

Communication

# Gradient Porous Structured MnO<sub>2</sub>-Nonwoven Composite: A Binder-Free Polymeric Air Filter for Effective Room-Temperature Formaldehyde Removal

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**Abstract:** Recently, MnO<sub>2</sub>-coated polymeric filters have shown promising performance in room-temperature formaldehyde abatement. However, a commonly known concern of MnO<sub>2</sub>/polymer composites is either MnO<sub>2</sub> crystal encapsulation or weak adhesion. This work reports a low-cost high-throughput and green strategy to produce binder-free MnO<sub>2</sub>-nonwoven composite air filters. The production approach is energy saving and environmentally friendly, which combines MnO<sub>2</sub> crystal coating on bicomponent polyolefin spunbond nonwovens and subsequent heat immobilizing of crystals, followed by the removal of weakly bonded MnO<sub>2</sub>. The binder-free MnO<sub>2</sub>-nonwoven composites show firm catalyst-fiber adhesion, a gradient porous structure, and excellent formaldehyde removal capability (94.5% ± 0.4%) at room temperature, and the reaction rate constant is 0.040 min<sup>-1</sup>. In contrast to the MnO<sub>2</sub>-nonwoven composites containing organic binders, the HCHO removal of binder-free filters increased by over 4%. This study proposes an alternative solution in producing catalyst/fabric composite filters for formaldehyde removal.

**Keywords:** MnO<sub>2</sub>; bicomponent polyolefin nonwovens; polymeric filter; binder-free; HCHO removal



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## 1. Introduction

Formaldehyde (HCHO), one of the major indoor air pollutants, is reported to be continuously emitted from construction and decoration materials [1,2]. In 2004, the International Agency for Research on Cancer (IARC) classified HCHO as carcinogenic to humans (Group 1), as evidence shows that nasopharyngeal cancer and leukemia correlate with exposure to formaldehyde [3,4]. In 2010, the World Health Organization (WHO) set the indoor guideline value for HCHO as 0.1 mg/m<sup>3</sup>, which has been adopted by major countries, such as Australia, China, Germany, and Japan [5]. According to a recent study investigating the residential HCHO concentrations in nine provinces in China, almost half (45.7%) of the residences exceeded the WHO limit [6]. Therefore, developing universal room-temperature HCHO treatment approaches is important and welcomed [7–9]. The commonly used catalysts for HCHO abatement include noble metals [10,11], transition metal oxides [12–14], modified carbons [15,16], metal–organic frameworks [17–19], and so on; however, transition metal oxide is the most attractive heterogeneous catalyst in terms of robust performance and low energy consumption.

Among transition metal oxide catalysts, manganese dioxide (MnO<sub>2</sub>) is widely used in HCHO heterogeneous catalytic removal as it can readily oxidize HCHO and convert it to H<sub>2</sub>O and CO<sub>2</sub> [20–22]. However, MnO<sub>2</sub> crystals are difficult to handle and utilize, not ideal for room-temperature HCHO abatement in practical applications [23]. In this regard, immobilizing MnO<sub>2</sub> on a fibrous substrate is of great interest, because the firm adhesion of MnO<sub>2</sub> on substrates sets a fundamental basis for real applications.

Previous reports on MnO<sub>2</sub>-fiber composite filters studied their performance for HCHO removal at room temperature. For example, Wang et al. [24] developed a one-step hydrothermal approach to deposit MnO<sub>2</sub> on polyethylene terephthalate (PET) fibers, allowing over 94% removal efficiency of HCHO (0.6 mg cm<sup>-3</sup>) at room temperature under a gas hourly space velocity (GHSV) of 90 L g<sub>cat</sub><sup>-1</sup> h<sup>-1</sup>. Hu et al. [25] produced a MnO<sub>2</sub>/polystyrene fibrous structure. Using 5 ppm of HCHO and a GHSV of 60 L g<sub>cat</sub><sup>-1</sup> h<sup>-1</sup>, the composites enable up to 88.2% HCHO removal efficiency. Additionally, Qu et al. [26] recently reported that utilizing a friction-heating adhesion approach shortened the production time of MnO<sub>2</sub>@PET composite. A possible concern with these systems is the low throughput in production, which could add cost to the final product. Organic binders are usually used to bind powderlike catalysts with fibrous substrates at mills. Sekine et al. [27] demonstrated continuous HCHO degradation capability using a fiber cloth filter binding with MnO<sub>2</sub> and activated carbons. However, the catalytic oxidation performance was partially hampered by the organic binders [24]. Besides, binders may also pose a threat to body health in production and utilization [28].

