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# Ti/Ti<sub>4</sub>O<sub>7</sub> Anodes for Efficient Electrodeposition of Manganese Metal and Anode Slime Generation Reduction

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 ABSTRACT: Preventing lead-based anodes from causing high Image: Supporting Information

**ABSTRACT:** Preventing lead-based anodes from causing highenergy consumption, lead pollution, and harmful anode slime emission is a major challenge for the current electrolytic manganese metal industry. In this work, a Ti<sub>4</sub>O<sub>7</sub>-coated titanium electrode was used as anode material (Ti/Ti<sub>4</sub>O<sub>7</sub> anode) in manganese electrowinning process for the first time and compared with a lead-based anode (Pb anode). The Ti/Ti<sub>4</sub>O<sub>7</sub> anode was used for galvanostatic electrolysis; the cathodic current efficiency improved by 3.22% and energy consumption decreased by 7.82%. During 8 h of electrolysis, it reduced 90.42% solution anode slime and 72.80% plate anode slime formation. Anode product characterization and electrochemical tests indicated that the Ti/Ti<sub>4</sub>O<sub>7</sub> anode possesses good oxygen evolution activity, and  $\gamma$ -MnO<sub>2</sub> has a positive catalytic



effect on oxygen evolution reaction (OER), which inhibited anode  $Mn^{2+}$  oxidation reaction and reduced the formation of anode slime. In addition, the low charge-transfer resistance, high diffusion resistance, and dense  $MnO_2$  layer of the anode blocked the diffusion path of  $Mn^{3+}$  in the system and inhibited the formation of anode slime. The Ti/Ti<sub>4</sub>O<sub>7</sub> anode exhibits excellent electrochemical performance, which provides a new idea for the selection of novel anodes, energy savings and emission reduction, and the establishment of a new mode of clean production in the electrolytic manganese metal industry.

## 1. INTRODUCTION

Manganese is an important material. It is widely used in iron and steel smelting, nonferrous metallurgy, and new energy and other industries.<sup>1–3</sup> At present, metal manganese is produced by electrolysis in industry. In the process of electrodeposition of metal manganese, the electrode reactions on the cathode and anode are as follows

Cathode:

$$Mn^{2+} + 2e^- = Mn \quad E^{\Theta} = -1.18V$$
 (1)

$$2H_2O + 2e^- = H_2 \uparrow + 2OH^- \quad E^\Theta = 0V \tag{2}$$

Anode:

$$2H_2O = O_2 \uparrow +4H^+ + 4e^- E^\Theta = 1.229V$$
 (3)

$$Mn^{2+} + 2H_2O = MnO_2 \downarrow + 4H^+ + 2e^- E^\Theta = 1.223V$$
(4)

The electroreduction of the manganese metal is the main cathodic reaction, and the side reaction is the hydrogen evolution reaction (HER). The oxygen evolution reaction (OER) is the main anodic reaction, and the side reaction is the electro-oxidation reaction to generate anode slime (mainly  $MnO_2$ ). Owing to the relatively close potential of OER and  $MnO_2$  deposition, it is difficult to avoid the side reaction of  $MnO_2$  formation.<sup>4</sup> Therefore, strict control of anode slime

production is one of the important technical problems and indicators for high-quality development of the electrolytic manganese industry.

In the actual production of manganese, a lead-based quaternary alloy anode (Pb–Ag–Sn-Sb) is widely used as an anode. The lead-based anode undergoes oxidation reaction in the acid system to form a smooth and dense oxide layer, which is resistant to corrosion and highly conductive, and has the stability of continuous operation.<sup>5–7</sup> However, the lead-based anode has a high oxygen evolution potential (OEP), which leads to the violent occurrence of anode side reactions, resulting in a large amount of anode slime.<sup>8,9</sup> The anode slime layer deposited on the anode surface is mainly  $\alpha$ -MnO<sub>2</sub> with poor conductivity, which leads to the increase of cell voltage and energy consumption. In addition, the anode slime (MnO<sub>2</sub> particles) suspended in the solution can block the diaphragm and cause the short circuit of the cathode and anode.<sup>10,11</sup> More seriously, the lead-based anode will continue to be electro-

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© 2023 The Authors. Published by American Chemical Society oxidized and dissolved during the process of manganese electrowinning, and the  $\alpha$ -MnO<sub>2</sub> layer is loose and porous, which cannot effectively protect the lead-based anode substrate,<sup>12</sup> resulting in the anode slime becoming an industrial hazardous waste containing lead.<sup>13</sup> At the same time, our research shows that the use of lead-based anodes in manganese electrowinning causes periodic anode potential oscillation or current oscillation, resulting in additional nonpower energy consumption, and the crystal form and morphology of the anode MnO<sub>2</sub> layer are the main factors inducing electrochemical oscillation.<sup>14,15</sup> Therefore, exploring a novel anode instead of a lead-based anode can reduce the production of anode slime and lead pollution and improve current efficiency in manganese electrowinning, which plays an important role in promoting the clean production and sustainable development of the electrolytic manganese industry.

