



## Research article

## Modeling of lattice parameters of cubic perovskite oxides and halides

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## ABSTRACT

Perovskites having the chemical formulae of  $ABX_3$  are promising candidates for various electronic, magnetic, and thermal applications. One of the important structural factors is  $a$  (the lattice constant), which represents the unit cell size. The variation in the lattice constant is a combined result of interactions between different ions, determined by valence electrons and ionic radii. The size and stability of unit cells have important influences on structural stabilities, bandgap structures, and therefore performance of materials. To obtain the lattice constant of cubic perovskites without going through experimental efforts such as synthesis and measurements, we construct a model based on Gaussian process regressions for cubic perovskite lattice constant predictions. The model utilizes the number of valence electrons as well as ionic radii of alloying elements as predictors. A total of 149 cubic perovskites containing fluorides, chlorides, and bromides with cation combinations of  $A^{1+}B^{2+}$ , as well as oxides with cation combinations of  $A^{1+}B^{5+}$ ,  $A^{2+}B^{4+}$ , and  $A^{3+}B^{3+}$  are explored. The model demonstrates good performance in terms of stabilities and accuracy, and thus could be a rapid approach to estimate lattice constants.

## 1. Introduction

Cubic perovskites,  $ABX_3$ , represent large groups of compounds that possess enormous diversities in the stoichiometry, structure, and physicochemical property. Depending on the anion type, cubic perovskites can be divided into two major groups, which are the oxide and halide. Because of differences in the valence of the ions of the halogen and oxygen, other alloying elements' types as well as oxidation states are different, and hence the properties of the materials. The monovalent  $A$ -cation will occupy unit cells' central positions, and the monovalent  $X$ -anions and the divalent  $B$ -cation will form the  $[BX_6]$  octahedra which will occupy corners around the  $A$ -cation, in cubic perovskite halides' ideal forms [1]. The monovalent ions (e.g.,  $Li^+$ ,  $Ag^+$ ,  $Cs^+$ , and  $K^+$ ) and organic ions ( $NH_4^+$ ) could replace  $A$ -cations. The divalent ions (e.g.,  $Sn^{2+}$ ,  $Mg^{2+}$ , and  $Ge^{2+}$ ) could replace  $B$ -cations. The halogens (e.g.,  $Cl^-$ ,  $I^-$ ,  $F^-$ , and  $Br^-$ ) could replace  $X$ -anions. In the cubic perovskite oxide, however,  $A$ -site and  $B$ -site cations' valence states can be flexible as well as exhibit different combinations, including  $A^{1+}B^{5+}$ ,  $A^{2+}B^{4+}$ , and  $A^{3+}B^{3+}$ .

With different constituting elements, compounds will have varying properties, which could include magnetoresistance, ferromagnetism, ferroelectricity, superconductivity, and piezoelectricity [2, 3, 4, 5]. These materials are promising candidates in different application fields, e.g., the high temperature superconductor [6, 7, 8, 9, 10, 11, 12, 13, 14], the multiferroic material [15, 16, 17, 18, 19], the magnetoresistor [15, 16, 17, 18, 19], the multiferroic material [20], and the topological insulator. In recent years, the halide perovskite has attracted a great amount of attention in many different areas, e.g., the laser cooling, the water splitting, the light emitting diode, and the solar cell [21, 22, 23].

The crystal structure is the fundamental parameter of a crystalline material, which is described by lattice parameters and atomic positions. Despite the large varieties of  $ABX_3$  cubic perovskites, lattice constants ( $a$ ) represent unit cell sizes. Ionic radii and the number of valence electrons of alloying elements, have a great influence on lattice parameters. Geometrically, ionic radius that depend on the element types, the valence states, the spin states, and the coordination number, are the most basic factors that determine the lengths of unit cell axes in three directions. The number of valence electrons influences the interatomic bonding and thus the lattice structure. Computational approaches have

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been utilized to simulate the crystal structure and model electronic structures, bandgaps, and magnetic orderings to help understand the structure-property relationship. Density-function-theory-based tools are frequently used, which require, at least, the basic structural parameters of repeat units. As one of the inputs, lattice constant values are mostly acquired using experimental methods that need great amounts of materials synthesis efforts as well as measurements [24]. It also limits exploring the  $ABX_3$  compound that is cubic but has not yet been synthesized. Additionally, first-principle simulations are based on known quantum mechanics, which demand high levels of computational resource and may be susceptible to underestimations or overestimations of the ionic interaction in other complex oxides. Machine learning has been applied for modeling and estimating many physical parameters of interest as well as performance of many materials across various types of systems [25, 26, 27, 28, 29, 30, 31, 32, 33, 34, 35, 36, 37, 38, 39, 40, 41, 42, 43, 44, 45, 46, 47, 48, 49, 50, 51]. We construct a model using Gaussian process regressions in order to conduct predictions of the cubic perovskite lattice constants. The model uses ionic radii as well as the number of valence electrons as predictors. The model demonstrates good performance in terms of stabilities and accuracy, and thus could be a rapid approach to estimate lattice constants. Particularly, by incorporating the number of valence electrons into the descriptor set, the model is able to distinguish the same ion with different structural surroundings based on valence, which enhances the predictive power of the model. Due to enormous choices of alloying elements, predicting the lattice constant accurately and efficiently can benefit researchers by saving great amounts of time and predictions can be used as inputs to theoretical research to possibly help expedite studies.

**2. Methodology**

The Gaussian process regressions (GPRs) come from nonparametric probabilistic types of models that tend to have decent performance for small data [52]. Let us employ  $y = x^T \beta + \epsilon$  to express a linear regression, where  $\epsilon \sim N(0, \sigma^2)$ . A GPR incorporates the following two items in order to explain the target  $y$ : (1) latent variables, expressed as  $l(x_i)$ ,  $i = 1, 2, \dots, n$ , of Gaussian processes (GPs), which satisfies  $l(x_i)$ 's being jointly Gaussian, and (2) basis functions, denoted by  $b$ , which project the predictors  $x$  into the feature space. Covariances of latent variables will capture smoothness of targets.

A GPR can be characterized by the mean and covariance. Let us employ  $k(x, x') = \text{Cov}[l(x), l(x')]$  to express the covariance,  $m(x) = E(l(x))$  to express the mean, and  $y = b(x)^T \beta + l(x)$  to express the GPR.  $l(x) \sim GP(0, k(x, x'))$  and  $b(x) \in \mathbb{R}^p$ . We parameterize  $k(x, x')$  by employing the hyperparameter expressed as  $\theta$ , and express it with  $k(x, x'|\theta)$ . Various algorithms will estimate  $\beta$ ,  $\sigma^2$ , and  $\theta$  and let one to specify  $b$  and  $k$ .

In this study, we consider the exponential (Equation (1)), squared exponential (Equation (2)), Matern 5/2 (Equation (3)), rational quadratic (Equation (4)), and Matern 3/2 (Equation (5)) kernels, as well as their automatic relevance determination (ARD) variations (Equations (6), (7), (8), (9), and (10)). We also study the empty (Equation (11)), constant (Equation (12)), linear (Equation (13)), and pure quadratic (Equation (14)) basis functions. In Equations (1)–(14),  $\sigma_l$  expresses the characteristic length scale,  $\sigma_f$  expresses the signal standard deviation,

