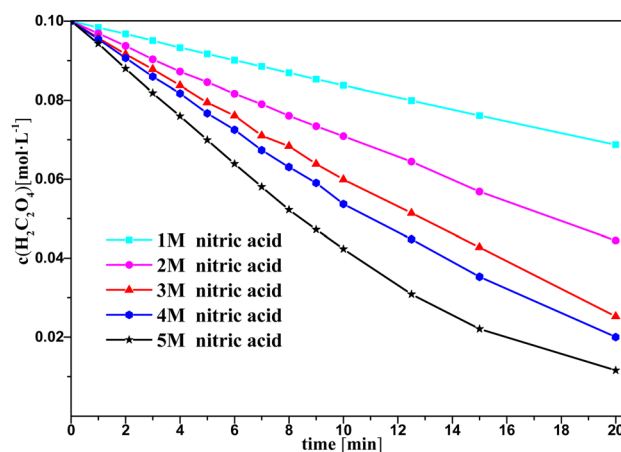


Fig. 3 Oxalic acid concentration in solution versus time at varying nitric acid concentrations at  $T = 90\text{ }^\circ\text{C}$ , where  $c_0(\text{HNO}_3) = 1\text{--}5\text{ M}$ ,  $c_0(\text{H}_2\text{C}_2\text{O}_4) = 0.1\text{ M}$ , and  $S/L = 19.5\text{ g L}^{-1}$ .

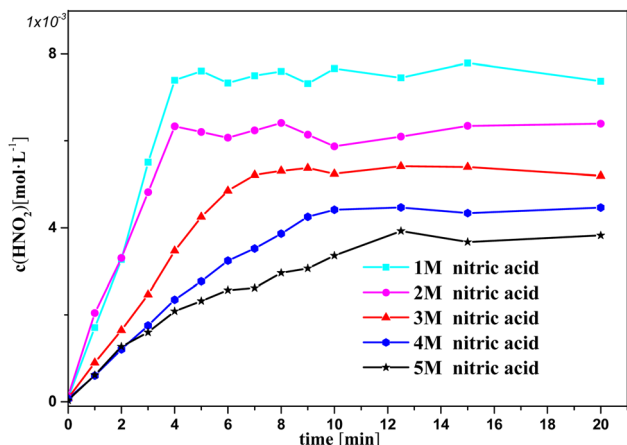


Fig. 4 Nitrous acid concentration versus time at varying nitric acid concentrations at  $T = 90\text{ }^{\circ}\text{C}$ , where  $c_0(\text{HNO}_3) = 1\text{--}5\text{ M}$ ,  $c_0(\text{H}_2\text{C}_2\text{O}_4) = 0.1\text{ M}$ , and  $S/L = 19.5\text{ g L}^{-1}$ .

based on the good fit, namely as the first-order rate constant between the oxalic acid concentration and time reached above 99%, and then increased with increasing the nitric acid concentration, as shown in Fig. 3. However, during the first  $t$  min of oxalic acid degradation in Fig. 4, the nitrous acid concentration at different nitric acid concentrations changed continuously. The saturation value of nitrous acid concentration in Fig. 4 decreased with the nitric acid concentration. These results show the low correlation between the nitrous acid concentration and oxalic acid degradation.

Together, strong evidence proving that nitrous acid was the primary oxidizing substance involved in oxalic acid degradation was not found from Fig. 1–4. Indeed, the results in Fig. 1–4 indicate that the nitrous acid in solution had almost no effect on oxalic acid degradation compared to  $\text{NO}_3^-$  and  $\text{H}^+$ , which could more reasonably be explained by the fact that nitrous acid is considered to be a by-product of the catalytic reactions in this study.

### 3.2 Reaction kinetics

This section briefly describes the effects of varying the concentration of oxalic acid, amount of catalyst and nitric acid on oxalic acid degradation during catalytic reactions, as shown also in Fig. 5–7. The ranges and values of the kinetic parameters in terms of the concentrations of the oxalic acid, catalyst, and nitric acid were obtained. In addition, the initial rate of oxalic acid degradation ( $k_0$ ) was obtained from the mean oxalic acid degradation rate over a period of time when the goodness-of-fit of the mean oxalic acid degradation rate was above 99%.

**3.2.1 Effect of oxalic acid concentration on  $k_0$ .** Fig. 5 shows  $k_0$  in solution with Pt/SiO<sub>2</sub> as a catalyst in the oxalic acid concentration range from 0.02–0.1 M, showing the clear relationship between  $c(\text{H}_2\text{C}_2\text{O}_4)$  and  $k_0$ , which directly indicated that oxalic acid was involved in the catalytic reactions. The goodness-of-fit of  $\ln[k_0]$  and  $\ln[c_0(\text{H}_2\text{C}_2\text{O}_4)]$  was 0.9878 based on the calculation of the experimental data in the oxalic acid range 0.02–0.1 M, and the reaction order for the oxalic acid

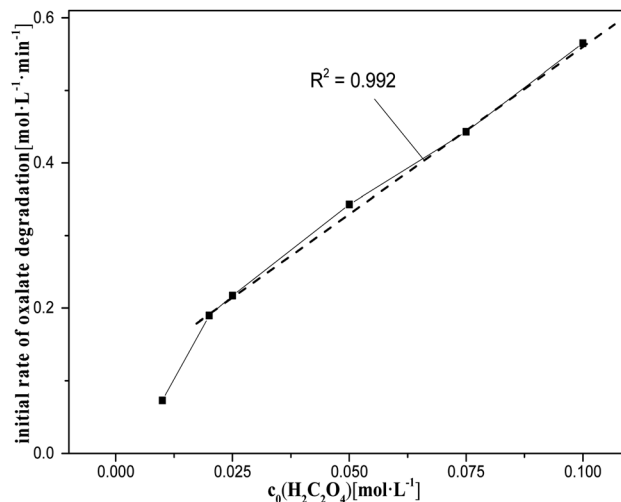


Fig. 5 Initial rate of oxalic acid degradation in solution at varying oxalic acid concentrations at  $T = 90\text{ }^{\circ}\text{C}$ , where  $c_0(\text{HNO}_3) = 5\text{ M}$ ,  $c_0(\text{H}_2\text{C}_2\text{O}_4) = 0.01\text{--}0.1\text{ M}$ ,  $S/L = 19.5\text{ g L}^{-1}$ .