Direct adhesion of MnO<sub>2</sub> on polymeric fabrics remains a challenge for a scalable process. Therefore, it is of great importance to develop a green method that produces catalyst-supported hybrid filters at lower cost and high throughput. Here, we proposed a robust methodology to produce MnO<sub>2</sub>-coated fibrous filters by attaching MnO<sub>2</sub> to bicomponent polyolefin (bico-polyolefin) spunbond nonwovens. The bico-polyolefin spunbond nonwovens are made with core component polypropylene (PP) surrounded by sheath component polyethylene (PE). Due to its different melting temperature, a PE sheath will be sufficiently softened and infused to bind MnO<sub>2</sub> crystals at a lower temperature without destroying PP cores; thus, no additional organic binder is required for the system. The binder-free MnO<sub>2</sub>-nonwoven composite filters have gradient pore structures and excellent catalytic oxidation ability of HCHO at room temperature.

## 2. Materials and Methods

### 2.1. Materials

Potassium permanganate ( $\geq 99.5\%$ , KMnO<sub>4</sub>) was supplied by Shanghai Lingfeng Chemical Reagent Co., Ltd., Shanghai, China. n-Butyl alcohol ( $\geq 99.5\%$ , BA) was supplied by Shanghai Titan Scientific Co., Ltd., Shanghai, China. Poly(vinyl alcohol) (PVA) 1788 and HCHO solution ( $\geq 36\%$ ) were purchased from Shanghai Aladdin Reagent Co., Ltd., Shanghai, China. All reagents were of analytical grade and used without further purification. Hydrophilic bicomponent polyolefin (polyethylene/polypropylene, PE/PP) nonwovens with a basis weight of 110 g m<sup>-2</sup> were provided by Hangzhou Holyway Co., Ltd., Hangzhou, China. Styrene-acrylic emulsion (SAE, 7199A, solid content, 48.2%) was purchased from Guangzhou Suixin Chemical Co., Ltd., Guangzhou, China.

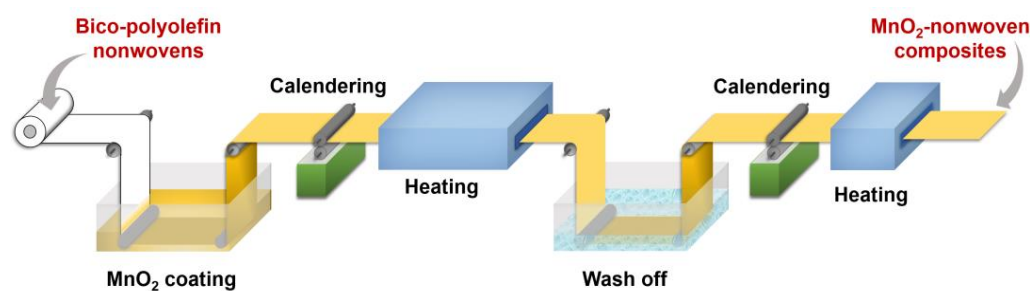
### 2.2. Synthesis of MnO<sub>2</sub> Catalysts

MnO<sub>2</sub> crystals were synthesized using reported procedures [29]. Briefly, 37.92 g of KMnO<sub>4</sub> was fully dissolved in 600 mL of distilled water under vigorous stirring at room temperature. Then 96 mL of BA was added to the above solution and stirred constantly for 12 h to complete the redox reaction. The synthesized crystals were filtered and washed in deionized water twice, finally dried at 90 °C for 12 h before use.