$r = \sqrt{(x_i - x_j)^T (x_i - x_j)}$ ,  $\alpha$  expresses the positive scale-mixture parameter,  $\sigma_m$  ( $m = 1, 2, \dots, d$  and  $d$  expresses the number of predictors) expresses the separate length scale for each predictor in the ARD kernels whose  $\theta$  is expressed as  $(\log \sigma_1, \dots, \log \sigma_d, \log \sigma_f)$ ,  $B$  is expressed as  $(b(x_1), b(x_2), \dots, b(x_n))^T$ ,  $X$  is expressed as  $(x_1, x_2, \dots, x_n)^T$ , and

$$X^2 = \begin{pmatrix} x_{11}^2 & x_{12}^2 & \dots & x_{1d}^2 \\ x_{21}^2 & x_{22}^2 & \dots & x_{2d}^2 \\ \vdots & \vdots & \vdots & \vdots \\ x_{n1}^2 & x_{n2}^2 & \dots & x_{nd}^2 \end{pmatrix}$$

$$k(x_i, x_j|\theta) = \sigma_f^2 e^{-\frac{r}{\sigma_l}} \sim \text{Exponential Kernel} \tag{1}$$

$$k(x_i, x_j|\theta) = \sigma_f^2 e^{-\frac{1}{2} \frac{(x_i - x_j)^T (x_i - x_j)}{\sigma_l^2}} \sim \text{Squared Exponential Kernel} \tag{2}$$

$$k(x_i, x_j|\theta) = \sigma_f^2 \left( 1 + \frac{\sqrt{5}r}{\sigma_l} + \frac{5r^2}{3\sigma_l^2} \right) e^{-\frac{\sqrt{5}r}{\sigma_l}} \sim \text{Matern 5/2 Kernel} \tag{3}$$

$$k(x_i, x_j|\theta) = \sigma_f^2 \left( 1 + \frac{r^2}{2\alpha\sigma_l^2} \right)^{-\alpha} \sim \text{Rational Quadratic Kernel} \tag{4}$$

$$k(x_i, x_j|\theta) = \sigma_f^2 \left( 1 + \frac{\sqrt{3}r}{\sigma_l} \right) e^{-\frac{\sqrt{3}r}{\sigma_l}} \sim \text{Matern 3/2 Kernel} \tag{5}$$

$$k(x_i, x_j|\theta) = \sigma_f^2 e^{-\sqrt{\sum_{m=1}^d \frac{(x_{im} - x_{jm})^2}{\sigma_m^2}}} \sim \text{ARD-Exponential Kernel} \tag{6}$$

$$k(x_i, x_j|\theta) = \sigma_f^2 e^{-\frac{1}{2} \sum_{m=1}^d \frac{(x_{im} - x_{jm})^2}{\sigma_m^2}} \sim \text{ARD-Squared Exponential Kernel} \tag{7}$$

$$k(x_i, x_j|\theta) = \sigma_f^2 e^{\left( -\sqrt{5 \sum_{m=1}^d \frac{(x_{im} - x_{jm})^2}{\sigma_m^2}} \right) \left( 1 + \sqrt{5 \sum_{m=1}^d \frac{(x_{im} - x_{jm})^2}{\sigma_m^2}} + \frac{5}{3} \sum_{m=1}^d \frac{(x_{im} - x_{jm})^2}{\sigma_m^2} \right)}$$

~ ARD-Matern 5/2 Kernel (8)

$$k(x_i, x_j|\theta) = \sigma_f^2 \left( 1 + \frac{1}{2\alpha} \sum_{m=1}^d \frac{(x_{im} - x_{jm})^2}{\sigma_m^2} \right)^{-\alpha}$$

~ ARD-Rational Quadratic Kernel (9)

$$k(x_i, x_j|\theta) = \sigma_f^2 e^{\left( -\sqrt{3 \sum_{m=1}^d \frac{(x_{im} - x_{jm})^2}{\sigma_m^2}} \right) \left( 1 + \sqrt{3 \sum_{m=1}^d \frac{(x_{im} - x_{jm})^2}{\sigma_m^2}} \right)}$$

~ ARD-Matern 3/2 Kernel (10)

$$B = \text{Empty Matrix} \sim \text{Empty Basis Function} \tag{11}$$

$$B = I_{n \times 1} \sim \text{Constant Basis Function} \tag{12}$$

$$B = [1, X] \sim \text{Linear Basis Function} \tag{13}$$

$$B = [1, X, X^2] \sim \text{Pure Quadratic Basis Function} \tag{14}$$

We use the cross-validation technique as well as the Bayesian optimization utilizing the lower confidence bound (LCB) algorithm in order to make parameter estimations. More technical details can be found in, e.g., [26, 27, 28, 29, 30, 31, 32, 33, 34, 35, 36, 37, 39, 40, 41, 42, 43, 44, 45, 46, 47, 48, 49]. For the cross validation, we employ ten randomized folds (refer to Table 1). For a GPR ( $f(x)$ ), the algorithm will evaluate  $y_i = f(x_i)$  based on  $N_s$  observations ( $x_i$ 's) randomly obtained in variable bounds, where  $N_s$  denotes the point number utilized for the initial evaluation purpose, and, we employ 4. If the evaluation error is determined, the algorithm will take points randomly until it reaches  $N_s$  evaluations that are successful. It will proceed to repeat these following procedures: (a) making updates to  $f(x)$  in order to reach the posterior distribution ( $Q(f|x_i, y_i$  for  $i = 1, \dots, n)$ ); (b) locating the point ( $x$ ), which maximizes  $a(x)$ —the acquisition function. It will stop after it reaches 200 iterations.  $a(x)$  evaluates the goodness of a point based on  $Q$ . The LCB acquisition function is designed to examine  $G$  that is 2 standard deviations (denoted by  $2\sigma_Q$ ) lower than the posterior mean (denoted by  $\mu_Q$ ) for every observation. That is,  $G(x) = \mu_Q(x) - 2\sigma_Q(x)$ . Hence,  $G(x)$  can be seen as representing objective function's lower confidence envelopes of  $2\sigma_Q$ . The algorithm of the LCB aims at maximizing  $2\sigma_Q(x) - \mu_Q(x)$ . We perform Bayesian optimizations across the basis function, the kernel, and  $\sigma$ —the noise standard deviation in order to make minimization of cross-validation errors. Fig. 1 expresses the results. We conduct the likelihood maximization expressed in Equation (15) to make estimations of  $\theta$  and  $\beta$ , where  $K(X, X|\theta)$  is expressed

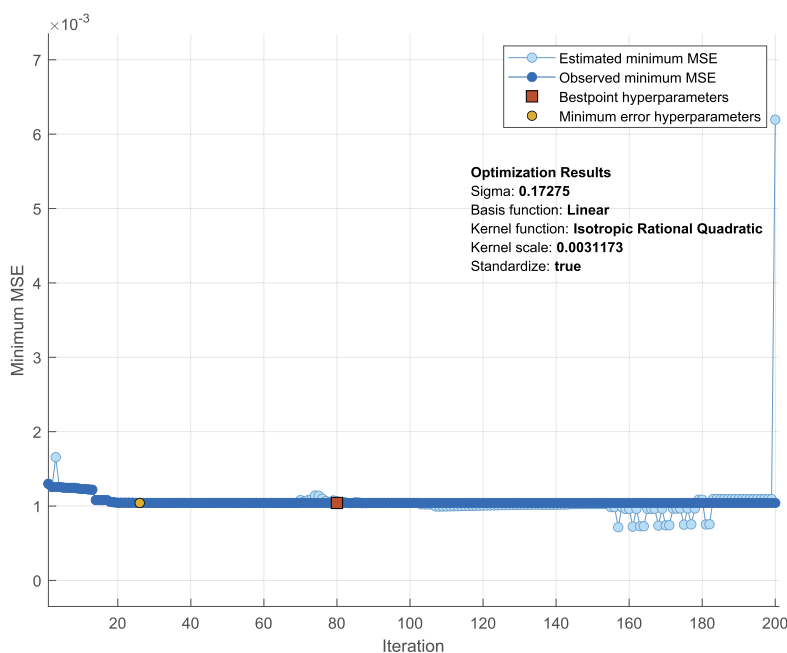


Fig. 1. Bayesian optimization processes.

as  $\begin{pmatrix} k(x_1, x_1) & k(x_1, x_2) & \cdots & k(x_1, x_n) \\ k(x_2, x_1) & k(x_2, x_2) & \cdots & k(x_2, x_n) \\ \vdots & \vdots & \ddots & \vdots \\ k(x_n, x_1) & k(x_n, x_2) & \cdots & k(x_n, x_n) \end{pmatrix}$ . We make assessments of the

model performance using the correlation coefficient (denoted as CC), root mean square error (denoted as RMSE), and mean absolute error (denoted as MAE).