Coated titanium anode is a promising novel anode for manganese electrodeposition, which can replace the lead-based anode.<sup>16</sup> Liu et al. investigated the performance of the Ti/ IrO<sub>2</sub>-RuO<sub>2</sub>-SiO<sub>2</sub> anode for manganese electrowinning in an anion-exchange membrane electrolysis reactor; the current efficiency increased by 10% while energy consumption decreased by 27%, and no anode slime was produced.<sup>17</sup> Luo et al. prepared a  $Ti/Ru_{1/3}Sn_{2/3}O_2$  anode, which exhibited excellent OER catalytic performance and reduced about onethird of the anode slime.<sup>18</sup> Coated titanium anodes still have disadvantages of a complex preparation process, participation of precious metals, and difficulty in maintaining coating activity. Therefore, coating materials with low cost, high coating catalytic activity, and stability become necessary. As a member of the Magnéli phase (Ti<sub>n</sub>O<sub>2n-1</sub>,  $n \ge 4$ ), Ti<sub>4</sub>O<sub>7</sub> has the advantages of good electrical conductivity, excellent chemical stability in acidic systems, and strong cost competitiveness.<sup>19,20</sup> Li et al. used a Ti<sub>4</sub>O<sub>7</sub> anode to electro-oxidate tetracycline (TC) in wastewater, and the total removal rate of TC was more than 90%.<sup>21</sup> The S/Ti<sub>4</sub>O<sub>7</sub> composite cathode prepared by Liu et al. exhibited a capacity decay of about 0.09% per cycle in 500 cycles and low battery-transfer resistance.<sup>22</sup> Li et al. studied the performance of the electrode with Ti<sub>4</sub>O<sub>7</sub> material and found that the electrode has both oxygen reduction reaction and OER activity.<sup>23</sup> Han et al. studied the performance of the Al/Ti<sub>4</sub>O<sub>7</sub>/RuO<sub>2</sub>-TiO<sub>2</sub>-SnO<sub>2</sub> anode and found that the electrode potential was evenly distributed. The current efficiency and electrolysis energy consumption were 5.59% higher and 16.2% lower than the Ti/RuO<sub>2</sub>-TiO<sub>2</sub> anode in cobalt electrodeposition, respectively.<sup>24</sup> Although Ti<sub>4</sub>O<sub>7</sub> has shown technical applications in environmental water treatment, fuel cells, and batteries,  $^{22,25,26}$  the application of Ti<sub>4</sub>O<sub>7</sub>coated anodes in manganese electrodeposition has not been studied.

In this study, a  $Ti_4O_7$ -coated titanium anode ( $Ti/Ti_4O_7$ anode) was applied to manganese electrodeposition for the first time. The anode performance, anode reaction, and anode slime formation mechanism of the  $Ti/Ti_4O_7$  anode were investigated, and the lead-based anode (Pb anode) was used as the comparison electrode. The feasibility of the  $Ti/Ti_4O_7$ anode as an alternative anode material for industrial manganese electrodeposition was evaluated by a galvanostatic electrolysis experiment. The chemical composition and microstructure of anode products were characterized by scanning electron microscopy (SEM), X-ray photoelectron spectroscopy (XPS), and X-ray diffraction (XRD). The anodic reaction mechanism of the  $Ti/Ti_4O_7$  anode in the process of electrodeposition of manganese was further clarified by electrochemical tests such as cyclic voltammetry (CV), linear voltammetry (LSV), chronopotentiometry (CP), Tafel polarization test, and electrochemical impedance spectroscopy (EIS). This study aims to provide a theoretical basis for the electrolytic manganese metal industry to find alternative, energy-saving, and environmentally friendly anode materials.

#### 2. EXPERIMENTAL SECTION

**2.1. Materials.** The Ti/Ti<sub>4</sub>O<sub>7</sub> anode was kindly supplied by Changsha Purong Chemical Co., Ltd. The Ti/Ti<sub>4</sub>O<sub>7</sub> anode was prepared by the plasma spraying method, the preparation method (Text S1) is discussed in the Supporting Information. The lead-based quaternary alloy anode (PbSb<sub>0.003</sub>Sn<sub>0.0003</sub>Ag<sub>0.0003</sub>) was provided by Southern Manganese Group Co., Ltd. Manganese sulfate (MnSO<sub>4</sub>·H<sub>2</sub>O), ammonium sulfate ((NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub>), selenium dioxide (SeO<sub>2</sub>), and sulfuric acid (H<sub>2</sub>SO<sub>4</sub>) were all analytical grade, purchased from Guoyao Holding Chemical Reagents Co., Ltd. All reagents were prepared by using ultrapure water (specific resistance of 18 MΩ·cm). The composition of the simulated manganese sulfate electrolyte is 30 g L<sup>-1</sup> Mn<sup>2+</sup> (MnSO<sub>4</sub>), 120 g L<sup>-1</sup> (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub>, and 30 mg L<sup>-1</sup> SeO<sub>2</sub>.