concentration in the catalytic reactions was 0.7325. However,  $k_0$  deviated significantly from the fitted curve at  $c(\text{H}_2\text{C}_2\text{O}_4) = 0.01\text{ M}$ , indicating that oxalic acid degradation could not occur efficiently near  $c(\text{H}_2\text{C}_2\text{O}_4) = 0.01\text{ M}$ . This may be due to the insufficient concentration of oxalic acid with respect to the concentrations of the other reactants and the amount of catalysts.

**3.2.2 Effect of amount of catalysts on  $k_0$ .** Fig. 6 shows  $k_0$  in solution with Pt/SiO<sub>2</sub> as a catalyst in the  $S/L$  range 9.7–39  $\text{g L}^{-1}$ , showing the clear relationship between  $S/L$  and  $k_0$ , which directly indicated that catalyst was involved in the catalytic reactions. The goodness-of-fit of  $\ln[k_0]$  and  $\ln[S/L]$  was 0.9979 based on the calculation of the experimental data in the  $S/L$  range 9.7–39  $\text{g L}^{-1}$ , and the reaction order for the solid/liquid ratio in the catalytic reactions was 0.9115.

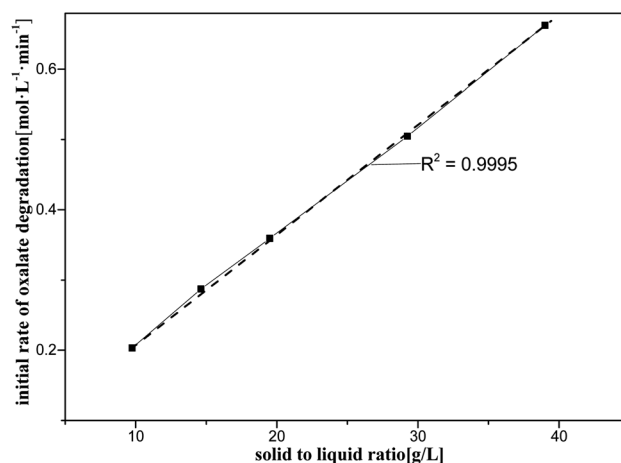


Fig. 6 Initial rate of oxalic acid degradation in solution at varying solid/liquid ratios at  $T = 90\text{ }^{\circ}\text{C}$ , where  $c_0(\text{HNO}_3) = 5\text{ M}$ ,  $c_0(\text{H}_2\text{C}_2\text{O}_4) = 0.1\text{ M}$ , and  $S/L = 9.7\text{--}39\text{ g L}^{-1}$ .

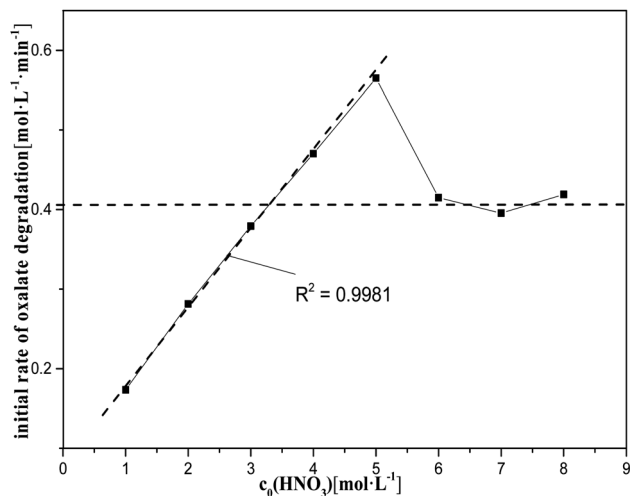


Fig. 7 Initial rate of oxalic acid degradation in solution at varying nitric acid concentrations at  $T = 90\text{ }^{\circ}\text{C}$ , where  $c_0(\text{HNO}_3) = 1\text{--}8\text{ M}$ ,  $c_0(\text{H}_2\text{C}_2\text{O}_4) = 0.1\text{ M}$ , and  $S/L = 19.5\text{ g L}^{-1}$ .

**3.2.3 Effect of nitric acid concentration on  $k_0$ .** Fig. 7 shows  $k_0$  in solution with Pt/SiO<sub>2</sub> as a catalyst in the nitric acid concentration range from 1–8 M, showing the clear relationship between  $c_0(\text{HNO}_3)$  and  $k_0$ , which directly indicated that nitric acid was involved in the catalytic reactions. The goodness of fit of  $\ln[k_0]$  and  $\ln[c_0(\text{HNO}_3)]$  was 0.9951 based on the calculation of the experimental data in the nitric acid range 1–5 M, and the reaction order for the nitric acid concentration in the catalytic reactions was 0.2047.

However, the nitric acid range from 5 M to 8 M did not show a clear relationship between  $c_0(\text{HNO}_3)$  and  $k_0$ , and the degradation rate of oxalic acid decreased rapidly with increasing the nitric acid concentration, tending to reach a steady value. This may be due, on the one hand, to the fact that the diffusion of oxalic acid to the catalysts is more and more significantly hindered by the solute as the reaction progresses, which increases with the concentration of nitric acid in the solution, leading to a decrease in the rate of catalytic reactions. On the other hand, the rate of HNO<sub>3</sub> molecular oxidation of oxalic acid is significantly accelerated with the increase of nitric acid in the solution. This somewhat slows down the impact of the decrease in the rate of oxalic acid degradation caused by the decrease in the rate of catalytic reactions with increasing the nitric acid concentration.