$$\log P(y|X, \beta, \theta, \sigma^2) = -\frac{1}{2} \{(y - B\beta)^T [K(X, X|\theta) + \sigma^2 I_n]^{-1} (y - B\beta)\} - \frac{n}{2} \log 2\pi - \frac{1}{2} \log |K(X, X|\theta) + \sigma^2 I_n| \quad (15)$$

### 3. Dataset

Data analyzed in Table 1 are from [25, 51, 53, 54, 55, 56, 57, 58], which contains fluorides, chlorides, and bromides with cation combinations of  $A^{1+}B^{2+}$ , as well as oxides with cation combinations of  $A^{3+}B^{3+}$ ,  $A^{1+}B^{5+}$ , and  $A^{2+}B^{4+}$ . Descriptors include  $r_A$  ( $\text{\AA}$ )—the  $A$ -site cation's ionic radii,  $r_B$  ( $\text{\AA}$ )—the  $B$ -site cation's ionic radii, and  $r_X$  ( $\text{\AA}$ )—the  $X$ -site anion's ionic radii. Descriptors,  $V_A$ ,  $V_B$ , and  $V_X$ , are the numbers of valence electrons of each ion. The targets are  $a$  ( $\text{\AA}$ )—experimental lattice constants. It should be noted that  $V_X$  is not selected as a predictor in our final model because the value of  $V_X$ , or whether the anion is a halogen or an oxygen, is actually dependent on values of  $V_A$  and  $V_B$ . Fig. 2 plots the data.

## 4. Result

### 4.1. Model specification

As can be seen in Fig. 1, the GPR model is specified through the linear basis function and the isotropic rational quadratic kernel, and, the predictors are standardized. The final GPR model is arrived at according to the following procedures. First, we construct the models GPR.CV  $F_i$  ( $i = 1, 2, \dots, 10$ ), employing samples corresponding to CV  $F_j$ 's ( $j \neq i$ ) listed in Table 1. There, "CV" expresses "cross-validation" and "F" expresses "fold." Second, every GPR.CV  $F_i$  is employ for scoring samples 1–145. Finally, averages of predictions from GPR.CV  $F_i$ 's serve as predictions from the final model. Through this, the final GPR model could cancel out idiosyncratic irregularities across the data's different folds. Detailed model estimates can be seen from Table 2.

### 4.2. Model performance

The final GPR model's performance can be seen from Table 3. Its CC, RMSE, and MAE are, respectively, 99.87%, 0.02104, and 0.01618 for observations 1–145 in Table 1. These results show high accuracy. Table 3 summarizes performance of existing models in the literature, including the log-linear equation [25] and linear regressions [51, 53], where we observe improvements through the GPR model. Fig. 3 visualizes different predictions, where it can be observed that the GPR model generates predictions closest to the perfect prediction line.

For observations 146–149, there are no experimental  $a$  ( $\text{\AA}$ ) values. We apply the final GPR model to obtain their predictions and visualize them with those from [25, 51, 53] in Fig. 4.

One can see that our GPR predictions, generally, lie between those from the log-linear equation [25] and linear regressions [51, 53].

### 4.3. Stability

The sample has the size of 145, and, is relatively small and shows some potential idiosyncratic patterns of irregularities. Estimates of parameters of the models, expressed in Table 2, in this situation are in general stable. Cross-validation results can be seen from Fig. 5, and, performance of the cross-validation can be seen from Table 4. One can observe that the performance is in general stable too. Because of the cross-validation results' general stabilities, we build the final GPR as a model combination. It could cancel out idiosyncratic patterns of irregularities and produce predictions that are more stable, which can be seen from Fig. 3.

## 5. Conclusion

As a data-driven method, we construct a model using the Gaussian process regressions in order to make predictions of the lattice constants of cubic perovskite  $ABX_3$ . The model uses readily-available parameters of constituting elements and presents the statistical relationship among the ionic radii, the valence electrons number, and the lattice constants. The model's stabilities and accuracy are high. Thus, the model has the potential to be a fast tool for robust estimates of the lattice constants. The model applies to various types of  $ABX_3$  perovskites, both oxides

Table 1. Data analyzed and target predictions.

