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Original Article

Possible predictive formulas for quantitative and time-based estimation of muscle strength during motion

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Abstract. [Purpose] To examine the validity of the predictive formulas based on the angle information of the segment center of mass and moments of inertia, and to propose a joint moment estimation method. [Participants and Methods] Twenty nine young healthy adults were divided into two groups: the Creation group (20 adults) was needed to create the prediction formulas, and the Verification group (9 adults) was needed to verify the formulas. By monitoring the Creation group, the angular information from inertial motion sensors and moments of inertia of each limb were used to estimate actual ankle joint moment and knee joint moment. Thereafter, the actual joint moments was derived from the Verification group and compared to the predicted values via Pearson correlations. [Results] Good to excellent correlations were obtained between the actual joint moments of the two groups for most of the motions. [Conclusion] It is suggested that the predictive formulas created from the angle information of the segment center of mass and moments of inertia can be used for an approximate estimation of the lower limb joint moments in the sagittal plane and more clinically useful tools need to be considered in the future. Key words: Joint moment, Prediction formulas, Muscle strength

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INTRODUCTION

Muscle strength measurements are essential for determining therapeutic interventions and functional prognosis related to physical therapy¹⁾. Manual Muscle Testing (MMT) or Hand-Held Dynamometers (HHD) are commonly used for strength assessment²). MMT is subjective and can vary with the physical strength of the examiner³). Also, HHD can cause an error depending on the muscle to be assessed and the measurement position⁴). Furthermore, these assessments are limited by measurement of maximum muscle strength that a specific muscle group exerts during isometric contractions in a fixed posture.

Physical therapy, which maintains, restores, and improves movement and activity⁵), would be optimized by evaluations of muscle strength exerted during motions. Initially, motions can be determined by movements that move in a particular manner over time⁶) and most human movements are rotational of a segment around a joint. Joint moment, defined as the force required at a particular time, can not only be used to reflect muscle force during motions but also the timing of the exertion of muscle strength. For example, the joint moments during walking of patients with knee osteoarthritis differs not only in peak value but also in its timing depending on disease severity⁷). Also, joint moments during moving the seat off in patients with hip osteoarthritis differ as well⁸). Therefore, quantitative and time-based measures of joint moments are necessary in physical

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Table 1. Number of parameters

| Rigid link model | 5-Link | 4-Link | 3-Link |
|----------------------|--------|--------|--------|
| Number of parameters | 58 | 45 | 32 |
| Number of sensors | 7 | 6 | 5 |

therapy. Currently, the most common methods to measure of joint moments are combining three dimensional motion analysis system with force plate analyses⁹). However, this apparatus is too expensive, requires considerable space and thus is limited to use in clinics¹⁰).

Kodama et al.¹⁰⁾ have been suggested the way to estimate joint moments of squat and sit-to-stand by using the wearable inertial motion sensors. Their estimation applied the segment parameters calculated based on inertial properties of body segments¹¹⁾ and the segment inclination angles calculated from the motion sensors to Newton's equation of motion. The five-link model and the four-link model that the trunk was divided at the highest point of the iliac crest showed average correlation coefficients of about 0.98 for knee joint and about 0.80 for ankle joint. Even the three-link model that consisted of head, arm and trunk (HAT), Thigh, and Shank showed average correlation coefficients of about 0.95 for knee joint and about 0.60 for ankle joint. However, not only the vertical but also the horizontal factors have to consider and various parameters are necessary in order to solve the equation (Table 1). In addition, it must be applied to the equation one by one, which has a difficulty to generalize. Thus, it can be still difficult to use in busy clinics.