**3.2.4 Effect of the reaction temperature on  $k_0$ .** Fig. 8 shows  $k_0$  in solution with Pt/SiO<sub>2</sub> as a catalyst in the temperature range 30–100 °C. There is a clear linear relationship between  $\ln(k_0)$  and  $T^{-1}$ , especially in the temperature range 40–90 °C, and the activation energy  $E_a$  was 0.5694 kJ mol<sup>-1</sup> based on the calculation using the experimental data. The activation energy of the catalytic reactions was thus small, indicating that the catalytic reactions can easily occur.

The value of  $\ln(k_0)$  at 30 °C deviated from the fitted curve, probably due to the low temperature of the reaction system, which did not provide sufficient activation energy for the catalytic reactions. The value of  $\ln(k_0)$  at 100 °C also deviated

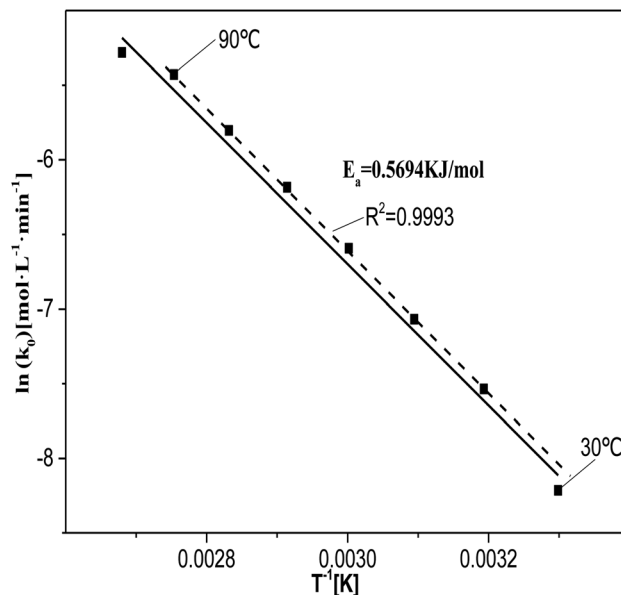


Fig. 8 Relationship between  $\ln(k_0)$  and  $1/T$  at  $T = 30\text{--}100\text{ }^{\circ}\text{C}$ , where  $c_0(\text{HNO}_3) = 5\text{ M}$ ,  $c_0(\text{H}_2\text{C}_2\text{O}_4) = 0.1\text{ M}$ , and  $S/L = 19.5\text{ g L}^{-1}$ .

from the fitting curve. This may be due to the fact at 100 °C the rate at which the reactants diffuse from the solution to the catalyst surface was lower than the rate of reaction between the reactants and active sites or active species. This indicates that the degradation of oxalic acid occurs at or near the catalyst surface.

Further, some evidence for the involvement of  $\text{NO}_3^-/\text{H}^+$  in the catalytic reactions could be found in Fig. 1 and 7. As a result, the effects of  $\text{NO}_3^-$  and  $\text{H}^+$  on oxalic acid degradation were investigated separately and are described in the next section.

### 3.3 Influence of $\text{NO}_3^-/\text{H}^+$ on oxalic acid degradation

Based on the experimental results shown in Fig. 9, a hypothesis for the involvement of  $\text{NO}_3^-$  and  $\text{H}^+$  in the catalytic reactions is proposed, which is supported by the results for the  $\text{H}^+$  effect on  $k_0$  in Fig. 10 and 11. The oxalic acid degradation associated with the oxalic acid form in solution is shown in Fig. 11.

**3.3.1  $\text{NO}_3^-$  effect on  $k_0$ .** Fig. 9 shows  $k_0$  in solution with Pt/SiO<sub>2</sub> as a catalyst in the nitrous acid/sodium nitrate range from 1–5 M. Oxalic acid degradation clearly increased with the increasing  $c(\text{NO}_3^-)$  in the  $c(\text{NaNO}_3)$  range from 1–5 M. Considering that  $c(\text{H}^+)$  is much lower than  $c(\text{NO}_3^-)$  in solution, the oxalic acid degradation should be attributed to  $\text{NO}_3^-$  rather than  $\text{H}^+$  (measurement pH  $\approx 1.9$  in the reaction solution,  $c(\text{H}^+) \approx 0.0126\text{ M}$  from the ionized oxalic acid). This result indicated that  $\text{NO}_3^-$  is involved in the catalytic reactions, and in particular that  $\text{NO}_3^-$  may interact with Pt. In addition, the concentration of HNO<sub>3</sub> molecules in solution increased linearly with the nitrate concentration, and the concentration range of HNO<sub>3</sub> molecules was  $0.632\text{--}3.16 \times 10^{-3}\text{ M}$  in solution. If the HNO<sub>3</sub> molecule is the primary oxidant during the degradation of oxalic acid under catalysis, at  $c(\text{NaNO}_3) = 1\text{ M}$  (HNO<sub>3</sub> molecules  $\approx 0.632 \times 10^{-3}\text{ M}$ ), the

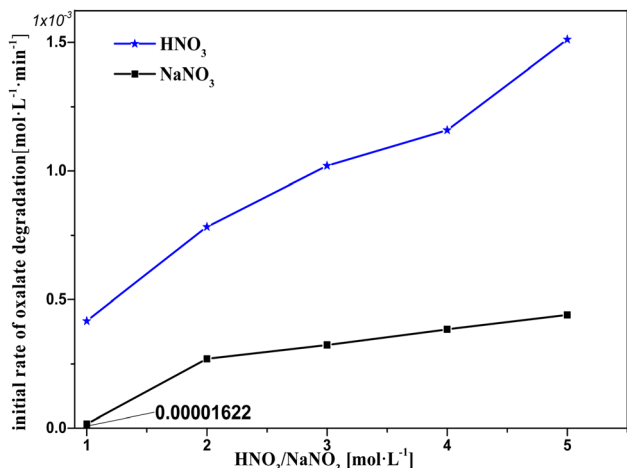


Fig. 9 Initial rate of oxalic acid degradation in solution at varying  $\text{HNO}_3/\text{NaNO}_3$  concentrations at  $T = 90^\circ\text{C}$ , where  $c_0(\text{HNO}_3/\text{NaNO}_3) = 1\text{--}5\text{ M}$ ,  $c_0(\text{H}_2\text{C}_2\text{O}_4) = 0.1\text{ M}$ , and  $S/L = 19.5\text{ g L}^{-1}$ .