Category	Index	Solids	Predictors						Target: $a$ (Å)					CV Fold
			$r_A$ (Å)	$r_B$ (Å)	$r_X$ (Å)	$V_A$	$V_B$	$V_X$	Exp.	Pred. [53]	Pred. [51]	Pred. [25]	GPR	
A1 + B2 + X3	1	CsCdF <sub>3</sub>	1.880	0.950	1.285	1	2	7	4.470	4.430	4.475	4.262	4.477	CV F4
	2	CsCaF <sub>3</sub>	1.880	1.000	1.285	1	2	7	4.523	4.496	4.539	4.313	4.547	CV F10
	3	CsHgF <sub>3</sub>	1.880	1.020	1.285	1	2	7	4.570	4.523	4.565	4.334	4.582	CV F3
	4	CsSrF <sub>3</sub>	1.880	1.180	1.285	1	2	7	4.750	4.747	4.781	4.500	4.786	CV F1
	5	CsEuF <sub>3</sub>	1.880	1.170	1.285	1	2	7	4.780	4.729	4.767	4.489	4.774	CV F3
	6	CsPbF <sub>3</sub>	1.880	1.190	1.285	1	2	7	4.800	4.575	4.795	4.510	4.801	CV F5
	7	CsYbF <sub>3</sub>	1.880	1.020	1.285	1	2	7	4.610	4.523	4.565	4.334	4.582	CV F3
	8	CsCaCl <sub>3</sub>	1.880	1.000	1.790	1	2	7	5.396	5.360	5.391	4.836	5.381	CV F2
	9	CsCdCl <sub>3</sub>	1.880	0.950	1.790	1	2	7	5.210	5.289	5.321	4.785	5.257	CV F10
	10	CsPbCl <sub>3</sub>	1.880	1.190	1.790	1	2	7	5.605	5.639	5.667	5.033	5.628	CV F3
	11	CsHgCl <sub>3</sub>	1.880	1.020	1.790	1	2	7	5.410	5.389	5.420	4.857	5.425	CV F8
	12	CsEuCl <sub>3</sub>	1.880	1.170	1.790	1	2	7	5.627	5.610	5.637	5.012	5.605	CV F6
	13	CsTmCl <sub>3</sub>	1.880	1.030	1.790	1	2	7	5.476	5.404	5.406	4.867	5.442	CV F7
	14	CsYbCl <sub>3</sub>	1.880	1.020	1.790	1	2	7	5.437	5.389	5.420	4.857	5.425	CV F2
	15	CsPbBr <sub>3</sub>	1.880	1.190	1.950	1	2	7	5.874	5.921	5.941	5.199	5.879	CV F6
	16	RbZnF <sub>3</sub>	1.720	0.740	1.285	1	2	7	4.122	4.102	4.143	3.878	4.120	CV F4
	17	RbCoF <sub>3</sub>	1.720	0.745	1.285	1	2	7	4.141	4.108	4.143	3.884	4.128	CV F7
	18	RbVF <sub>3</sub>	1.720	0.790	1.285	1	2	7	4.170	4.165	4.203	3.930	4.187	CV F7
	19	RbFeF <sub>3</sub>	1.720	0.780	1.285	1	2	7	4.174	4.152	4.191	3.920	4.174	CV F9
	20	RbMnF <sub>3</sub>	1.720	0.830	1.285	1	2	7	4.240	4.215	4.252	3.972	4.246	CV F7
	21	RbCdF <sub>3</sub>	1.720	0.950	1.285	1	2	7	4.398	4.373	4.405	4.096	4.398	CV F1
	22	RbCaF <sub>3</sub>	1.720	1.000	1.285	1	2	7	4.452	4.440	4.471	4.148	4.463	CV F6
	23	RbHgF <sub>3</sub>	1.720	1.020	1.285	1	2	7	4.470	4.468	4.498	4.168	4.493	CV F10
	24	RbPdF <sub>3</sub>	1.720	0.860	1.285	1	2	7	4.298	4.254	4.290	4.003	4.292	CV F6
	25	RbYbF <sub>3</sub>	1.720	1.020	1.285	1	2	7	4.530	4.468	4.498	4.168	4.493	CV F2
	26	RbPbF <sub>3</sub>	1.720	1.190	1.285	1	2	7	4.790	4.705	4.732	4.344	4.759	CV F2
	27	KCaF <sub>3</sub>	1.640	1.000	1.285	1	2	7	4.380	–	–	4.065	4.391	CV F5
	28	KCdF <sub>3</sub>	1.640	0.950	1.285	1	2	7	4.293	4.344	4.341	4.013	4.319	CV F6
	29	KMgF <sub>3</sub>	1.640	0.720	1.285	1	2	7	3.989	4.046	4.048	3.775	4.020	CV F1
	30	KNiF <sub>3</sub>	1.640	0.690	1.285	1	2	7	4.013	4.009	4.012	3.744	3.984	CV F4
	31	KZnF <sub>3</sub>	1.640	0.740	1.285	1	2	7	4.056	4.070	4.072	3.796	4.045	CV F6
	32	KCoF <sub>3</sub>	1.640	0.745	1.285	1	2	7	4.071	4.077	4.072	3.801	4.052	CV F8
33	KVF <sub>3</sub>	1.640	0.790	1.285	1	2	7	4.100	4.134	4.134	3.847	4.117	CV F1	
34	KFeF <sub>3</sub>	1.640	0.780	1.285	1	2	7	4.121	4.121	4.121	3.837	4.102	CV F4	
35	KMnF <sub>3</sub>	1.640	0.830	1.285	1	2	7	4.189	4.185	4.184	3.889	4.184	CV F5	
36	NaVF <sub>3</sub>	1.390	0.790	1.285	1	2	7	3.940	4.037	3.955	3.588	3.947	CV F9	
37	NaMgF <sub>3</sub>	1.390	0.720	1.285	1	2	7	3.840	–	–	3.516	3.853	CV F3	
38	NaZnF <sub>3</sub>	1.390	0.740	1.285	1	2	7	3.880	–	–	3.537	3.882	CV F3	
39	NaCoF <sub>3</sub>	1.390	0.745	1.285	1	2	7	3.900	–	–	3.542	3.889	CV F1	
40	AgMgF <sub>3</sub>	1.480	0.720	1.285	1	2	7	3.918	3.982	3.930	3.609	3.938	CV F10	
41	AgNiF <sub>3</sub>	1.480	0.690	1.285	1	2	7	3.936	3.944	3.892	3.578	3.898	CV F8	
42	AgZnF <sub>3</sub>	1.480	0.740	1.285	1	2	7	3.972	4.004	3.955	3.630	3.961	CV F5	
43	AgCoF <sub>3</sub>	1.480	0.745	1.285	1	2	7	3.983	4.013	3.955	3.635	3.967	CV F2	
44	AgMnF <sub>3</sub>	1.480	0.830	1.285	1	2	7	4.030	4.124	4.072	3.723	4.049	CV F4	
45	LiBaF <sub>3</sub>	1.610	0.760	1.285	1	2	7	3.992	4.084	3.984	3.785	4.033	CV F8	
46	NH <sub>4</sub> ZnF <sub>3</sub>	1.800	0.740	1.285	1	2	7	4.115	4.134	4.128	3.961	4.119	CV F7	
47	NH <sub>4</sub> CoF <sub>3</sub>	1.800	0.745	1.285	1	2	7	4.129	4.140	4.128	3.966	4.127	CV F4	
48	NH <sub>4</sub> FeF <sub>3</sub>	1.800	0.780	1.285	1	2	7	4.177	4.183	4.176	4.003	4.182	CV F9	
49	NH <sub>4</sub> MnF <sub>3</sub>	1.800	0.830	1.285	1	2	7	4.241	4.246	4.238	4.054	4.256	CV F1	
50	NH <sub>4</sub> MgF <sub>3</sub>	1.800	0.720	1.285	1	2	7	4.060	4.110	4.104	3.940	4.088	CV F9	
51	TiCoF <sub>3</sub>	1.700	0.745	1.285	1	2	7	4.138	4.100	4.133	3.863	4.121	CV F7	
52	TiFeF <sub>3</sub>	1.700	0.780	1.285	1	2	7	4.188	4.144	4.181	3.899	4.168	CV F4	
53	TiMnF <sub>3</sub>	1.700	0.830	1.285	1	2	7	4.260	4.208	4.243	3.951	4.240	CV F2	
54	TiCdF <sub>3</sub>	1.700	0.950	1.285	1	2	7	4.400	4.366	4.396	4.075	4.381	CV F10	
55	TiPdF <sub>3</sub>	1.700	0.860	1.285	1	2	7	4.301	4.247	4.280	3.982	4.284	CV F3	
56	TiMnCl <sub>3</sub>	1.700	0.830	1.790	1	2	7	5.020	5.064	5.087	4.474	5.013	CV F9	
A1 + B5 + O3	57	CsIO <sub>3</sub>	1.880	0.950	1.350	1	5	6	4.674	4.539	4.596	4.636	4.667	CV F9
	58	RbUO <sub>3</sub>	1.720	0.760	1.350	1	5	6	4.323	4.234	4.286	4.248	4.319	CV F6
	59	KUO <sub>3</sub>	1.640	0.760	1.350	1	5	6	4.290	4.203	4.218	4.159	4.280	CV F8
	60	RbPaO <sub>3</sub>	1.720	0.780	1.350	1	5	6	4.368	4.259	4.311	4.270	4.350	CV F2
	61	KPaO <sub>3</sub>	1.640	0.780	1.350	1	5	6	4.341	4.229	4.243	4.181	4.311	CV F2
	62	KTaO <sub>3</sub>	1.640	0.640	1.350	1	5	6	3.988	4.053	4.072	4.026	4.020	CV F1
	63	KNbO <sub>3</sub>	1.640	0.640	1.350	1	5	6	4.007	4.053	4.072	4.026	4.020	CV F8
	64	NaTaO <sub>3</sub>	1.390	0.640	1.350	1	5	6	3.881	3.952	3.886	3.749	3.889	CV F2
	65	NaAlO <sub>3</sub>	1.390	0.535	1.350	1	5	6	3.730	3.823	3.762	3.632	3.744	CV F9
	66	NaWO <sub>3</sub>	1.390	0.620	1.350	1	5	6	3.850	3.927	3.861	3.727	3.860	CV F1
A2 + B4 + O3	67	BaFeO <sub>3</sub>	1.610	0.585	1.350	2	4	6	3.994	3.975	3.998	4.102	3.995	CV F5
	68	BaMoO <sub>3</sub>	1.610	0.650	1.350	2	4	6	4.040	4.053	4.068	4.177	4.062	CV F7
	69	BaNbO <sub>3</sub>	1.610	0.680	1.350	2	4	6	4.080	4.091	4.104	4.212	4.092	CV F7
	70	BaSnO <sub>3</sub>	1.610	0.690	1.350	2	4	6	4.116	4.103	4.117	4.223	4.111	CV F4
	71	BaHfO <sub>3</sub>	1.610	0.710	1.350	2	4	6	4.171	4.128	4.141	4.246	4.158	CV F5
	72	BaZrO <sub>3</sub>	1.610	0.720	1.350	2	4	6	4.193	4.141	4.154	4.258	4.183	CV F5
	73	BaIrO <sub>3</sub>	1.610	0.625	1.350	2	4	6	4.100	4.023	4.045	4.148	4.048	CV F4
	74	BaPbO <sub>3</sub>	1.610	0.775	1.350	2	4	6	4.265	4.211	4.229	4.322	4.275	CV F8

Table 1 (continued)