Clinical prediction models are commonly developed to facilitate diagnostic or prognostic probability estimations in daily medical practice¹²⁾. A user-friendly modality is necessary for the use of such formulas and nomograms to become a wide-spread part of routine practice¹³⁾. To the best of our knowledge, a prediction model for joint moments has not been developed yet. Joint moment can be calculated from angular acceleration and moment of inertia, although it is well known that joint moment varies with the changing joint angle¹⁴⁾. In addition, accelerations of the segment Center of Mass (CoM) position are crucial to calculate joint reaction forces. For these reasons, it is postulated that the prediction formulas for joint moments are utilized for the measurement of joint moments in sagittal plane for the purpose of pursuing the simplicity rather than strict accuracy. Therefore, the purpose of this study was to examine the validity of the prediction formulas created from angle information of inertia, and to propose an estimation method for joint moments.

PARTICIPANTS AND METHODS

Twenty-nine (15 males and 14 females) young healthy were analyzed. Individuals were excluded if they had orthopedic conditions, skin abnormalities, or were not able to provide consent. Participants were assigned randomly to two groups: the Creation group to create the prediction formulas of joint moments and the Verification group to verify the formulas. Twenty adults, consisting of 10 males and females (mean age: 21.1 ± 1.0 years, mean height: 166 ± 7.0 cm, mean weight: 60.8 ± 7.1 kg) participated in the Creation group and nine adults, consisting of 5 males and 4 females (mean age: 20.4 ± 0.8 years, mean height: 165 ± 6.0 cm, mean weight: 54.7 ± 6.5 kg) participated in the Verification group. After full explanation of the study, informed written consent was obtained. The study was approved by the Ethics Committee of the Graduate School of Medical Facilities, Nagasaki University (Approved number 18061429).

All the participants performed half squat, knee flexion and extension while standing on one leg, and walking. Participants were instructed to position the trunk vertically over the hip joints¹⁵). All motions were measured three times at three different speeds except walking. One-minute rest was taken every one measurement to minimize the effect of fatigue. During walking, participants crossed the force plates starting with their right foot 1 m from its entry.

Three Wearable inertial motion sensors (LP-WSD1101-OA Ver.1.0.0, 1,000 Hz, LOGICAL PRODUCT, Fukuoka, Japan) were attached to the outside of right limbs by using double-sided adhesive tape¹⁰ (Fig. 1). Wearable inertial motion sensors, often consist of tri-axial accelerometer, gyroscopes and magnetic sensors¹⁶ can measure angular velocity and have a high accuracy in calculating lower limb segmental angles during motions^{10, 17}). The sensors were oriented to have its sensitive axis of rotation perpendicular to the sagittal plane of motion¹⁸ in order to obtain the angular information in the segment CoM position. Attachment positions were as follows based on the positions of the approximate each

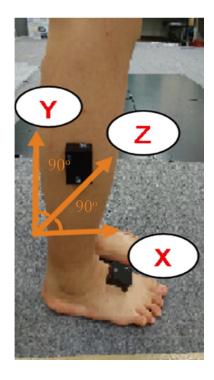


Fig. 1. Wearable inertial motion sensors

| Table 2. Estimation | formulas of moment of ine | ertia (Ae et al. 1992) |
|---------------------|---------------------------|------------------------|
|---------------------|---------------------------|------------------------|

| Gender | Moment of inertia |
|--------|--|
| | $I_1 = -350.3 + 418.3 \times L_1 + 6.6 \times W$ |
| Male | $I_2 = -62.8 + 104.7 \times L_2 + 1.1 \times W$ |
| | $I_3 = -41.0 + 228.1 \times L_3 + 0.01 \times W$ |
| | $I_1 = -262.1 - 14.1 \times L_1 + 9.0 \times W$ |
| Female | $I_2 = -46.4 + 67.1 \times L_2 + 1.2 \times W$ |
| | $I_3 = 32.2 + 153.7 \times L_3 + 0.16 \times W$ |

I=moment of inertia (kgcm²), 1=Thigh, 2=Shank, 3=Foot, L: length of the segment (m); W: weight (kg).

segment CoM position¹¹: *Thigh*: midway between greater trochanter and lateral knee joint space; *Shank*: midway between lateral knee joint space and lateral malleolus, *Foot*: center of dorsum of foot.