2.2. Electrochemical Measurement. Electrochemical analysis was carried out using an electrochemistry workstation (CHI660E, Shanghai Chenhua) with a three-electrode system. Ti/Ti<sub>4</sub>O<sub>7</sub> and Pb anodes with a working area of 1 cm<sup>2</sup> were used as working electrodes, and a stainless steel electrode and a saturated calomel electrode (SCE) were used as counter electrode and reference electrode, respectively. When the cathodic current density is 350 A m<sup>-2</sup>, the change of anode potential with time under direct current (DC) power and hyperchaotic circuit (HCC) was tested by CP. In the electrolyte without  $Mn^{2+}$  (120 g L<sup>-1</sup> (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub>, 30 mg L<sup>-1</sup>  $SeO_2$ ), the LSV test was carried out at a scanning rate of 10 mV s<sup>-1</sup>. The polarization curve was plotted by the relationship between the overpotential  $(\eta)$  and log (j). In the MnSO<sub>4</sub> electrolyte, the EIS test was performed at an open circuit voltage with an amplitude of 5 mV and a frequency range of 0.01 Hz to 100 kHz. CV tests were performed at a scan rate of  $5 \text{ mV s}^{-1}$  in the potential range of 0.3–2.0 V and 5, 10, 15, 25, and 50 mV s<sup>-1</sup> in the potential range of 0.3-1.8 V. The Tafel polarization test was performed at a scan rate of 10 mV s<sup>-1</sup> in a 1 mol/L  $H_2SO_4$  solution, and the test range was from 0 to 1.2 V.

**2.3. Characterization Techniques.** The morphology of the anode and anode slime were characterized by SEM (VEGA IILMA, TESCAN). The phase and elemental compositions of Ti<sub>4</sub>O<sub>7</sub> coating and plate anode slime were determined by XRD (D/Max-2500, j Rigaku) using Cu K $\alpha$  radiation. The chemical composition and elemental valence were analyzed by XPS (ESCALAB250Xi, Thermo Scientific). The binding energy values were corrected using the carbon C 1s binding energy at 284.8 eV.

**2.4. Electrolysis Experiments.** Galvanostatic electrolysis was conducted in 450 mL of laboratory cell electrolyte solution capacity. The anode area and cathode area are separated by a nonwoven membrane. The anode was a flat  $Ti/Ti_4O_7$  anode or a Pb anode ( $3.0 \times 4.5 \text{ cm}^2$  per piece), and the cathode was a stainless steel sheet ( $3.0 \times 4.5 \text{ cm}^2$  per piece). The cathode current density of  $350 \text{ Am}^{-2}$  was maintained by a DC-regulated power supply for electrolysis, and the electrolysis time was set to 2, 4, 6, and 8 h. During long-term electrolysis



Figure 1. Characterization of the  $Ti_1/Ti_4O_7$  anode: (a) XRD spectrum of the  $Ti_4O_7$  powder, (b) XPS full spectrum of the  $Ti_4O_7$  powder, (c) Ti 2p, and (d) SEM image of the anode surface.



Figure 2. Schematic diagram of the manganese electrolysis experiment using the Ti/Ti<sub>4</sub>O<sub>7</sub> anode.

(after 2 h), the electrolyte was supplemented and extracted by a circulating pump. The cathode current efficiency (CE) and the energy consumption (EC) for Mn electrowinning were calculated as follows

$$CE = \Delta m / (q \cdot i \cdot \Delta t) \tag{5}$$

$$EC = (U \cdot 1000) / (q \cdot CE) \tag{6}$$

where  $\Delta m/\Delta t$  is the mass gain per unit area of the cathode over the time interval  $\Delta t$  (g h<sup>-1</sup>); *i* is the applied current (A); *q* is the electrochemical equivalent of Mn (1.025 g (A h)<sup>-1</sup>); EC is the energy consumption ((kW h) t<sup>-1</sup>); and *U* is the cell voltage (V).

# 3. RESULTS AND DISCUSSION

**3.1. Chemical Composition and Structural Character istics.** Figure 1a shows the XRD pattern of the  $Ti_4O_7$  powder in the coating material. The major peaks matching the characteristic peaks of Ti<sub>4</sub>O<sub>7</sub> (PDF card 50-0789) occur at 20.7, 26.3, 31.7, 34.0, 40.5, 53.1, 55.0, 66.4, and 67.8° (and indicated by red dots), confirming the presence of the Magnéli phase Ti<sub>4</sub>O<sub>7</sub> as the major composition. Ti<sub>5</sub>O<sub>9</sub> also exists (Figure S1);  $Ti_4O_7$  and  $Ti_5O_9$  are the most conductive titanium oxides, which do not affect the conductivity of the electrode.<sup>27,28</sup> XPS was employed to identify the chemical composition and element combination state of the Ti<sub>4</sub>O<sub>7</sub> powder. The XPS full spectrum shown in Figure 1b confirms the coexistence of Ti and O elements. Figure 1c shows the Ti 2p double peak of Ti<sub>4</sub>O<sub>7</sub>. Ti  $2p_{3/2}$  has a tail at 456.8 eV, which is a typical feature of Ti<sup>3+</sup>, and the main peak at 459.0 eV can be assigned to Ti<sup>4+</sup>.<sup>20</sup> According to the XPS spectrum, there is about 18% Ti<sup>3+</sup> in the structure of the Magnéli phase Ti<sub>4</sub>O<sub>7</sub>. The valence state of the Ti<sub>4</sub>O<sub>7</sub> powder in the coating is consistent with the results of Tominaka et al., indicating that the crystal structure of Ti<sub>4</sub>O<sub>7</sub> is rutile block interspersed with corundum-like Ti<sub>2</sub>O<sub>3</sub> layer, and the resulting vacancies may



Figure 3. Experimental parameters of electrolysis process: (a) cell voltage, (b) pH of the anodic solution, and (c) pH of the cathodic solution.