Category	Index	Solids	Predictors						Target: $a$ (Å)					CV Fold
			$r_A$ (Å)	$r_B$ (Å)	$r_X$ (Å)	$V_A$	$V_B$	$V_X$	Exp.	Pred. [53]	Pred. [51]	Pred. [25]	GPR	
	75	BaTbO <sub>3</sub>	1.610	0.760	1.350	2	4	6	4.285	4.192	4.204	4.304	4.258	CV F9
	76	BaPrO <sub>3</sub>	1.610	0.850	1.350	2	4	6	4.354	4.310	4.319	4.408	4.356	CV F8
	77	BaCeO <sub>3</sub>	1.610	0.870	1.350	2	4	6	4.397	4.336	4.346	4.432	4.384	CV F5
	78	BaAmO <sub>3</sub>	1.610	0.850	1.350	2	4	6	4.357	4.310	4.319	4.408	4.356	CV F10
	79	BaNpO <sub>3</sub>	1.610	0.870	1.350	2	4	6	4.384	4.336	4.346	4.432	4.384	CV F1
	80	BaUO <sub>3</sub>	1.610	0.890	1.350	2	4	6	4.387	4.363	4.372	4.455	4.413	CV F8
	81	BaPaO <sub>3</sub>	1.610	0.900	1.350	2	4	6	4.450	4.377	4.386	4.466	4.428	CV F9
	82	BaThO <sub>3</sub>	1.610	0.940	1.350	2	4	6	4.480	4.431	4.439	4.513	4.486	CV F4
	83	BaTiO <sub>3</sub>	1.610	0.605	1.350	2	4	6	4.012	3.999	4.021	4.125	4.026	CV F10
	84	BaRuO <sub>3</sub>	1.610	0.680	1.350	2	4	6	4.050	–	–	4.212	4.092	CV F7
	85	BaPuO <sub>3</sub>	1.610	0.860	1.350	2	4	6	4.360	–	–	4.420	4.370	CV F10
	86	SrMnO <sub>3</sub>	1.440	0.530	1.350	2	4	6	3.806	3.838	3.837	3.841	3.817	CV F3
	87	SrVO <sub>3</sub>	1.440	0.580	1.350	2	4	6	3.890	3.898	3.932	3.899	3.872	CV F6
	88	SrFeO <sub>3</sub>	1.440	0.585	1.350	2	4	6	3.850	3.904	3.908	3.905	3.878	CV F9
	89	SrTiO <sub>3</sub>	1.440	0.605	1.350	2	4	6	3.905	3.929	3.932	3.928	3.902	CV F9
	90	SrTcO <sub>3</sub>	1.440	0.645	1.350	2	4	6	3.949	3.979	3.981	3.975	3.950	CV F4
	91	SrMoO <sub>3</sub>	1.440	0.650	1.350	2	4	6	3.975	3.985	3.981	3.980	3.956	CV F10
	92	SrNbO <sub>3</sub>	1.440	0.680	1.350	2	4	6	4.016	4.023	4.018	4.015	3.999	CV F2
	93	SrSnO <sub>3</sub>	1.440	0.690	1.350	2	4	6	4.034	4.036	4.031	4.027	4.018	CV F6
	94	SrHfO <sub>3</sub>	1.440	0.710	1.350	2	4	6	4.069	4.062	4.056	4.050	4.063	CV F3
	95	SrTbO <sub>3</sub>	1.440	0.760	1.350	2	4	6	4.180	4.127	4.121	4.108	4.156	CV F10
	96	SrAmO <sub>3</sub>	1.440	0.850	1.350	2	4	6	4.230	4.248	4.240	4.212	4.250	CV F8
	97	SrPuO <sub>3</sub>	1.440	0.860	1.350	2	4	6	4.280	4.261	4.253	4.223	4.265	CV F5
	98	SrCoO <sub>3</sub>	1.440	0.530	1.350	2	4	6	3.850	3.838	3.837	3.841	3.817	CV F2
	99	SrZrO <sub>3</sub>	1.440	0.720	1.350	2	4	6	4.104	4.075	4.069	4.061	4.086	CV F10
	100	SrRuO <sub>3</sub>	1.440	0.680	1.350	2	4	6	3.930	3.927	–	4.015	3.999	CV F8
	101	SrThO <sub>3</sub>	1.440	0.940	1.350	2	4	6	4.420	–	–	4.316	4.399	CV F1
	102	CaVO <sub>3</sub>	1.340	0.580	1.350	2	4	6	3.767	3.857	3.838	3.784	3.790	CV F2
	103	CaHfO <sub>3</sub>	1.340	0.710	1.350	2	4	6	3.990	–	–	3.934	3.977	CV F9
	104	CaZrO <sub>3</sub>	1.340	0.720	1.350	2	4	6	4.010	–	–	3.946	4.000	CV F1
	105	CaRuO <sub>3</sub>	1.340	0.680	1.350	2	4	6	3.840	–	–	3.899	3.911	CV F8
	106	CaSnO <sub>3</sub>	1.340	0.690	1.350	2	4	6	3.950	–	–	3.911	3.931	CV F7
	107	CaTiO <sub>3</sub>	1.340	0.605	1.350	2	4	6	3.840	3.888	3.838	3.813	3.825	CV F4
A3 + B3 + O3	108	EuTiO <sub>3</sub>	1.230	0.670	1.350	3	3	6	3.905	3.927	3.889	3.801	3.877	CV F5
	109	EuAlO <sub>3</sub>	1.230	0.535	1.350	3	3	6	3.725	3.755	3.724	3.643	3.718	CV F5
	110	EuCrO <sub>3</sub>	1.230	0.615	1.350	3	3	6	3.803	3.856	3.824	3.736	3.809	CV F10
	111	EuFeO <sub>3</sub>	1.230	0.645	1.350	3	3	6	3.836	3.894	3.856	3.771	3.841	CV F3
	112	EuGaO <sub>3</sub>	1.230	0.620	1.350	3	3	6	3.840	–	–	3.742	3.814	CV F5
	113	EuInO <sub>3</sub>	1.230	0.800	1.350	3	3	6	4.030	–	–	3.593	4.044	CV F1
	114	CeAlO <sub>3</sub>	1.340	0.535	1.350	3	3	6	3.772	3.801	3.757	3.771	3.769	CV F6
	115	GdAlO <sub>3</sub>	1.220	0.535	1.350	3	3	6	3.710	3.750	3.719	3.631	3.708	CV F4
	116	GdCrO <sub>3</sub>	1.220	0.615	1.350	3	3	6	3.795	3.852	3.819	3.725	3.799	CV F2
	117	GdFeO <sub>3</sub>	1.220	0.645	1.350	3	3	6	3.820	3.890	3.851	3.760	3.833	CV F6
	118	LaAlO <sub>3</sub>	1.360	0.535	1.350	3	3	6	3.778	3.810	3.768	3.795	3.777	CV F7
	119	LaCrO <sub>3</sub>	1.360	0.615	1.350	3	3	6	3.874	3.909	3.866	3.888	3.877	CV F7
	120	LaFeO <sub>3</sub>	1.360	0.645	1.350	3	3	6	3.920	3.947	3.898	3.923	3.910	CV F3
	121	LaGaO <sub>3</sub>	1.360	0.620	1.350	3	3	6	3.874	3.915	3.866	3.894	3.883	CV F2
	122	LaRhO <sub>3</sub>	1.360	0.665	1.350	3	3	6	3.940	3.972	3.930	3.947	3.935	CV F4
	123	LaTiO <sub>3</sub>	1.360	0.670	1.350	3	3	6	3.920	3.979	3.930	3.953	3.942	CV F2
	124	LaVO <sub>3</sub>	1.360	0.640	1.350	3	3	6	3.910	3.940	3.891	3.917	3.905	CV F7
	125	LaInO <sub>3</sub>	1.360	0.800	1.350	3	3	6	4.110	–	–	4.105	4.128	CV F8
	126	NdAlO <sub>3</sub>	1.270	0.535	1.350	3	3	6	3.752	3.772	3.740	3.689	3.748	CV F6
	127	NdGaO <sub>3</sub>	1.270	0.620	1.350	3	3	6	3.860	–	–	3.789	3.842	CV F3
	128	NdInO <sub>3</sub>	1.270	0.800	1.350	3	3	6	4.070	–	–	3.999	4.071	CV F3
	129	NdCoO <sub>3</sub>	1.270	0.545	1.350	3	3	6	3.777	3.784	3.753	3.701	3.764	CV F5
	130	NdCrO <sub>3</sub>	1.270	0.615	1.350	3	3	6	3.835	3.872	3.840	3.783	3.838	CV F5
	131	NdFeO <sub>3</sub>	1.270	0.645	1.350	3	3	6	3.870	3.910	3.872	3.818	3.861	CV F9
	132	NdMnO <sub>3</sub>	1.270	0.645	1.350	3	3	6	3.800	3.910	3.872	3.818	3.861	CV F6
	133	PrAlO <sub>3</sub>	1.300	0.535	1.350	3	3	6	3.757	3.784	3.746	3.725	3.758	CV F6
	134	PrCrO <sub>3</sub>	1.300	0.615	1.350	3	3	6	3.852	3.884	3.845	3.818	3.849	CV F5
	135	PrFeO <sub>3</sub>	1.300	0.645	1.350	3	3	6	3.887	3.923	3.877	3.853	3.871	CV F6
	136	PrGaO <sub>3</sub>	1.300	0.620	1.350	3	3	6	3.863	3.891	3.845	3.824	3.853	CV F10
	137	PrMnO <sub>3</sub>	1.300	0.645	1.350	3	3	6	3.820	3.923	3.877	3.853	3.871	CV F4
	138	PrVO <sub>3</sub>	1.300	0.640	1.350	3	3	6	3.890	3.916	3.871	3.847	3.867	CV F10
	139	SmAlO <sub>3</sub>	1.240	0.535	1.350	3	3	6	3.734	3.759	3.729	3.654	3.727	CV F7
	140	SmCoO <sub>3</sub>	1.240	0.545	1.350	3	3	6	3.750	3.771	3.742	3.666	3.743	CV F1
	141	SmVO <sub>3</sub>	1.240	0.640	1.350	3	3	6	3.890	3.892	3.855	3.777	3.843	CV F8
	142	SmFeO <sub>3</sub>	1.240	0.645	1.350	3	3	6	3.845	3.898	3.861	3.783	3.848	CV F3
	143	YAlO <sub>3</sub>	1.200	0.535	1.350	3	3	6	3.680	3.742	3.697	3.608	3.685	CV F1
	144	YCrO <sub>3</sub>	1.200	0.615	1.350	3	3	6	3.768	3.843	3.798	3.701	3.777	CV F3
	145	YFeO <sub>3</sub>	1.200	0.645	1.350	3	3	6	3.785	3.882	3.831	3.736	3.815	CV F9
	146	BiAlO <sub>3</sub>	1.030	0.535	1.350	3	3	6	–	3.723	3.715	3.409	3.556	–
	147	BiGaO <sub>3</sub>	1.030	0.620	1.350	3	3	6	–	3.834	3.821	3.508	3.677	–
	148	BiInO <sub>3</sub>	1.030	0.800	1.350	3	3	6	–	4.111	4.193	3.719	3.932	–
	149	BiScO <sub>3</sub>	1.030	0.745	1.350	3	3	6	–	4.080	3.974	3.654	3.854	–