The three-dimensional motion analysis system equipped with 16 cameras and four force plates (DF5UM034A-1, 100 Hz, ANIMA, Tokyo, Japan) were used to measure actual joint moments. Reflection markers were attached to both anterior superior iliac spines, greater trochanters, lateral knee joint spaces, lateral malleoli, fifth metatarsal bones. These were synchronized to the motion sensors by using the wireless 8ch logger (LP-WSD1311-OA Ver1.1.0, LOGICAL PRODUCT).

All data were resampled to 1/30 seconds on the time axis by taking an average to reduce the high-frequency noise and to avoid aliasing of the sampling signal¹⁹. Analysis was done on sagittal plane and regarded as the rigid link model consisting of Thigh, Shank and Foot. The angular velocities v_j (deg/s) were integrated with time displacement dt (s) by using the trapezoidal approximation to calculate the angle of limbs θ_i (deg).

j=1-3 1=Thigh, 2=Shank, 3=Foot

 $\theta_j = \int v_j(t) \times dt$

The lineal resetting mechanism was applied by weighting linearly during integration in order to remove measurement error due to noise and drift²⁰⁾. The calculated angles were converted to the angular accelerations a_j (deg/s²) by doubly differentiating.

$a_j = d^2 \theta_j / dt^2$

The moments of inertia of the segments I_j (kgcm²) were estimated by substituting the body weight W (kg) and the partial lengths of limbs L_j (m) into the estimation formula (Table 2) created by Ae et al¹¹). Partial lengths were measured as follows: *Thigh*-greater trochanter to lateral knee joint space; *Shank*-lateral knee joint space to lateral malleolus; *Foot*-lateral malleolus to fifth metatarsal bone.

Statistical analysis was performed using JMP Pro 14 (SAS Institute Inc.). Stepwise-multi-regression analysis was performed to create the prediction formulas from the Creation group data. Actual Ankle Joint Moment (AJM) and Knee Joint Moment (KJM) were targeted variables whereas angular information and moments of inertia of each segment were explanatory variables. The foot rotation was accompanied by shank rotation at the motions under no load. Therefore, the explanatory variables did not include the foot items from knee flexion during single leg stance or swing phase during walking. The significance level for adopting the coefficients was p<0.05. Joint moments were estimated by inserting each explanatory variable of the Verification group into the formulas determined from the data of the Created group. Predicted and actual joint moments were compared by Pearson correlation analyses. Correlations were rated according to Portney and Watkins²¹): little or no relationship if ≤ 0.25 ; fair if 0.25 to 0.50; moderate to good if 0.50 to 0.75 and good to excellent if ≥ 0.75 .

RESULTS

Angular information obtained from the motion sensors are shown as the range between maximum and minimum values (Table 3). The angular accelerations were quite large relative to the angles in every motion. Only coefficients of the prediction formulas that were included in the regression analysis are listed in Table 4. Table 5 showed the peak of each direction and the correlations between predicted and actual joint moments. Joint moments represented plus toward extension and minus toward flexion. The peak of the predicted moments often differed from the actual ones. Though AJM had little correlation and differed within each individual R=0.34 (0.39), KJM had good to excellent correlations with little differences among individuals R=0.93 (0.03) during Half squat. Also, AJM and KJM showed good to excellent correlations in Knee flexion-extension during single leg stance: Knee flexion, AJM; R=0.89 (0.03), KJM; 0.78 (0.12) and Knee extension, AJM; R=0.94 (0.02), KJM; 0.94 (0.02). Furthermore, walking, a moving motion, also moderate to good correlations for both AJM and KJM, AJM; 0.79 (0.08), KJM; 0.51 (0.15).