Figure 4. Anodic potential-time curves of galvanostatic polarization for 1 h under different power sources: (a, c) DC and enlarged view; (b, d) HCC and enlarged view.

allow sufficient shrinkage in the lattice, resulting in high conductivity of the Magnéli phase titanium oxide.<sup>29</sup> The SEM of the anode surface shown in Figure 1d, and the microstructure of the  $Ti/Ti_4O_7$  anode surface, presents a dense honeycomb-like surface. The  $Ti_4O_7$  aggregates are tightly packed in spherical particles with a particle diameter of 60–100 nm. There are abundant porous channels on the anode surface, which provide sufficient surface area and internal space to expose more reactive sites.

**3.2. Experimental Study on Electrolysis Process.** The galvanostatic electrolysis for 2 h was carried out at a cathode current density of 350 A m<sup>-2</sup> to evaluate the feasibility of the  $Ti/Ti_4O_7$  anode as an alternative anode material for industrial manganese electrodeposition. The schematic diagram of the electrolysis experiment is shown in Figure 2, and the Pb anode serves as the comparison anode. As presented in Figure 3a, the

U of the Pb anode decreased from 4.02 to 3.87 V after 2 h. For the Ti/Ti<sub>4</sub>O<sub>7</sub> anode, the U increased with the electrolysis, from 3.73 to 3.77 V. This is because MnO<sub>2</sub> gradually covers the surface of the Ti/Ti4O7 anode, and the OER process is transferred to the MnO<sub>2</sub> layer, resulting in different changes. The average cell voltages  $(U_{aver})$  of Ti/Ti<sub>4</sub>O<sub>7</sub> and Pb anodes were 3.752 and 3.915 V, respectively, which decreased by about 163 mV. The CE was 83.80%, which was 3.22% higher than that of the Pb anode, and EC was 4368.12 k Wh  $t^{-1}$ , reduced by 7.82%, which shows excellent anode performance. In Figure 3b, the pH of the anode region decreases with the increase of time. The average pH values of the Ti/Ti<sub>4</sub>O<sub>7</sub> anode and the Pb anode were 1.98 and 1.63, respectively. The Ti/ Ti<sub>4</sub>O<sub>7</sub> anode has a higher pH, indicating that the solution becomes acidic and can inhibit the hydrolysis reaction of Mn<sup>3+</sup> in the solution to form anode slime.<sup>30</sup> The pH of the cathode

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region showed a trend of increasing first and then decreasing (Figure 3c). This is because the hydrogen evolution overpotential of the Mn metal is higher than that of the stainless steel.<sup>31</sup> Under the Ti/Ti<sub>4</sub>O<sub>7</sub> anode, the cathode pH is lower and the maximum pH value appears 30 min earlier. The possible reasons could be explained as Mn is uniformly covered on the cathode earlier and the HER is inhibited.<sup>32</sup>

The anode potential was analyzed under DC and HCC. The design and principle of the hyperchaotic circuit have been shown in a previous research work.<sup>33</sup> The anode potentialtime curves under the HCC before filtering are shown in Figure S2. As presented in Figure 4a,b, the Pb anode has an obvious electrochemical oscillation phenomenon, resulting in additional energy consumption. Under the Ti/Ti<sub>4</sub>O<sub>7</sub> anode, there was no obvious anodic electrochemical oscillation, but only a slight fluctuation of the anode potential (Figure 4c,d). In DC polarization, the anode potential of the  $Ti/Ti_4O_7$  anode and Pb anode was 1.8 and 2.23 V, respectively, and the average anode potential of the Ti/Ti<sub>4</sub>O<sub>7</sub> anode was 430 mV lower. In HCC polarization, the anode potential was 1.75 and 2.19 V, respectively, and the Ti/Ti<sub>4</sub>O<sub>7</sub> anode still has low anode potential. The application under different power sources showed that the anode potential under the Ti/Ti<sub>4</sub>O<sub>7</sub> anode was reduced, which greatly reduced the energy consumption of electrolysis and avoided the additional energy consumption caused by the electrochemical oscillation.

The stability of the  $Ti/Ti_4O_7$  anode and the distribution of anode slime were investigated, and long-term electrolysis experiments (2, 4, 6, 8 h) were carried out. The experimental parameters of the electrolysis process are given in Table 1. The

Table 1. Ti/Ti<sub>4</sub>O<sub>7</sub>-Anode Galvanostatic Electrolysis Experimental Results

	$U_{\rm aver}$ (V)		CE (%)		EC (kwh $t^{-1}$ )	
experiment time(h)	Pb	Ti <sub>4</sub> O <sub>7</sub>	Pb	Ti <sub>4</sub> O <sub>7</sub>	Pb	Ti <sub>4</sub> O <sub>7</sub>
2	3.85	3.71	80.84	82.97	4646.33	4362.43
4	3.91	3.82	79.77	81.95	4782.04	4547.68
6	3.88	3.76	80.74	82.6	4688.34	4441.03
8	3.84	3.74	77.58	80.04	4829.04	4558.71

 $U_{\text{aver}}$  of the Ti/Ti<sub>4</sub>O<sub>7</sub> anode in 2–8 h was 3.71, 3.82, 3.76, and 3.74 V, respectively, which was 100–150 mV lower than that of Pb anode at the same time. After 8 h of electrolysis,

compared with the Pb anode, CE of the  $Ti/Ti_4O_7$  anode improved by 2.48% and EC reduced by 5.60%.