### 2.3. Preparation of MnO<sub>2</sub>-Nonwoven Composites

To produce binder-free MnO<sub>2</sub>-nonwoven composite air filters, a laboratory production line was utilized, as depicted in Figure 1. First, a certain amount of MnO<sub>2</sub> crystals was added to the water tank. After this step, PVA solution was added to the above water tank, which allowed MnO<sub>2</sub> crystals to suspend in solution. The weight percentage of the PVA agent was controlled at 1–3% compared with MnO<sub>2</sub>. Then the precursor solution was under vigorous stirring for 10 h to create MnO<sub>2</sub> suspension. After that, one piece of bico-polyolefin nonwoven swatch (11 cm × 12 cm) was soaked into MnO<sub>2</sub> suspension,

and then heated at 135 °C for 3 min after going through the calendaring process. When the heating process was completed, the MnO<sub>2</sub>-nonwoven composite was washed in a water bath to remove PVA, unbonded MnO<sub>2</sub>, and was finally dried at 100 °C (Figure S1). Repeating the above soaking, calendaring, heating, and washing steps one more time, the binder-free MnO<sub>2</sub>-nonwoven composite was obtained. Using 10%, 15%, and 20% of MnO<sub>2</sub> concentration in solution, the loading amount of MnO<sub>2</sub> in composite air filters ranges from 45 to 66 wt% (Table 1), denoted as 10%MnO<sub>2</sub>@Polyolefin, 15%MnO<sub>2</sub>@Polyolefin, and 20%MnO<sub>2</sub>@Polyolefin, respectively. The uniform dark color of the as-prepared MnO<sub>2</sub>-nonwoven composite confirms full coverage of white colored bico-polyolefin spunbond nonwovens (Figure S2).



**Figure 1.** Technological production process of MnO<sub>2</sub>-nonwoven composite filters.

**Table 1.** Preparation details in MnO<sub>2</sub>-nonwoven composites.

Sample	Concentration of MnO <sub>2</sub> in Precursor Solution	MnO <sub>2</sub> Content in MnO <sub>2</sub> -Nonwoven Composite
10%MnO <sub>2</sub> @Polyolefin	10%	45% ± 3%
15%MnO <sub>2</sub> @Polyolefin	15%	54% ± 4%
20%MnO <sub>2</sub> @Polyolefin	20%	66% ± 4%
MnO <sub>2</sub> @binder@Polyolefin	15%	50% ± 3%

As control, another type of MnO<sub>2</sub>-nonwoven composite was produced, where MnO<sub>2</sub> was bonded to PE/PP nonwovens with a SAE binder, denoted as MnO<sub>2</sub>@binder@Polyolefin. To prepare MnO<sub>2</sub>@binder@Polyolefin, 15% of MnO<sub>2</sub> crystals were first added to the water tank and stirred. Then SAE (SAE/MnO<sub>2</sub>, 0.4:1, *w/w*) was added under stirring. After that, another PE/PP swatch (11 cm × 12 cm) was soaked into the above solution, calendared, and heated at 90 °C for 5 min.

#### 2.4. Characterization

X-ray diffraction (XRD) pattern was recorded on an XRD tool (D/max-II B, Shimadzu, Kyoto, Japan) to investigate the crystalline structure. Fourier-transform infrared (FTIR) spectroscopy was carried out with a spectrometer (Nicolet iS10, Thermo Fisher, Waltham, MA, USA). The surface morphology of bico-polyolefin spunbond nonwovens and MnO<sub>2</sub>-nonwoven composites was investigated using a scanning electron microscope (SEM, SU5000, Hitachi, Tokyo, Japan). The pore size distributions of PE/PP nonwovens and MnO<sub>2</sub>-nonwoven composites were evaluated by utilizing a capillary flow porometer (CFP-1100AI, Porous Materials, Inc., Ithaca, NY, USA). The pressure drop of the bico-polyolefin nonwovens and MnO<sub>2</sub>-nonwovens composites was measured by employing an automated filter tester (TSI 8130, TSI, Inc., Shoreview, MN, USA).

The formaldehyde (HCHO) removal efficiency of MnO<sub>2</sub>-nonwoven composite air filters was measured in the lab-scale setup (Figure S3). The testing samples were placed in a commercial car air purifier (GP5202, Philips, Lumileds (Shanghai) Management Co., Ltd., Shanghai, China), which was then put in an acrylic reactor (0.232 m<sup>3</sup>). An amount of 0.7 µL of HCHO solution was injected into the reactor, and then the indoor air was blended by a 5 watt fan, which was fixed on top of the reactor. When the concentration of

HCHO was stabilized to 0.89 ppm, the car air purifier was switched on to start the test. The concentration of HCHO was monitored by a portable gas detector (BSQ-BCH2O, Shanghai Benshan Instrument and Equipment Co., Ltd., Shanghai, China) at 25 °C for 120 min. The HCHO removal performance was evaluated by plotting  $(C/C_0)$  versus reaction time, and the reaction rate constant ( $k$ ) was defined as Equation (1):