(continued on next page)



Table 1 (continued)

Category	Index	Solids	Predictors				Target: $a$ ( $\text{\AA}$ )					CV Fold		
			$r_A$ ( $\text{\AA}$ )	$r_B$ ( $\text{\AA}$ )	$r_X$ ( $\text{\AA}$ )	$V_A$	$V_B$	$V_X$	Exp.	Pred. [53]	Pred. [51]		Pred. [25]	GPR
Minimum			1.030	0.530	1.285	1	2	6	3.680	3.723	3.697	3.409	3.556	–
Mean			1.517	0.755	1.357	1.839	3.034	6.376	4.164	4.176	4.175	4.015	4.153	–
Median			1.480	0.720	1.350	2	3	6	4.050	4.077	4.072	3.940	4.045	–
Std.			0.222	0.163	0.119	0.839	0.962	0.486	0.420	0.413	0.435	0.337	0.420	–
Maximum			1.880	1.190	1.950	3	5	7	5.874	5.921	5.941	5.199	5.879	–
CC w. Exp. $a$ (A)			77.56%	87.05%	70.59%	-53.42%	-29.67%	49.89%	–	99.31%	99.67%	91.18%	99.87%	–

Notes: It should be noted that  $V_X$  is not selected as a predictor in our final model because the value of  $V_X$ , or whether the anion is a halogen or an oxygen, is actually dependent on values of  $V_A$  and  $V_B$ . There are no experimental  $a$  ( $\text{\AA}$ ) values for observations 146–149. For these four samples, their GPR predictions are obtained by applying the final GPR model. Predictions in [25] are based on the log-linear equation and those in [51] and [53] are based on linear regressions.

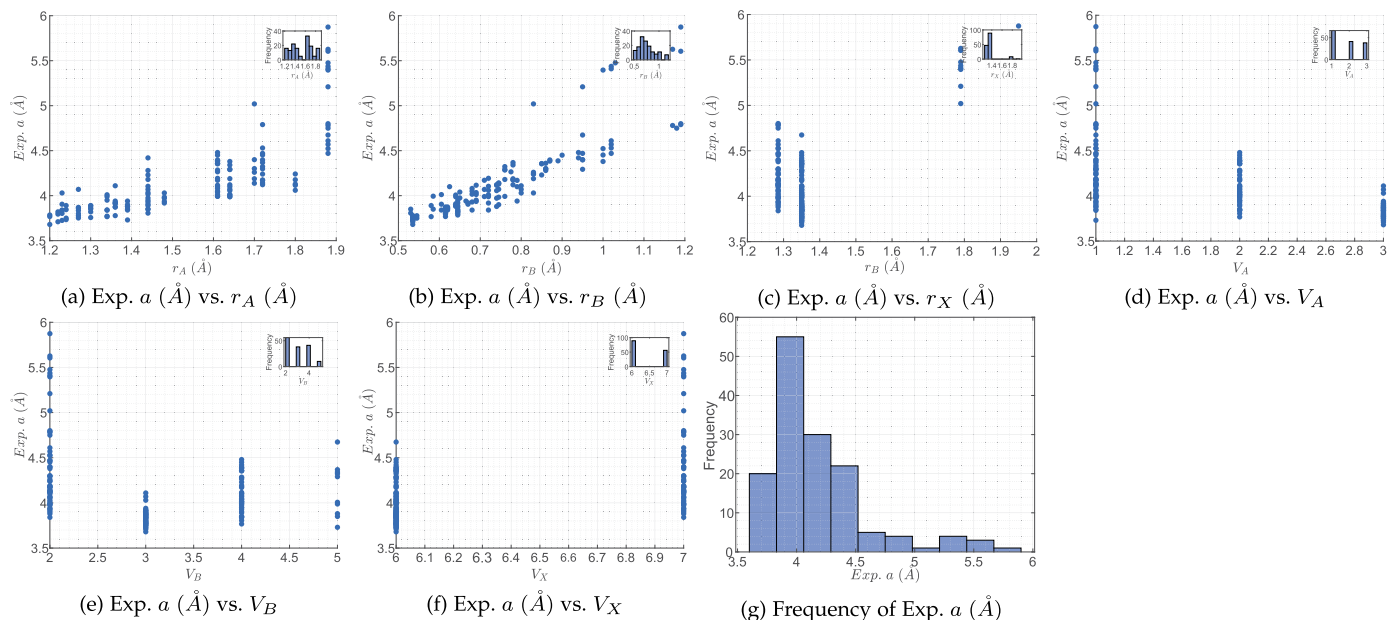


Fig. 2. Data plots. It should be noted that  $V_X$  is not selected as a predictor in our final model because the value of  $V_X$ , or whether the anion is a halogen or an oxygen, is actually dependent on values of  $V_A$  and  $V_B$ . (a) Exp.  $a$  ( $\text{\AA}$ ) vs.  $r_A$  ( $\text{\AA}$ ). (b) Exp.  $a$  ( $\text{\AA}$ ) vs.  $r_B$  ( $\text{\AA}$ ). (c) Exp.  $a$  ( $\text{\AA}$ ) vs.  $r_X$  ( $\text{\AA}$ ). (d) Exp.  $a$  ( $\text{\AA}$ ) vs.  $V_A$ . (e) Exp.  $a$  ( $\text{\AA}$ ) vs.  $V_B$ . (f) Exp.  $a$  ( $\text{\AA}$ ) vs.  $V_X$ . (g) Frequency of Exp.  $a$  ( $\text{\AA}$ ).