The anode slime on the plate and that suspended in the solution were collected, cleaned, and dried, respectively. The formation and composition of different positions are shown in Figure 5. Under the Pb anode, red-brown anode slime was rapidly formed in the electrolyte; after a period of time,  $MnO_2$  covered the surface of the anode, and a large number of black particles were suspended in the electrolyte. Under the Ti/ $Ti_4O_7$  anode, the anode product was mainly produced on the anode and the solution is always kept in a transparent state. After 8 h of electrolysis, the solution anode slime was 0.3273 g, which was reduced 90.42%. In summary, the Ti/ $Ti_4O_7$  anode has the function of stable and efficient operation for a long time inhibiting the formation of anode slime.

**3.3. Chemical Composition and Morphology Analysis of Anode Slime.** In order to explore the mechanism of anode slime generation under the  $Ti/Ti_4O_7$  anode, the plate anode slime was collected, and the phase, composition, and surface morphology were analyzed. The XRD spectra of the plate anode slime under different anodes are shown in Figure 6.



Figure 6. XRD patterns of the plate anode slime under different anodes.

MnO<sub>2</sub> produced under the Pb anode and the Ti/Ti<sub>4</sub>O<sub>7</sub> anode contained  $\alpha$ -MnO<sub>2</sub>,  $\gamma$ -MnO<sub>2</sub>, and  $\varepsilon$ -MnO<sub>2</sub>, but there were some differences. For the Pb anode, the peaks at 12.5, 18.0, 28.3, 37.5, 41.9, 55, and 65.4° were indexed to the characteristic peaks of the  $\alpha$ -MnO<sub>2</sub> phase (PDF card 44–



Figure 5. Generation and distribution of anode slime under different anodes: (a) solution anode slime and (b) plate anode slime.



Figure 7. SEM images of anode slime under different anodes: (a) Pb anode  $MnO_2$  layer, (b)  $Ti/Ti_4O_7$  anode  $MnO_2$  layer, (c) the enlarged view of the  $MnO_2$  layer on the  $Ti/Ti_4O_7$  anode, and (d)  $Ti/Ti_4O_7$  anode slime.



Figure 8. XPS spectra of anode slime: (a-c) Pb anode, (d-f) Ti/Ti<sub>4</sub>O<sub>7</sub> anode, (a, d) full spectrum, (b, e) O 1s, and (c, f) Mn 2p.

0141). The XRD pattern of the deposits on the Ti/Ti<sub>4</sub>O<sub>7</sub> anode has prominent diffraction peaks at 37.1 and 66.3°. The MnO<sub>2</sub> layer electrodeposited on the Ti/Ti<sub>4</sub>O<sub>7</sub> anode is a combination of  $\gamma$ -MnO<sub>2</sub> and  $\epsilon$ -MnO<sub>2</sub> (mainly  $\gamma$ -MnO<sub>2</sub>). As known, the gamma ( $\gamma$ ) and akhtenskite ( $\epsilon$ ) polymorphs are often considered as the most active phase for aqueous reaction.<sup>34</sup>

The microstructure of the  $MnO_2$  layer on the Pb anode is shown in Figure 7a, and a rough and porous surface and fluffy accumulation of the manganese oxide layer were observed. This led to lead contamination and the occurrence of hydrolysis sludge, which would affect the purity of the electrolytic product.<sup>9</sup> For the microstructure of the  $MnO_2$  layer on the  $Ti/Ti_4O_7$  anode (Figure 7b), the surface of  $MnO_2$  was smooth and dense, which uniformly covered the surface of the anode. This physically isolated the  $Ti/Ti_4O_7$  substrate from the electrolyte and effectively improved the corrosion resistance of the anode coating. Interestingly, needle-like  $\gamma$ - $MnO_2$  (Figure 7c,d) was found in the local amplification diagram and anode slime particles, respectively, confirming the

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Figure 9. LSV curves for the OER at a scan rate of 5 mV s<sup>-1</sup>: (a, b) Ti/Ti<sub>4</sub>O<sub>7</sub> anode and Pb anode, (c, d) LSV curve corresponding Tafel plots.

XRD results. The needle-like  $\gamma$ -MnO<sub>2</sub> increased the specific surface area of the anode, reduced the cell pressure, and has better oxygen evolution performance.<sup>35,36</sup>  $\gamma$ -MnO<sub>2</sub> has excellent oxygen evolution performance, as tested below. Meanwhile, this explains the maintenance of oxygen evolution activity and the decrease of anode potential of the Ti/Ti<sub>4</sub>O<sub>7</sub> anode during electrolysis. The morphology of anode sediment particles under different anodes can be seen (Figure S3), and the morphology of the anode mud particles is consistent with the surface MnO<sub>2</sub> layer.