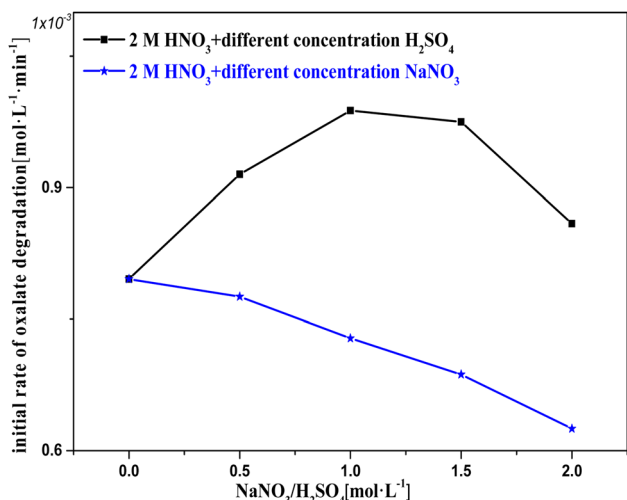


Fig. 10 Initial rate of oxalic acid degradation in solution based on 2 M nitric acid with varying  $\text{H}_2\text{SO}_4/\text{NaNO}_3$  concentrations added at  $T = 90^\circ\text{C}$ , where  $c_0(\text{HNO}_3) = 2\text{ M}$ ,  $c_0(\text{H}_2\text{SO}_4/\text{NaNO}_3) = 0\text{--}2\text{ M}$ ,  $c_0(\text{H}_2\text{C}_2\text{O}_4) = 0.1\text{ M}$ , and  $S/L = 19.5\text{ g L}^{-1}$ .

degradation of oxalic acid should be evident. However, oxalic acid was practically never degraded in the experiments with  $c(\text{NaNO}_3) = 1\text{ M}$ . This result suggests that the primary oxidant was not the  $\text{HNO}_3$  molecule.

At  $c(\text{NaNO}_3) = 1\text{ M}$ , oxalic acid degradation hardly occurred. This may be because the  $\text{NO}_3^-$  in the solution barely diffuses on the catalyst surface, resulting from the fact that each  $\text{NO}_3^-$  is firmly bound by hydrogen bonding in a cage made of water molecules and that the amount of  $\text{NO}_3^-$  is well below the amount of water molecules.<sup>24,25</sup> In the  $c(\text{NaNO}_3)$  range 1–2 M, oxalic acid degradation increased with the increasing  $c(\text{NaNO}_3)$ , resulting from the fact that the amount of  $\text{NO}_3^-$  that can diffuse out to the catalyst surface unbound by water molecules rapidly increases with increasing  $c(\text{NaNO}_3)$ . In the  $c(\text{NaNO}_3)$  range 2–5 M, the amount of adsorbed sites on the catalyst surface was much

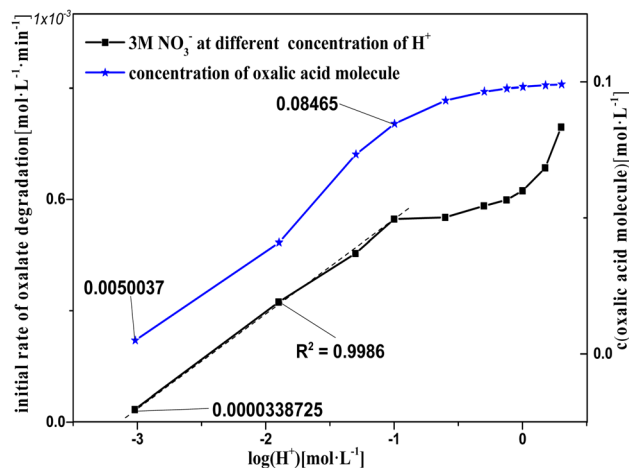


Fig. 11 Concentration of oxalic acid molecules and initial rate of oxalic acid degradation based on 2 M nitric acid solution with varying concentrations of sodium hydroxide added at  $T = 90^\circ\text{C}$ , where  $c_0(\text{NO}_3^-) = 2\text{ M}$ ,  $c_0(\text{H}^+) = 10^{-3}$  to 2 M,  $c_0(\text{H}_2\text{C}_2\text{O}_4) = 0.1\text{ M}$ , and  $S/L = 19.5\text{ g L}^{-1}$ .

smaller than the nearby  $\text{NO}_3^-$ , resulting in a substantial buffer against oxalic acid degradation compared to the  $c(\text{NaNO}_3)$  range 1–2 M. Moreover, the fact that  $\text{H}^+$  obviously promotes oxalic acid degradation could be found by comparing the  $k_0$  of each sodium nitrate solution experiment with the corresponding nitric acid solution. From the above discussion, we conclude the following hypothesis:

$\text{NO}_3^-$  is readily adsorbed on the catalyst surface and the probability of direct  $\text{NO}_3^-$  activation by Pt is relatively low, but  $\text{H}^+$  has an effective boost effect on the  $\text{NO}_3^-$  activation reaction.

**3.3.2  $\text{H}^+$  effect on  $k_0$ .** The effect of  $\text{H}^+$  on  $k_0$  is discussed based on 2 M  $c(\text{NO}_3^-)$  separately in the  $c(\text{H}^+)$  range 2–4 M (Fig. 10) and in the  $c(\text{H}^+)$  range 0.001–2 M (Fig. 11).