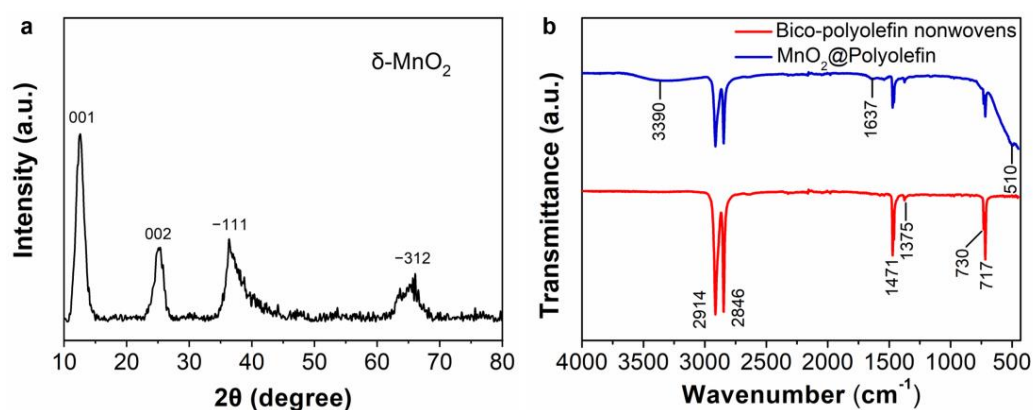
$$k = \ln\left(\frac{C_0}{C}\right) / t \quad (1)$$

where  $C_0$  (ppm) is the initial concentration of HCHO before the test, and  $C$  (ppm) is the dynamic concentration of HCHO at different time points.

### 3. Results and Discussion

#### 3.1. Production and Characterization of $MnO_2$ -Nonwoven Composites

The crystallographic structure of  $MnO_2$  crystal was identified by using XRD. Figure 2a presents the main diffraction peaks at 12.5°, 25.1°, 36.1°, and 65.4°, which correspond to the characteristic peaks of  $\delta$ - $MnO_2$  [30]. The FTIR spectra show surface features of bico-polyolefin nonwovens and a  $MnO_2$ @Polyolefin sample. As can be seen from the red spectrum of PE/PP nonwovens in Figure 2b, the peaks at 2914 and 2846  $cm^{-1}$  are assigned to the  $CH_2$  asymmetric stretch and  $CH_2$  symmetric stretch modes, respectively [31]. Interestingly, the characteristic peaks of low-density polyethylene (LDPE) and high-density polyethylene (HDPE) are all observed on the spectrum of PE/PP nonwovens. The peak located at 1375  $cm^{-1}$  belongs to the  $CH_2$  umbrella mode of LDPE, whereas the peaks at 730 and 717  $cm^{-1}$  are split  $CH_2$  rocking peaks of HDPE [31,32]. The above results indicate that both of the HDPE and LDPE chips were added to produce a PE sheath component in bico-polyolefin spunbond nonwoven production. It is worth noting that no peak of the PP component is observed in the FTIR spectrum due to the core–sheath feature of bico-polyolefin nonwovens. Compared with the red curve, the  $MnO_2$ @Polyolefin FTIR spectrum presents additional peaks at 3390, 1637, and 510  $cm^{-1}$ , which are assigned to the stretching vibration of -OH groups, -OH bending mode, and characteristic band of layered manganese oxides, respectively [33].