XPS analysis was performed to characterize the surface elemental composition and the chemical valence of the plate anode slime, and all peaks were calibrated at the peak position of C 1s. The full spectrum in Figure 8a,d shows that the anode slime under the two anodes was composed of Mn, O, and C elements. The O 1s spectrum of anode slime under the Ti/  $Ti_4O_7$  anode was located at 530.10 and 531.70 eV (Figure 8b), and anode slime under the Pb anode was located at 529.80 and 531.60 eV (Figure 8e). The main peak with a binding energy of about 530 eV represented metal oxides, while the peak with a binding energy of about 531.60 eV may be chemisorption oxygen such as low-coordinated O<sup>2-</sup> or O<sup>-.37,38</sup> The XPS spectra of Mn 2p in Ti/Ti<sub>4</sub>O<sub>7</sub> anode slime after electrolysis are shown in Figure 8c. The Mn 2p<sub>3/2</sub> binding energy peak was located at 642.3 eV, and the  $2p_{1/2}$  peak was located at 654.0 eV. The peak position distance between Mn  $2p_{3/2}$  and  $2p_{1/2}$ was 11.7 eV, which was in good agreement with the reported data of MnO<sub>2</sub>,<sup>4,39</sup> The main peak of binding energy at 642.3 eV was ascribed to Mn (III), and the binding energy at 644.0 eV was attributed to Mn (IV).<sup>40,41</sup> There was a significant difference in the valence state of manganese in the anode slime under the electrolysis of the Pb anode and the Ti/Ti<sub>4</sub>O<sub>7</sub> anode. The relative content ratio of Mn(III) and Mn(IV) in deposited

 $MnO_2$  is shown in Table S1. The ratio of Mn (III) to Mn (IV) in the anode slime under the Ti/Ti<sub>4</sub>O<sub>7</sub> anode was 2.3, and that under the Pb anode was 1.6. The rich Mn (III) in the lattice is responsible for the superior OER performances.<sup>42</sup>

Through the above analysis of the surface morphology, chemical composition, and element valence of anode slime under different anodes, the variability in the formation mechanism of anode slime is investigated. The anode slime of the Pb anode was mainly  $\alpha$ -MnO<sub>2</sub> crystal, which limited its catalytic oxygen evolution performance, resulting in a large amount of anode slime and a loose MnO<sub>2</sub> layer.<sup>4</sup> Variation in anode slime formation under different anodes can be explained by the hydrolysis mechanism of Mn<sup>2+</sup> oxidation, which is given by eqs 7-9.<sup>30,43</sup> In summary, the Ti<sub>4</sub>O<sub>7</sub> coating has high conductivity, which provided a large number of reactive sites, and generated a uniform and dense  $\gamma$ -MnO<sub>2</sub> layer. Needle-like  $\gamma$ -MnO<sub>2</sub> has higher catalytic oxygen evolution activity and conductivity, which inhibited the oxidation of  $Mn^{2+}$  (eq 7) and reduced the formation of anode slime. Dense MnO<sub>2</sub> layer and higher pH anode solution during the electrolysis process relatively completely inhibited the diffusion of Mn<sup>3+</sup> into the solution to produce solution anode slime (eqs 8, 9).

$$Mn^{2+} = Mn^{3+} + e^{-}$$
(7)

$$Mn^{3+} + 2H_2O = MnOOH + 3H^+(fast)$$
(8)

$$MnOOH = MnO_2 + H^+ + e^{-}(slow)$$
(9)

**3.4.** Analysis of Anodic Reaction Mechanism. The OER activity of the  $Ti/Ti_4O_7$  anode and the deposited  $MnO_2$  layer were evaluated in a simulated electrolyte without  $Mn^{2+}$ . Figure 9a,b shows the LSV polarization curves of the two anodes at a scan rate of 5 mV s<sup>-1</sup>. The initial OEP of the corresponding anode can be obtained by tangenting the stable



Figure 10. EIS with the  $Ti/Ti_4O_7$  and Pb anodes: (a) Nyquist plots, (b) equivalent circuit model of the anodes, and (c, d) Bode plots of the anodes.

Table 2. Electrochemical Data and the Corresponding Relative Errors Determined from Ero Frots with a 10 million
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$R_{\rm s} \left( \Omega \cdot {\rm cm}^{-2} \right)$	$CPE_1$ (F·cm <sup>-2</sup> )	$R_{\rm ct1} \; (\Omega \cdot {\rm cm}^{-2})$	$CPE_2 (F \cdot cm^{-2})$	$R_{\rm ct2}~(\Omega \cdot {\rm cm}^{-2})$
1.98 (1.24%)	$5.98 \times 10^{-4} (4.5\%)$	2.71 (4.24%)	$3.76 \times 10^{-2} (1.45\%)$	73.98 (5.43%)

oxygen evolution stage. For the Ti/Ti<sub>4</sub>O<sub>7</sub> and Pb anodes, the OEP values were 1.319 and 1.633 V, respectively, 324 mV lower than that of the Pb anode. After deposition of the MnO<sub>2</sub> layer, the initial OEP of the Ti/Ti<sub>4</sub>O<sub>7</sub> anode was 335 mV lower than that of the Pb anode. On the basis of the LSV, the corresponding Tafel plots of the two anodes were determined (Figure 9c,d). For the Pb anode, the Tafel plots have a double slope behavior in the low potential region and the high potential region; with the increase of potential, the OER becomes the dominant reaction.<sup>44,45</sup> For the polarized Pb anode, the Tafel slope of the OER process was 468 mV  $dec^{-1}$ , and for the polarized Ti/Ti<sub>4</sub>O<sub>7</sub> anode, the Tafel slope was 323 mV dec<sup>-1</sup>, which shows the kinetic advantages of the Ti/Ti<sub>4</sub>O<sub>7</sub> anode in the OER process. In manganese electrowinning, the Ti/Ti<sub>4</sub>O<sub>7</sub> anode always maintains good oxygen evolution activity, which can reversely inhibit the manganese oxidation reaction, thereby reducing the plate anode slime.