Fig. 10 shows  $k_0$  in solution with Pt/SiO<sub>2</sub> as a catalyst based on 2 M nitric acid solution with varying concentrations of  $\text{H}_2\text{SO}_4/\text{NaNO}_3$  added to adjust  $c(\text{H}^+)/c(\text{NO}_3^-)$ . In the  $c(\text{H}_2\text{SO}_4)$  range 0–1 M, the oxalic acid degradation effectively increased with  $c(\text{H}^+)$ , suggesting that an appropriate amount of  $\text{H}^+$  promotes catalytic reactions to occur. This result agrees with the hypothesis. In the  $c(\text{H}_2\text{SO}_4)$  range 1–2 M, the oxalic acid degradation slowly decreased with  $c(\text{H}^+)$ , suggesting that excess  $\text{H}^+$  promotes catalytic reactions to occur. The negative effect of excess  $\text{H}^+$  may result from excess  $\text{SO}_4^{2-}/\text{HSO}_4^-$  in the solution competing with the reactant for sites on the catalyst surface,<sup>26,27</sup> and by increasing  $c(\text{H}_2\text{SO}_4)$ , the promoting effect of  $\text{H}^+$  hardly increased substantially.

In the  $c(\text{NaNO}_3)$  range 0–2 M, oxalic acid degradation decreased with increasing  $c(\text{NO}_3^-)$ . This result indicates that excess  $\text{NO}_3^-$  makes a clearly negative contribution to the catalytic reactions, while the same result was obtained by an alternative experiment with potassium nitrate used in order to exclude  $\text{Na}^+$  interference. The effect of excess  $\text{NO}_3^-$  on oxalic acid degradation was similar to that of excess sulfuric acid, but the reduction in oxalic acid degradation due to excess  $\text{NO}_3^-$  exceeded the effect of excess sulfuric acid at the

same concentration. This phenomenon may be due to the fact that  $\text{HSO}_4^-$  can be given  $\text{H}^+$  to activate  $\text{NO}_3^-$  adsorbed on the active sites during the diffusion–collision process between  $\text{HSO}_4^-$  and the catalytic surface, but  $\text{NO}_3^-$  cannot.

Fig. 11 shows  $k_0$  in solution with Pt/SiO<sub>2</sub> as a catalyst based on 2 M nitric acid solution with varying concentrations of sodium hydroxide added to adjust  $c(\text{H}^+)$ . In the  $\log(\text{H}^+)$  range  $-7$  to  $-3$ , oxalic acid was a little degraded, as observed based on the absence of gas from the reaction solution, indicating that the catalytic reactions did not occur in this  $\log(\text{H}^+)$  range. There was a clear linear relationship between  $k_0$  and  $\log(\text{H}^+)$  in the  $\log(\text{H}^+)$  range  $-3$  to  $-1$ , and the pattern of  $k_0$  and  $\log(\text{H}^+)$  in the range from  $-1$  to  $0.3013$  was similar to a partial parabola. Clearly, the patterns of  $k_0$  and  $\log(\text{H}^+)$  were different in the  $\log(\text{H}^+)$  range  $-3$  to  $-1$  and  $-1$  to  $0.3013$ , suggesting that oxalic acid degradation in these two components was affected by different factors. The pattern of  $k_0$  in the  $\log(\text{H}^+)$  range  $-3$  to  $-1$  was attributed to the promotion of  $\text{H}^+$  to the  $\text{NO}_3^-$  activation reaction, and that in the range  $-1$  to  $0.3013$  was attributed to another reaction rather than the  $\text{NO}_3^-$  activation reaction. Furthermore, the patterns of  $k_0$  and  $\log(\text{H}^+)$  were similar with the concentration of oxalic acid molecules and  $\log(\text{H}^+)$  in the range from  $-1$  to  $0.3013$ , and the ionization degree of the oxalic acid carboxyl group ( $-\text{COOH}$ ) was controlled by the  $c(\text{H}^+)$  in solution. This result reveals that the  $-\text{COOH}$  of oxalic acid molecules were correlated with oxalic acid degradation, and that the ionized oxalic acid was hardly degraded in the catalytic reactions.

In general, there are two ways in which organic acids are degraded *via* the destruction of the  $-\text{COOH}$  in catalytic reactions. The first is that the Pt–H structure arises from the reaction between the carboxyl group and the nano-platinum, and the electron of the activated H atoms are transferred to oxidation intermediates *via* the potential difference at the catalyst surface, with  $\text{H}^+$  produced simultaneously.<sup>28–30</sup> The second is that the oxidation intermediates are reduced by the H atoms of the carboxyl group *via* the oxidative dehydrogenation reaction.<sup>30–32</sup> However, for both pathways, the oxidation intermediates must be present on the catalyst surface, and the nano-platinum of the active ingredient of the catalyst readily oxidizes to the Pt–O structure.<sup>33–37</sup>

### 3.4 Pt–O produced from the reaction between $\text{NO}_3^-$ and nano-platinum

This section briefly described how the Pt–O structure was found as the oxidation intermediates from the  $\text{NO}_3^-$  activation reaction, which supports and enriches the hypothesis from the plots in Fig. 12–14.

In the Raman and XPS experiments, the selected catalyst grains were evenly divided into two parts. One part was immersed in pure water, and the other in a solution of 5 M nitric acid for 2 h, washed three times in pure water, and finally dried in a nitrogenous atmosphere for 24 h, and separately ground to a powder for oxygen-free preservation.