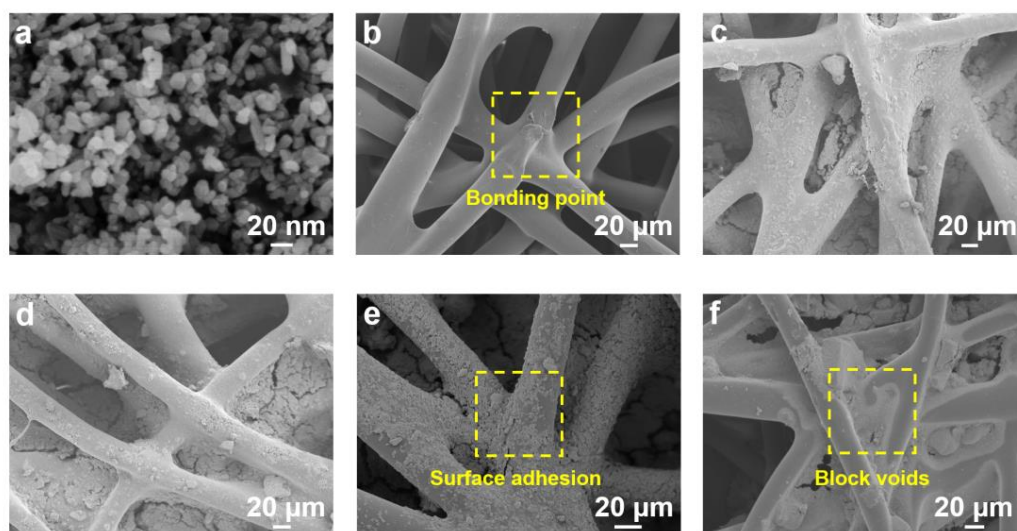


**Figure 2.** (a) XRD pattern of  $\delta$ - $MnO_2$ ; (b) FTIR spectra of bico-polyolefin spunbond nonwovens and  $MnO_2$ @Polyolefin filter.

The morphologies of  $\delta$ - $MnO_2$  crystals, bico-polyolefin nonwovens, and  $MnO_2$ -nonwoven composites were investigated by SEM. As shown in Figure 3a,  $\delta$ - $MnO_2$  crystals appear as spherules with an average diameter of 30 nm. The surface of bico-polyolefin nonwovens is relatively smooth compared with the  $MnO_2$ -nonwovens composites. The bonding points are clearly observed due to the diffusion of the molten PE sheath under appropriate temperature [34]. It can be seen from Figure 3c–e that a  $MnO_2$  nanocrystalline is firmly attached to the fiber surface, where the PE component acts as binders and assists in  $MnO_2$ -fiber adhesion. Notably, when a higher  $MnO_2$  concentration is prepared in so-



lution, the coverage areas for bico-polyolefin nonwovens increase significantly. It turns out that 20%MnO<sub>2</sub>@Polyolefin samples achieved almost full coverage. In contrast, as shown in Figure 3f, when the SAE adhesive was used to bind MnO<sub>2</sub>, the crystals tended to aggregate on fiber voids. We ascribe the observed particle agglomeration and block to the different surface tension caused by SAE. This is in stark contrast to the binder-free procedure that yields uniform and dense MnO<sub>2</sub> coatings on the surface of bico-polyolefin spunbond nonwovens.



**Figure 3.** SEM images of (a)  $\delta$ -MnO<sub>2</sub>, (b) bico-polyolefin nonwovens, (c) 10%MnO<sub>2</sub>@Polyolefin, (d) 15%MnO<sub>2</sub>@Polyolefin, (e) 20%MnO<sub>2</sub>@Polyolefin, and (f) MnO<sub>2</sub>@binder@Polyolefin.

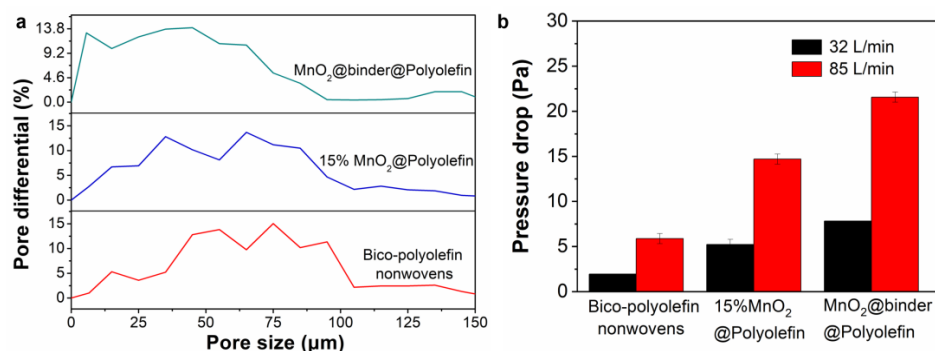
### 3.2. Evaluation of Pore Size Distribution of Bico-Polyolefin Nonwovens and MnO<sub>2</sub>-Nonwoven Composites