DISCUSSION

This study aimed to examine the validity of the prediction formulas created from angle information of the segment CoM and moments of inertia, and to propose an estimation method for joint moments in clinics. Since the equations of moments

Table 3. Range of angular information

| Angular information | Segment | Half squat | Knee flexion | Knee extension | Walking |
|--|---------|---------------|---------------|----------------|----------------|
| | Thigh | 48 (15) | 20(7) | 83 (18) | 39 (8) |
| Angle (deg) | Shank | 37 (8) | 111 (17) | 125 (23) | 77 (7) |
| | Foot | 7 (4) | 72 (18) | 77 (19) | 52 (10) |
| | Thigh | 2,588 (2,075) | 3,193 (2,274) | 4,872 (3,860) | 7,821 (4,288) |
| Angular acceleration (deg/s ²) | Shank | 1,266 (756) | 6,160 (4,032) | 6,842 (4,377) | 9,408 (2,821) |
| | Foot | 1,303 (1,141) | 8,721 (4,470) | 8,923 (4,399) | 14,432 (4,429) |

Range was represented difference between maximum and minimum values. Visible values showed mean (SD).

Table 4. Coefficient of prediction formulas

| Explanation | | Half | squat | Vno | e flexion | Vnaa | xtension | | Wa | alking | |
|--------------------------|---------|-----------------------|-----------------------|-------|----------------------|----------------------|----------------------|----------------------|-------|-----------------------|-----------------------|
| Explanation variables | Segment | пап | squai | Klie | enexion | Kliee e. | xtension | Stance | phase | Swing | phase |
| variables | | AJM | KJM | AJM | KJM | AJM | KJM | AJM | KJM | AJM | KJM |
| | Thigh | 0.33 | 0.42 | 0.86 | 2.41 | 2.60 | 2.57 | -1.25 | -0.24 | | 0.14 |
| Angle | Shank | 0.63 | -0.77 | 1.83 | -0.09 | 3.21 | 0.09 | -0.30 | 0.13 | 3.0×10^{-3} | -0.08 |
| | Foot | -0.33 | -0.42 | | _ | | | 0.17 | 0.12 | | |
| Angular | Thigh | 1.0×10^{-3} | -1.0×10^{-3} | 0.01 | | 3.0×10^{-3} | 2.0×10^{-3} | -0.01 | | -4.0×10^{-5} | -1.0×10^{-3} |
| | Shank | -5.0×10^{-3} | 0.01 | 0.01 | 3.0×10^{-3} | 4.0×10^{-3} | 0.01 | -0.01 | -0.01 | -1.0×10^{-4} | -3.0×10^{-3} |
| acceleration | Foot | -3.0×10^{-3} | | | | | | 3.0×10 ⁻³ | | _ | |
| Moment of | Thigh | -0.08 | -0.06 | -0.06 | -0.19 | -0.08 | -0.19 | | 0.12 | | -0.03 |
| | Shank | 0.42 | 0.34 | 0.13 | 0.95 | 0.63 | 1.27 | 0.77 | -0.76 | -0.01 | 0.13 |
| ineritia | Foot | | 0.12 | | | | | | -0.56 | | |

p values were all <0.05. The diagonal line meant that it was not included by statistical analysis.

| Table 5. | Correlation | between | predicted | and actual | joint moments |
|----------|-------------|---------|-----------|------------|---------------|
| | | | | | |