The Raman spectra for the catalyst treated with 5 M nitric acid showed a different absorption peak at 805 nm compared to the control sample in Fig. 12, and the 805 nm peak was

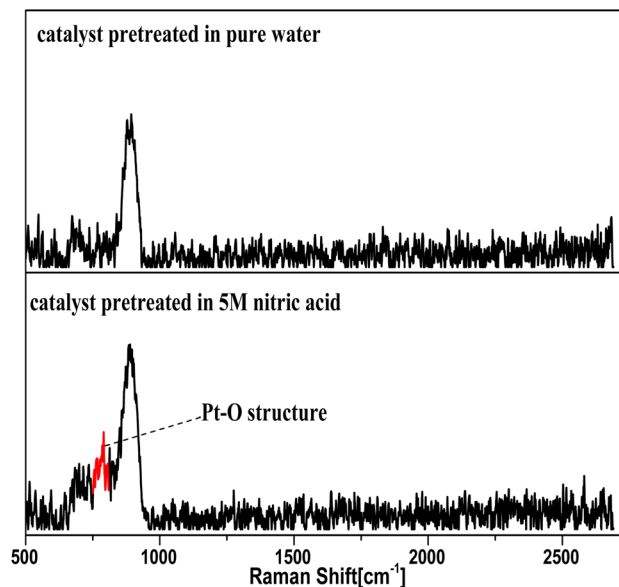


Fig. 12 Raman spectra of Pt/SiO<sub>2</sub> pretreated with 5 M HNO<sub>3</sub> and pure water.

attributed to the structure of Pt–O,<sup>38,39</sup> which revealed that the oxidation intermediates were Pt–O derived from the reaction between  $\text{NO}_3^-$  and the nano-platinum.

The Pt 4f XPS spectrum obtained from the catalyst treated with 5 M nitric acid is shown in Fig. 13. The spectrum exhibited a dominant doublet at the binding energy (BE) of 74.9 eV corresponding to Pt(IV), a doublet at 72.4 eV corresponding to Pt(II), and a doublet at 71.2 eV corresponding to Pt<sup>0</sup>.<sup>40</sup> The concentration ratios of Pt<sup>0</sup>/Pt(II)/Pt(IV) were 0.89 : 0.064 : 0.046 for the catalyst treated with pure water, and 0.1 : 0.702 : 0.198 for the catalyst

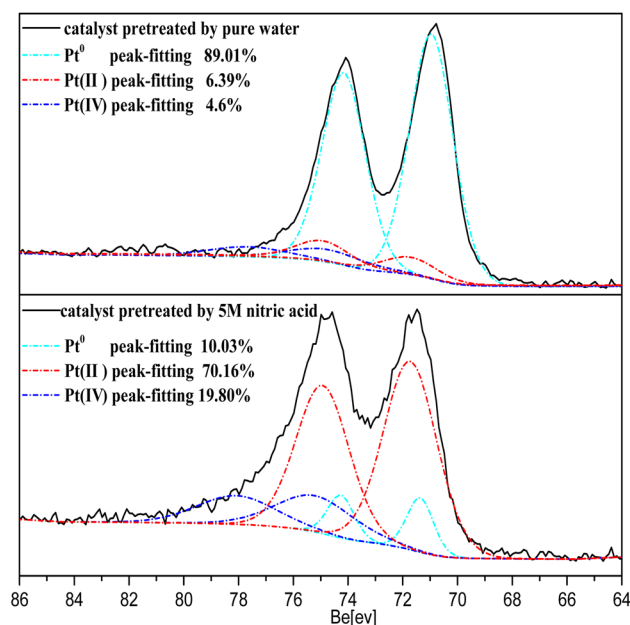


Fig. 13 Pt 4f XPS spectra of Pt/SiO<sub>2</sub> pretreated with 5 M HNO<sub>3</sub> and pure water.

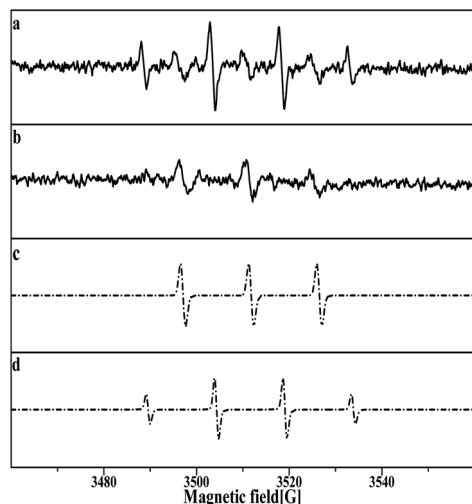


Fig. 14 Pt/SiO<sub>2</sub> pretreated with 5 M HNO<sub>3</sub> in (a) aqueous solution, (b) methanol solution. (c) Simulation of DMPO–OH with  $a_N = 14.76$ ,  $a_H = 14.76$ , and  $g = 2.00630$ , (d) simulation of DMPOX with  $a_N = 14.7$  and  $g = 2.00625$ .

treated with 5 M nitric acid, as determined from the region of the Pt<sup>0</sup>, Pt(II), Pt(IV) fits obtained by decomposing the Pt 4f spectrum in Fig. 13. It was found that most of the Pt<sup>0</sup> on the surface of the catalyst was oxidized in the form of Pt(II)/Pt(IV) through treatment with 5 M nitric acid, and the Pt(II) and Pt(IV) on the catalyst surface were commonly PtO and PtO<sub>2</sub>.<sup>40,41</sup> These results revealed the production of Pt–O from the reaction between NO<sub>3</sub><sup>−</sup> and the nano-platinum.

In the EPR experiments, the selected catalyst grains were immersed in a solution of 5 M nitric acid for 2 h, washed three times in pure water, and finally dried in a nitrogenous

atmosphere for 24 h for oxygen-free preservation. Prior to EPR detection, two single pretreated Pt/SiO<sub>2</sub> samples were placed in aqueous and methanol solutions, respectively, before DMPO was added to the solution for the trapping reaction.