The pore size distribution results for bico-polyolefin nonwovens and MnO<sub>2</sub>-nonwoven composites are presented in Figure 4a. The bico-polyolefin nonwoven sample shows disordered pore size distribution as several peaks stand out in profile. The addition of MnO<sub>2</sub> to the bico-polyolefin nonwovens leads to a narrowed and gradient pore size distribution. Taking 15%MnO<sub>2</sub>@Polyolefin as an example, it reveals three dominant peaks centered in sequence at around 13, 37, and 63  $\mu$ m. The mean pore diameter decreases from 67.75 to 52.85  $\mu$ m compared with the bico-polyolefin nonwovens. We observe that the peak becomes broader and shifts for the MnO<sub>2</sub>@binder@Polyolefin sample, which gives rise to a further decreased mean pore diameter value, reaching 41.57  $\mu$ m. However, using SAC adhesive to bind MnO<sub>2</sub> did not create a gradient pore distribution for MnO<sub>2</sub>-nonwoven composites because most of the fiber junctions were blocked, which is consistent with the SEM results in Figure 3f. The results in Figure 4b reflect that the marked increase in pressure drop for MnO<sub>2</sub>@binder@Polyolefin is also attributed to the blocked pores, and a decreased mean pore diameter correlates with dropped air permeability.

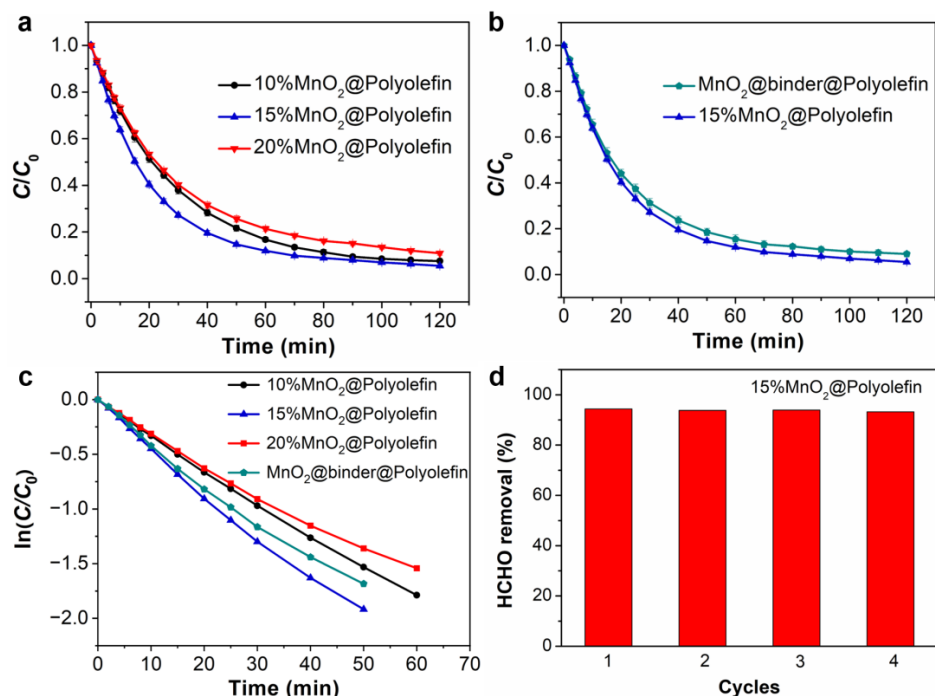
### 3.3. HCHO Removal Performance of MnO<sub>2</sub>-Nonwoven Composites

A low concentration HCHO removal performance over MnO<sub>2</sub>-nonwoven composites was investigated. Figure 5a shows HCHO removal results for 10%MnO<sub>2</sub>@Polyolefin, 15%MnO<sub>2</sub>@Polyolefin, and 20%MnO<sub>2</sub>@Polyolefin. All samples show good HCHO removal efficiency at low concentrations, and 15%MnO<sub>2</sub>@Polyolefin removed 94.5%  $\pm$  0.4% of HCHO within 120 min. Likewise, 10%MnO<sub>2</sub>@Polyolefin and 20%MnO<sub>2</sub>@Polyolefin removed 92.5%  $\pm$  0.6% and 89.1%  $\pm$  0.7%, respectively, in a same time period. The above results indicate that overloading MnO<sub>2</sub> crystals on nonwovens hinders the performance of HCHO catalytic removal. As shown in Figure 5b, using binders to produce MnO<sub>2</sub>-nonwoven composites could not only raise environmental concerns, but also lead to worse