EIS measurements were conducted to analyze the electrontransfer characteristics and anodic reaction of the Ti/Ti<sub>4</sub>O<sub>7</sub> anode. The equivalent circuit model obtained by EIS and the corresponding Nyquist diagram are shown in Figure 10. The data were simulated according to the Equivalent Circuit (Figure 10a), where  $R_s$  is the solution resistance,  $R_{ct}$  is the charge-transfer resistance,  $W_0$  is the Warburg diffusion resistance, and CPE<sub>1</sub> is the double-layer capacitance. For the Pb anode, two capacitor rings were observed in the Nyquist plots (Figure 10b), and the Bode plot showed two time constants (Figure 10c). This indicates that the reaction process was composed of two charge-transfer control processes. For the Ti/Ti<sub>4</sub>O<sub>7</sub> anode, the anodic reaction characteristics changed significantly. A semicircle appeared in the high frequency region of the Nyquist plots, indicating that the charge-transfer step was likely the control step; the linear correlation in the low frequency region indicates that the anodic reaction process was diffusion-controlled.<sup>46,47</sup>

Data were simulated according to the model circuit shown in Tables 2 and 3. Anode electrode reaction  $R_{ct}$  was reduced from

Table 3. Electrochemical Data and the Corresponding Relative Errors Determined from EIS with a  $\rm Ti/Ti_4O_7$  Anode

$R_{\rm s}~(\Omega{\cdot}{\rm cm}^{-2})$	CPE $(F \cdot cm^{-2})$	$R_{\rm ct} \; (\Omega \cdot {\rm cm}^{-2})$	$Z_{\rm w} \left( \Omega \cdot {\rm cm}^{-2} \right)$
1.94 (1.51%)	$3.85 \times 10^{-6} (3.02\%)$	1.81 (1.21%)	470.3 (1.35%)

73.98  $\Omega$  cm<sup>-2</sup> of the Pb anode to 1.81  $\Omega$  cm<sup>-2</sup>. The Ti/Ti<sub>4</sub>O<sub>7</sub> anode has a low charge-transfer resistance.  $W_0$  is 470.3  $\Omega$  cm<sup>-2</sup>, indicating that the diffusion of ions in the solution was the limiting step of the anodic reaction.<sup>48</sup> After the Ti/Ti<sub>4</sub>O<sub>7</sub> anode was used, the control step of the anodic reaction changed from a charge-transfer process to a charge-transfer process and a diffusion process. Combined with the analysis of the Ti/Ti<sub>4</sub>O<sub>7</sub> anode surface morphology, the honeycomb Ti<sub>4</sub>O<sub>7</sub> particle clusters on the anode surface have good electron transport properties, providing a larger interface area and a large number of reactive sites for the anodic electrochemical



Figure 11.  $Ti/Ti_4O_7$  anode reaction electrochemical test: (a) CV curve with a Pb anode in the MnSO<sub>4</sub> electrolyte, (b–d) LSV curves of the Pb, Pt, and Ti/Ti<sub>4</sub>O<sub>7</sub> anodes in different Mn<sup>2+</sup> concentrations in the electrolyte, (e) CV curves of the Ti/Ti<sub>4</sub>O<sub>7</sub> anode at different potential scanning rates (5, 10, 15, 25, and 50 mV/s), and (f) relationship between the anodic oxidation peak current and the potential scanning rate of the Ti/Ti<sub>4</sub>O<sub>7</sub> anode.

Table 4. Corrosion Performance Parameters in Tafel Curves of the  $Ti/Ti_4O_7$  and Pb Anodes under Different Polarization Times

anode	Pb anode			Ti/Ti <sub>4</sub> O <sub>7</sub> anode		
time (min)	$j_{\rm corr} \times 10^{-4} ~({\rm A} \cdot {\rm cm}^{-2})$	$E_{\rm corr}$ (V)	$R_{\rm p} (\Omega)$	$j_{\rm corr} \times 10^{-4} \ (\text{A} \cdot \text{cm}^{-2})$	$E_{\rm corr}$ (V)	$R_{\rm p}(\Omega)$
0	1.694	-0.378	258.1	0.359	-0.650	607.9
5	1.986	0.162	165.1	1.025	0.590	328
15	2.738	0.255	149.2	1.181	0.627	320.4
30	3.085	0.287	131.6	3.046	0.648	127.7
50	4.517	0.334	97.4	2.764	0.652	164.4
60	4.007	0.441	108.3	2.254	0.656	171.4

reaction.<sup>49,50</sup> This makes the Ti/Ti<sub>4</sub>O<sub>7</sub> anode exhibit excellent charge-transfer performance, and Mn<sup>2+</sup> can be rapidly and thoroughly oxidized at the interface to form a uniform and dense active  $\gamma$ -MnO<sub>2</sub> layer. The high diffusion resistance also blocks the diffusion path of Mn<sup>3+</sup> in the system.