The DMPO–OH and DMPOX signals were obtained in the aqueous solution condition in Fig. 14a. These results suggest that some oxidation intermediates were present on the surface of the catalyst pretreated with nitric acid, and that the structure of Pt–O was most plausible as the oxidation intermediates, considering that no trace of peroxide radicals or other reactive species were found at the same time. DMPOX generally is derived from the oxidation of DMPO–OH adducts in aqueous solution,<sup>42,43</sup> but unexpectedly a DMPOX signal was evident in the presence of sufficient DMPO relative to the oxidation intermediates, and only the DMPOX signal was obtained in the methanol solution condition shown in Fig. 14b. This result suggests that the source of the DMPOX signal was not only that produced from the oxidation of DMPO–OH, but also from reactions between DMPO and the oxidation intermediates. Therefore, the formation processes of DMPOX could be determined and are shown in Fig. 15a and b, and the DMPO–OH adducts in Fig. 15c.

### 3.5 Reaction between the structure of Pt–O and oxalic acid molecules

The bond cleavage of oxalic acid molecules by Pt–O oxidation is discussed in Fig. 16.

Only the signals of DMPO–OH and DMPOX were obtained in aqueous solution with nitric acid and oxalic acid in Fig. 16a, but the signal generated by oxalic acid was not obtained. It is interesting to note the information on the bond cleavage of oxalic acid found in Fig. 16a, which shows the pretreated

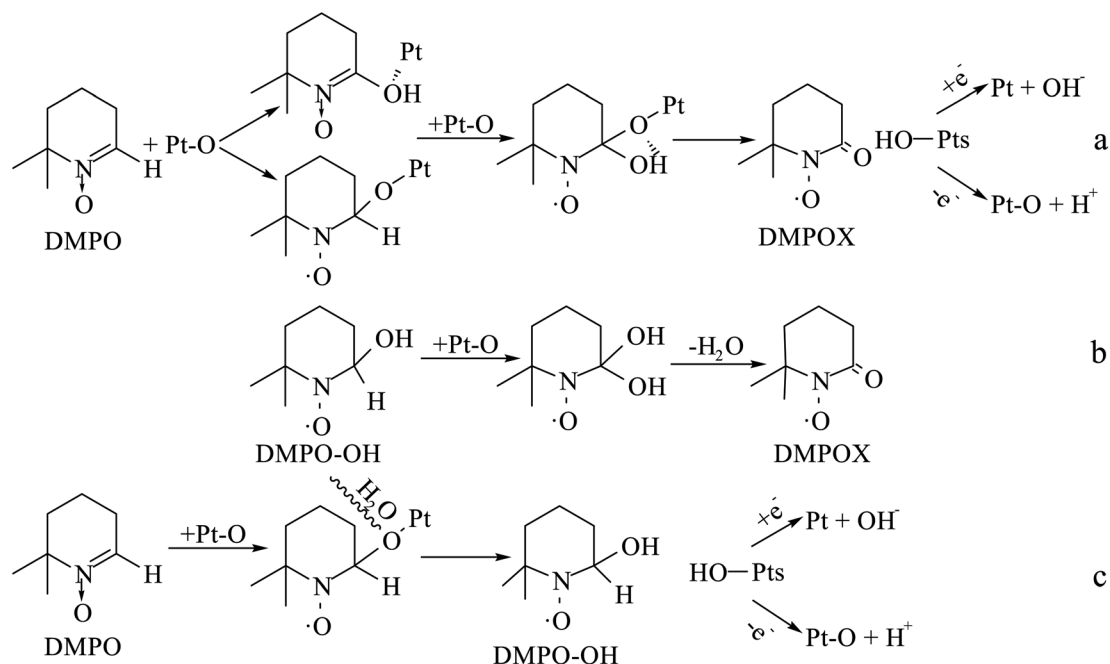


Fig. 15 Formation processes of DMPOX and DMPO–OH adducts for reactions between DMPO and Pt–O in aqueous or methanol solution.



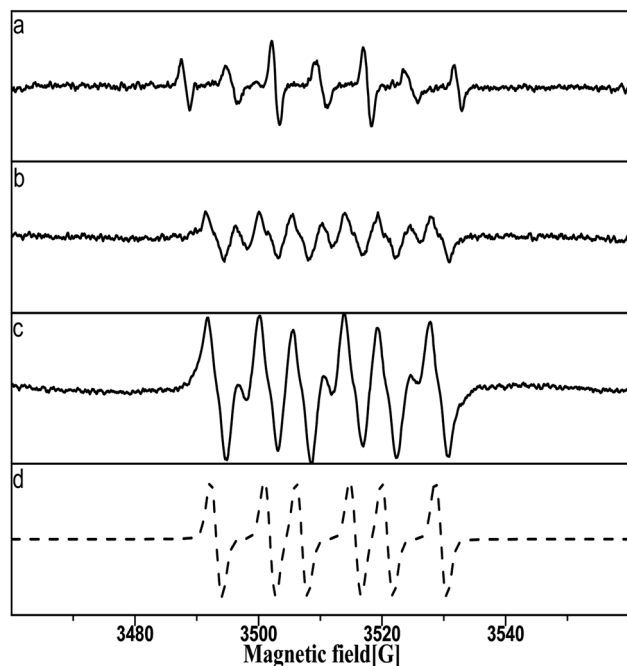


Fig. 16 Catalyst pretreated with 5 M nitric acid added to (a) aqueous solution containing 0.1 M nitric acid and 1 M oxalic acid, (b) aqueous solutions containing 1 M oxalic acid, (c) methanol solution containing 1 M oxalic acid. (d) Simulation of DMPO–OOC–COOH with  $a_N = 13.85$ ,  $a_H = 8.7$ , and  $g = 2.00665$ .

catalysts with 5 M nitric acid added to different solvents containing oxalic acid. In Fig. 16b and c, a clear signal can be seen related to the adduct of DMPO with the alkoxy radical, which in the experimental conditions should be  $\cdot\text{OOC-COOH}$  produced by the reaction of the oxalic acid molecule with Pt–O. This result indicates that the oxalic acid molecule was oxidized by Pt–O *via* an oxidative dehydrogenation reaction. It is worth noting that, in addition, the DMPO–OOC–COOH signal in Fig. 16c was much stronger than in Fig. 16b, and the  $\cdot\text{OOC-COOH}$  was not captured in Fig. 16a in the nitric acid solutions. This result reveals that  $\cdot\text{OOC-COOH}$  was unstable in aqueous solution and rapidly self-decomposed, particularly in the nitric acid solutions.