Table 2. Estimates of parameters.

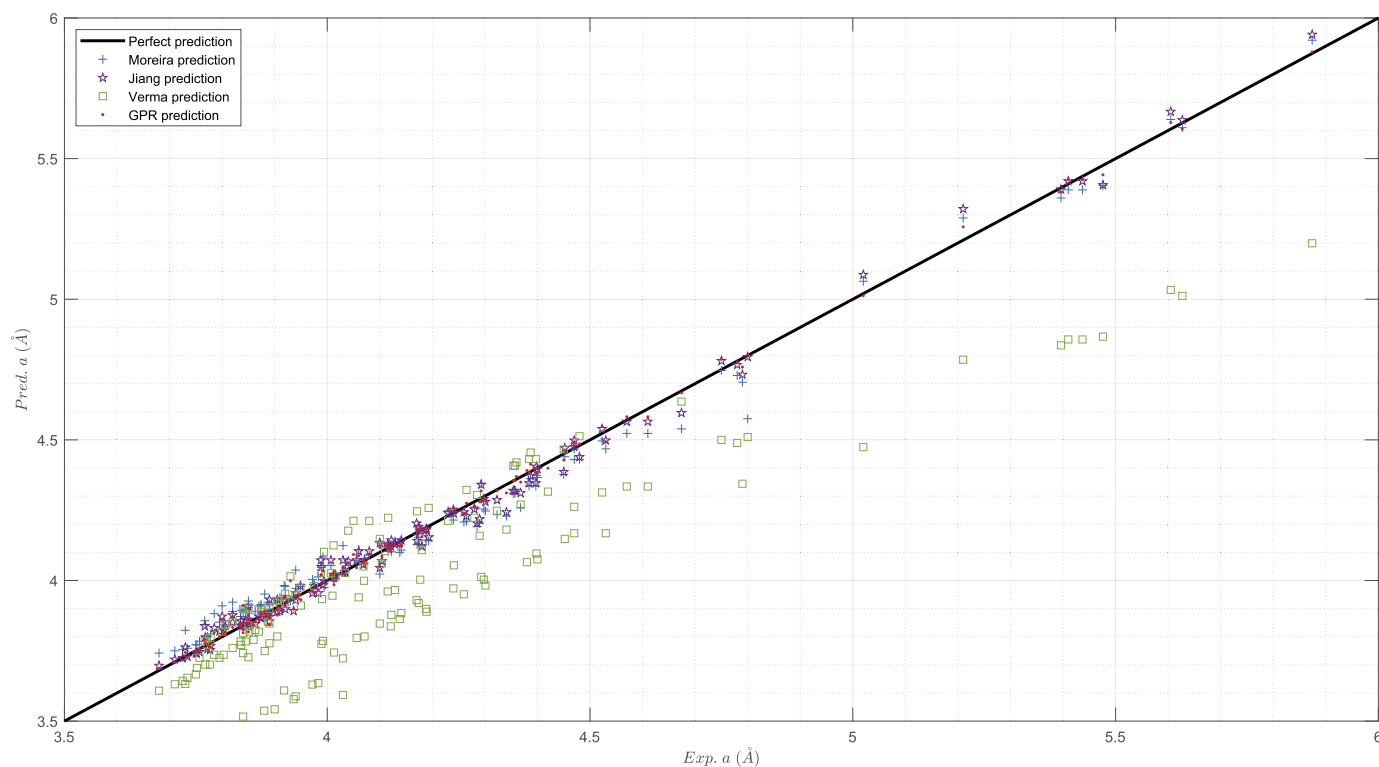
Model	Estimates of parameters										
	$\sigma$	$\beta_0$	$\beta_1$	$\beta_2$	$\beta_3$	$\beta_4$	$\beta_5$	$\sigma_l$	$\alpha$	$\sigma_f$	
Final GPR	GPR.CV F1	0.02548	4.16780	0.13684	0.22871	0.19869	0.02980	0.02068	0.23885	108326.10226	0.02496
	GPR.CV F2	0.02478	4.14943	0.13558	0.22257	0.18297	0.03199	0.01941	0.21371	81074.94010	0.02399
	GPR.CV F3	0.02559	4.15884	0.12722	0.22463	0.19245	0.02843	0.02228	0.26238	140011.28617	0.02736
	GPR.CV F4	0.02355	4.17089	0.13194	0.24320	0.19944	0.02956	0.02300	0.26913	236298.46045	0.02895
	GPR.CV F5	0.02582	4.17061	0.13415	0.23007	0.20057	0.02883	0.02206	0.25052	116079.78874	0.02662
	GPR.CV F6	0.02370	4.15284	0.13151	0.22344	0.17144	0.02896	0.02164	0.22335	63863.24868	0.02816
	GPR.CV F7	0.02534	4.16622	0.13642	0.23617	0.18963	0.03169	0.02280	0.27054	106792.36532	0.02585
	GPR.CV F8	0.02031	4.15864	0.13641	0.24320	0.19050	0.03384	0.02360	0.22511	142151.00534	0.02741
	GPR.CV F9	0.02483	4.16451	0.13185	0.23646	0.19044	0.02771	0.02033	0.23470	133097.23475	0.02710
	GPR.CV F10	0.02432	4.15616	0.13859	0.23156	0.19327	0.03080	0.01997	0.23543	97684.60661	0.02597

Notes:  $\beta_0$ ,  $\beta_1$ ,  $\beta_2$ ,  $\beta_3$ ,  $\beta_4$ , and  $\beta_5$  correspond to the intercept,  $r_A$  ( $\text{\AA}$ ),  $r_B$  ( $\text{\AA}$ ),  $r_X$  ( $\text{\AA}$ ),  $V_A$ , and  $V_B$ , respectively.

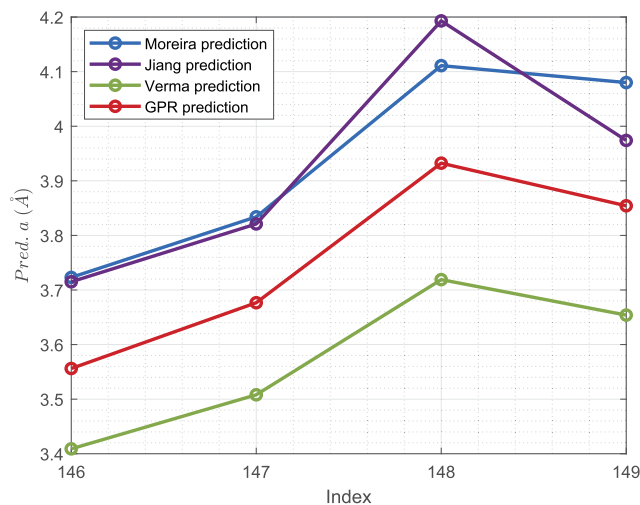
Table 3. Model performance.