| | | | AJM | | KJM | | | |
|----------------|-----------------------------|----------------|--------------|-------------|----------------|--------------|-------------|--|
| | | Extension peak | Flexion peak | R | Extension peak | Flexion peak | R | |
| II-16 | Predicted | 13 (3) | -12 (6) | 0.34 (0.39) | 55 (10) | -13 (7) | 0.93 (0.03) | |
| Half squat | Actual | 19 (6)* | -27 (13)* | | 75 (14)* | -13 (5) | | |
| Knee flexion | Predicted 24 (11) -205 (24) | 0.89 (0.03) | 71 (19) | -7 (6) | 0.78 (0.12) | | | |
| Knee nexion | Actual | 26 (12) | -161 (41)* | 0.89 (0.03) | 76 (18) | -27 (21)* | 0.78 (0.12) | |
| Knee extension | Predicted | 483 (71) | -134 (73) | 0.94 (0.02) | 242 (61) | -9 (12) | 0.94 (0.03) | |
| KIEC EXTENSION | Actual | 413 (54)* | -67 (20)* | | 233 (28) | -23 (19) | | |
| Walking | Predicted | 58 (14) | -14 (10) | 0.70 (0.08) | 17 (3) | -12 (2) | 0.51 (0.15) | |
| | Actual | 78 (10)* | -4 (2)* | 0.79 (0.08) | 17 (4) | -52 (17)* | 0.51 (0.15) | |

p values were all <0.001. Each visible value showed mean (SD).

* Indicated significant difference between groups p<0.05.

of inertia differed by gender and calculated from the body weight and the leg lengths, the influence of gender and body type was considered minimum. Thus, angular information of the segment was central for joint moments estimation.

KJM had good to excellent correlation but AJM had fair correlation during Half squat. On the other hand, good to excellent correlations were observed for both AJM and KJM in Knee flexion-extension during single leg stance. These knee bending were used for calibrating when measuring kinematic in sagittal plane²²). Since angular information was central in the prediction formulas, it is considered that sufficient estimation was possible with the calibrating motions that easily reflects the rotation of the segments.

Both AJM and KJM showed more than moderate to good correlations during Walking. The joint moments measurements in gait were diversified. For instance, Yang et al.²³⁾ added frontal and transverse intersegmental forces in addition to the kinematics of sagittal plane. Also, Karatsidis et al.²⁴⁾ used distribution algorithm from 17 motion sensors. These studies showed good to excellent correlations (from R=0.8), which indicates that intersegmental forces other than sagittal plane or many more sensors are required to obtain higher correlations.

Peak values in each direction of the predicted moments had some differences between actual ones. However, pursuing the accuracy makes it difficult to use in the clinics as more factors should be considered or more sensors are required^{23, 24)}. Ko-dama et al.¹⁰⁾ required at least total 32 parameters in both horizontal and vertical for estimation of joint moments. However, the prediction formulas in this study created from maximum 9 parameters using only three sensors and can obtain good to excellent correlations between actual joint moments for most of the motions. Thus, it is suggested that angle information of the segment CoM and moments of inertia can provide quantitative and time-based estimation for joint moments.

There are several limitations in the prediction formulas. Firstly, joint moments cannot be measured with the same accuracy as the large scale devices. Secondly, the sample size was small and limited to young healthy adults. Lastly, only AJM and KJM in sagittal plane were assumed, not including joint moments for other joints or in other than sagittal plane.

Further studies are necessary so that put to practical use in busy clinics. All data used for the prediction formulas were cut off to 30 samples per second, which is the same sampling frequency as the normal video camera^{25, 26)}. This means the acquisition of angular information could be substituted from the movie²⁷⁾. Recently, smartphones, which equipped with tri-axial accelerometer, gyroscopes and magnetic sensors, are widespread and can be used in place of the motion sensors²⁸⁾. These tools could be more clinically useful and need to consider whether can be used to estimate joint moment. Furthermore, an electromechanical delay exists from the onset of muscle electrical activation to the onset of joint moment²⁹⁾. Incorporating EMG could be more useful as an assessment of the timing of muscle strength exertion during motions.

In conclusion, it is suggested that the prediction formulas created from angle information of the segment CoM and moments of inertia can be used for approximate estimation of lower limb joint moments in sagittal plane. And more clinically useful tools need to consider in the future.

Presentation at a Conference

This paper was presented in World Confederation for Physical Therapy 2019 in Geneva. http://www.professionalabstracts.com/wcpt2019/iplanner/#/list

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