### 3.6 Catalyst durability

In the durability test, unpretreated Pt/SiO<sub>2</sub> was subjected to 20 cycles. The Pt leaching rate (Fig. 17) and  $k_0$  (Table 1) of these 20 cycles were obtained.

A single test was conducted with 4.88 g of catalyst added to a reaction mixture for reaction for 1 h, and then after obtaining 10 ml of sample solution from the reaction mixture, a new reaction mixture was added. The concentration of Pt in the sample solution was measured by ICP-OES (Avio 220 Max system).

The Pt leaching rate during the first catalytic run was 0.632% for Pt/SiO<sub>2</sub>, and it also appeared that the Pt leaching fluctuated around 0.15% from the 2nd to 20th runs, as shown in Fig. 17. Such Pt erosion may be mainly related to a fraction of Pt

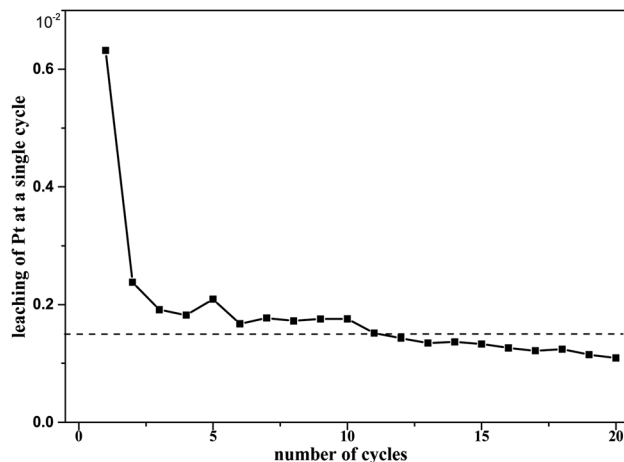


Fig. 17 Pt leaching of 20 cycles at  $T = 90\text{ }^\circ\text{C}$ , where  $c_0(\text{HNO}_3) = 3\text{ M}$ ,  $c_0(\text{H}_2\text{C}_2\text{O}_4) = 0.1\text{ M}$ , and  $S/L = 19.5\text{ g L}^{-1}$ .

Table 1 Initial rate of oxalic acid degradation of 20 cycles at  $T = 90\text{ }^\circ\text{C}$ , where  $c_0(\text{HNO}_3) = 3\text{ M}$ ,  $c_0(\text{H}_2\text{C}_2\text{O}_4) = 0.1\text{ M}$ , and  $S/L = 19.5\text{ g L}^{-1}$

Number of cycles	$N = 1$	$N = 2$	$N = 3$	$N = 4$	$N = 5$
$k_0$ [mol L <sup>-1</sup> min <sup>-1</sup> ]	0.00423	0.00403	0.00398	0.00390	0.00413
Number of cycles	$N = 6$	$N = 7$	$N = 8$	$N = 9$	$N = 10$
$k_0$ [mol L <sup>-1</sup> min <sup>-1</sup> ]	0.00397	0.00397	0.00406	0.00402	0.00398
Number of cycles	$N = 11$	$N = 12$	$N = 13$	$N = 14$	$N = 15$
$k_0$ [mol L <sup>-1</sup> min <sup>-1</sup> ]	0.00397	0.00400	0.00396	0.0390	0.00397
Number of cycles	$N = 16$	$N = 17$	$N = 18$	$N = 19$	$N = 20$
$k_0$ [mol L <sup>-1</sup> min <sup>-1</sup> ]	0.00395	0.00392	0.00395	0.00391	0.00388

particles being weakly bonded to the SiO<sub>2</sub> surface of freshly prepared catalysts during the first run. Therefore, pretreatment of catalysts is necessary before the catalysts are formally used for the first time. From the 2nd to the 20th cycle, the cumulative Pt leaching rate was approximately 2.98%. At the same time, the catalytic efficiency of Pt/SiO<sub>2</sub> did not decrease significantly over the total of 20 runs. This does not appear to be sufficient to justify the dramatic loss of activity of the catalyst during the runs. These results indicate the good durability of the catalyst in oxalic acid degradation with Pt/SiO<sub>2</sub> as a catalyst in the nitric acid solutions.

## 4 Reaction mechanism

Based on the above experimental results, the process of oxalic acid degradation in nitric acid solutions with Pt/SiO<sub>2</sub> as a catalyst occurred on the same catalyst surface as the following table of contents entry.

## 5 Conclusions

The reaction process of oxalic acid degradation in nitric acid solutions with Pt/SiO<sub>2</sub> as a catalyst was investigated and described. Strictly speaking, it is difficult to find evidence of oxalic acid degradation from catalytic reactions involving

nitrous acid, given that nitrous acid concentrations in nitric acid solutions are generally  $10^{2-3}$  times smaller than  $\text{NO}_3^-$ . The oxidation intermediates that can be produced by the reaction between nitrous acid and nano-platinum are still uncertain, but nitrous acid did not affect the experimental results in this work. The specific process of Pt-O formation from the reaction between  $\text{NO}_3^-$  and the nano-platinum requires further investigation. No evident self-decomposition of oxalic acid adsorbed on a catalyst was found. Catalytic reactions should be considered to have no induction period, and if an induction period exists, its duration should not exceed the mixing time of the reagent. The feasibility of applying this method to industrial production needs to be investigated. In industrial production, it is necessary to take into account that certain substances poison the catalyst, and that this substance is continuously produced from the irradiated decomposition of an extractive agent containing phosphorus in solution.

## Conflicts of interest

There are no conflicts to declare.

## Acknowledgements

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