removal performance. The HCHO removal efficiency for the  $\text{MnO}_2$ @binder@Polyolefin sample was reduced by over 4% compared with  $15\%\text{MnO}_2$ @Polyolefin. It is believed that particle agglomeration and encapsulation by an adhesive are the main factors that contribute to worse removal performance. In Figure 5c, we plotted the kinetic curves by measuring  $\ln(C/C_0)$  versus the reaction time. According to the pseudo-first-order model, the initial rate constants of  $10\%\text{MnO}_2$ @Polyolefin,  $15\%\text{MnO}_2$ @Polyolefin,  $20\%\text{MnO}_2$ @Polyolefin, and  $\text{MnO}_2$ @binder@Polyolefin were  $0.030$ ,  $0.040$ ,  $0.027$ , and  $0.035 \text{ min}^{-1}$ , respectively. In addition,  $15\%\text{MnO}_2$ @Polyolefin exhibited impressive reproducibility (Figure 5d) as the HCHO removal performance showed no significant difference after four tests. The HCHO removal performance of selected catalysts is summarized in Table S1, Supporting Information. In comparison with other materials,  $15\%\text{MnO}_2$ @Polyolefin showed acceptable performance in overall HCHO removal.



**Figure 4.** (a) Pore size distribution and (b) pressure drop of bico-polyolefin nonwovens,  $15\%\text{MnO}_2$ @Polyolefin, and  $\text{MnO}_2$ @binder@Polyolefin.



**Figure 5.** (a) HCHO removal test on  $10\%\text{MnO}_2$ @Polyolefin,  $15\%\text{MnO}_2$ @Polyolefin, and  $20\%\text{MnO}_2$ @Polyolefin. (b) Comparisons of HCHO removal performance on  $15\%\text{MnO}_2$ @Polyolefin and  $\text{MnO}_2$ @binder@Polyolefin. (c) Reaction kinetic curves of  $10\%\text{MnO}_2$ @Polyolefin,  $15\%\text{MnO}_2$ @Polyolefin,  $20\%\text{MnO}_2$ @Polyolefin, and  $\text{MnO}_2$ @binder@Polyolefin for HCHO removal following the pseudo-first-order model. (d) Reproducibility tests of HCHO removal performance on  $15\%\text{MnO}_2$ @Polyolefin.

#### 4. Conclusions

In summary, we demonstrated a robust approach to produce binder-free MnO<sub>2</sub>-nonwoven composite filters using  $\delta$ -MnO<sub>2</sub> crystals bonded firmly on the surface of bicomponent PE/PP spunbond nonwovens. The SEM images of MnO<sub>2</sub>@Polyolefin samples show that the molten PE component enables MnO<sub>2</sub> to be attached to a fiber surface, whereas nanocrystalline MnO<sub>2</sub> tends to be aggregate at fiber junctions to block inherent pores for MnO<sub>2</sub>@binder@Polyolefin. Results of pore size distribution and pressure drop confirm that the gradient porous structures are constructed for MnO<sub>2</sub>@Polyolefin filters. Moreover, the HCHO removal test elucidates that binder-free MnO<sub>2</sub>@Polyolefin filters show improved HCHO removal performance ( $94.5\% \pm 0.4\%$ ,  $k = 0.040 \text{ min}^{-1}$ ) in contrast to MnO<sub>2</sub>@binder@Polyolefin filters ( $90.2\% \pm 0.9\%$ ,  $k = 0.035 \text{ min}^{-1}$ ). We believe that such a green and environmentally friendly approach will provide an alternative solution in producing catalyst/fabric composite filters.

**Supplementary Materials:** The following supporting information can be downloaded at: <https://www.mdpi.com/article/10.3390/polym14122504/s1>, Figure S1: Washing step to remove PVA and unbonded MnO<sub>2</sub> crystals; Figure S2: Optical photograph of bico-polyolefin nonwovens and 15%MnO<sub>2</sub>@Polyolefin; Figure S3: Lab-scale setup for formaldehyde removal testing; Figure S4: Linear fitting of the reaction kinetic curves; Table S1: Summary of HCHO removal performance on a selected catalyst.

**Author Contributions:** Conceptualization, Z.D.; methodology, Z.D.; validation, Z.D.; investigation, Z.D., Y.S. and J.Y.; writing—original draft preparation, Z.D.; writing—review and editing, Z.D. and Y.S.; supervision, J.Y. All authors have read and agreed to the published version of the manuscript.

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