	CC	RMSE	RMSE Sample Mean	MAE	MAE Sample Mean
Pred. [53]	99.31%	0.05476	1.31%	0.04367	1.04%
Pred. [51]	99.67%	0.03541	0.85%	0.02655	0.63%
Pred. [25]	91.18%	0.22609	5.43%	0.16345	3.92%
GPR	99.87%	0.02104	0.51%	0.01618	0.39%

Notes: Results are based on observations 1–145 in Table 1.



**Fig. 3.** Experimental lattice constants vs. predicted lattice constants. “Moreira prediction” [53] and “Jiang prediction” [51] are based on linear regression models. “Verma prediction” [25] is based on the log-linear equation. “GPR prediction” shows our result. Results are based on observations 1–145 in Table 1.



**Fig. 4.** Predictions of lattice constants. “Moreira prediction” [53] and “Jiang prediction” [51] are based on linear regression models. “Verma prediction” [25] is based on the log-linear equation. “GPR prediction” shows our result. Results are based on observations 146–149 in Table 1.

and halides. Particularly, by incorporating the number of valence electrons into the descriptor set, the model is able to distinguish the same ion with different structural surroundings based on valence, which enhances the predictive power of the model. Compared with many other machine learning methods, the GPR model here is simple and straightforward, without the need of a large number of inputs.

#### Declarations

#### Author contribution statement

Yun Zhang: Conceived and designed the experiments; Performed the experiments; Analyzed and interpreted the data; Wrote the paper.

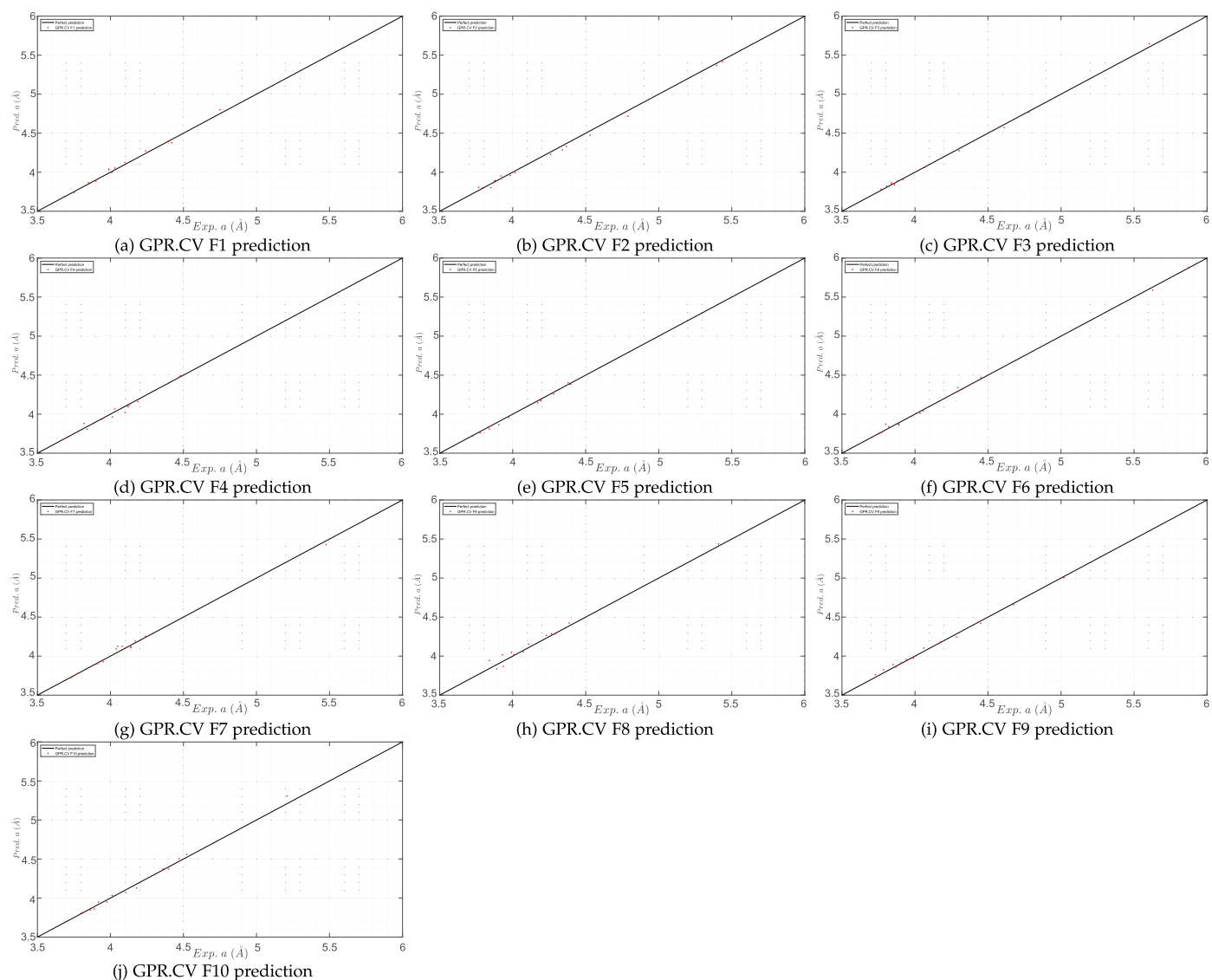
Xiaojie Xu: Performed the experiments; Analyzed and interpreted the data; Contributed reagents, materials, analysis tools or data; Wrote the paper.

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#### Data availability statement

Data included in article/supplementary material/referenced in article.



**Fig. 5.** Cross validation performance. (a) GPR.CV F1 prediction. (b) GPR.CV F2 prediction. (c) GPR.CV F3 prediction. (d) GPR.CV F4 prediction. (e) GPR.CV F5 prediction. (f) GPR.CV F6 prediction. (g) GPR.CV F7 prediction. (h) GPR.CV F8 prediction. (i) GPR.CV F9 prediction. (j) GPR.CV F10 prediction.

**Table 4.** Performance of the cross-validation.

	CC		RMSE				MAE			
	Training	Validation	Training	% of Training Sample Mean	Validation	% of Validation Sample Mean	Training	% of Training Sample Mean	Validation	% of Validation Sample Mean
CV F1	99.88%	99.58%	0.021	0.51%	0.029	0.71%	0.016	0.39%	0.024	0.57%
CV F2	99.87%	99.85%	0.021	0.50%	0.038	0.88%	0.015	0.37%	0.033	0.77%
CV F3	99.87%	99.93%	0.021	0.51%	0.019	0.46%	0.016	0.39%	0.015	0.36%
CV F4	99.90%	98.79%	0.019	0.46%	0.033	0.82%	0.015	0.35%	0.024	0.59%
CV F5	99.87%	99.88%	0.022	0.52%	0.019	0.48%	0.017	0.40%	0.016	0.38%
CV F6	99.88%	99.91%	0.019	0.46%	0.027	0.64%	0.015	0.36%	0.020	0.47%
CV F7	99.87%	99.70%	0.021	0.51%	0.033	0.79%	0.016	0.40%	0.025	0.61%
CV F8	99.93%	99.28%	0.016	0.39%	0.049	1.18%	0.012	0.29%	0.040	0.96%
CV F9	99.88%	99.81%	0.021	0.49%	0.026	0.64%	0.016	0.38%	0.023	0.54%
CV F10	99.89%	99.73%	0.020	0.48%	0.038	0.89%	0.016	0.37%	0.030	0.71%
Minimum	99.87%	98.79%	0.016	0.39%	0.019	0.46%	0.012	0.29%	0.015	0.36%
Mean	99.88%	99.65%	0.020	0.48%	0.031	0.75%	0.015	0.37%	0.025	0.60%
Median	99.88%	99.77%	0.021	0.50%	0.031	0.75%	0.016	0.38%	0.024	0.58%
Maximum	99.93%	99.93%	0.022	0.52%	0.049	1.18%	0.017	0.40%	0.040	0.96%
Std	0.02%	0.36%	0.002	0.04%	0.009	0.21%	0.001	0.03%	0.008	0.18%

**Declaration of interests statement**

The authors declare no conflict of interest.

**Additional information**

No additional information is available for this paper.



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