The anodic reaction mechanism of the  $Ti/Ti_4O_7$  anode was investigated. CV test was carried out in the  $MnSO_4$  electrolyte at a scanning rate of 5 mV s<sup>-1</sup>. As shown in Figure 11a, the CV curve of the Pb anode does not show the redox peak of manganese, and the lead oxidation peak appears at 1.5 V. The CV curve of the Ti/Ti<sub>4</sub>O<sub>7</sub> anode shows a pair of redox peaks. The oxidation peak is at about 1.1 V, and the reduction peak is nearly 0.8 V. However, the peak current of the reverse reduction peak is small, which shows that partial reversible reaction of manganese may occur in the anode.<sup>51</sup> In order to determine whether the oxidation peak in the CV curve is caused by the oxidation of manganese, an LSV test of the anode at different  $Mn^{2+}$  concentrations was carried out. A Pb anode and a platinum electrode (Pt anode) were selected as the comparison anode. Only the oxidation peak and oxygen evolution characteristic curve of lead appeared on the Pb anode (Figure 11b). The oxidation peak of the Pt anode appeared at about 1.1 V, and the peak current increased with the increase of Mn<sup>2+</sup> concentration (Figure 11c). The Ti/ Ti<sub>4</sub>O<sub>7</sub> electrode also has an oxidation peak at 1.1 V, and the change in trend of the peak current density is the same as that of the Pt anode (Figure 11d). Through the comparison experiments, it could be obtained that the anodic peak on the Ti/Ti<sub>4</sub>O<sub>7</sub> anode at about 1.1 V is the oxidation reaction of Mn<sup>2+</sup>. Combined with CV test, it shows that the oxidation effect of Mn<sup>2+</sup> on the Ti/Ti<sub>4</sub>O<sub>7</sub> anode is more significant than that on the Pb anode. The oxidation reaction is faster, and the anode surface is faster to generate a dense MnO<sub>2</sub> layer. Figure 11e shows the CV curves of the Ti/Ti<sub>4</sub>O<sub>7</sub> anode at different scan rates in the range of  $5-50 \text{ mV s}^{-1}$ . The shape of the CV curve is not affected by the change of the potential scanning rate. The redox potential difference enlarges with the increases of the scanning speed, and all of them show symmetrical partial



Figure 12. Tafel curves of the anode in 1 mol  $L^{-1}$  H<sub>2</sub>SO<sub>4</sub>: (a) anode metal matrix and polarization for 60 min, and (b, c) different polarization times of the Pb and Ti/Ti<sub>4</sub>O<sub>7</sub> anodes.

reversible redox peaks. In Figure 11f, the anodic oxidation peak current density is linearly related to the square root of the potential scanning rate, indicating that the anodic reaction is controlled by the diffusion process. This is consistent with the EIS results of the above anodic reaction.

3.5. Ti/Ti<sub>4</sub>O<sub>7</sub> Anode Corrosion Resistance. Corrosion potential  $(E_{corr})$ , corrosion current density  $(j_{corr})$ , and polarization resistance  $(R_p)$  were obtained by linear fitting of Tafel curves, as shown in Table 4.  $E_{corr}$  is a thermodynamic parameter to characterize the degree of difficulty of corrosion of materials in the medium.  $j_{corr}$  and  $R_p$  are kinetic parameters used to characterize the corrosion rate of the material in the medium. From Figure 12a, it can be seen that the  $E_{\rm corr}$  of the  $Ti/Ti_4O_7$  anode metal matrix is the smallest, which is -0.65 V, indicating that metal matrix is corroded first in acidic solution, while the  $E_{\rm corr}$  of Pb anode is the second, which is -0.378 V. However, the  $j_{corr}$  of the Ti/Ti<sub>4</sub>O<sub>7</sub> anode metal matrix is the smallest, which is  $3.59 \times 10^{-5}$  A cm<sup>-2</sup>, and the corrosion rate in  $H_2SO_4$  solution is the smallest. The  $E_{corr}$  of different anode metal matrixes and 60 min polarizations is as follows: Ti/  $Ti_4O_7$ -60 min > Pb-60 min > Pb metal matrix >  $Ti/Ti_4O_7$ metal matrix. Figure 12b,c explores the effect of the MnO<sub>2</sub> layer formed under different anodes on the corrosion performance. Tafel tests were carried out on the anodes after galvanostatic polarization at 5, 15, 30, and 50 min. The  $E_{\text{corr}}$  of the Ti/Ti<sub>4</sub>O<sub>7</sub> anode after different polarization times is higher than that of the Pb anode, indicating that the  $Ti/Ti_4O_7$  anode has better chemical stability under the coverage of the MnO<sub>2</sub> layer. At the same time,  $j_{corr}$  of the Ti/Ti<sub>4</sub>O<sub>7</sub> anode MnO<sub>2</sub> layer is smaller and the corrosion rate in the acidic system is lower. The results show that the Ti/Ti<sub>4</sub>O<sub>7</sub> anode has good corrosion resistance during the electrolysis process. The reason for this is that a more stable  $MnO_2$  layer is formed on the anode surface, which acts as a physical barrier to prevent corrosion and metal substrate oxidation.

## 4. CONCLUSIONS

In this study, a Ti<sub>4</sub>O<sub>7</sub>-coated titanium electrode was proposed as the anode for manganese electrolysis. The anode performance, anode reaction, and anode slime formation mechanism of the Ti/Ti<sub>4</sub>O<sub>7</sub> anode was studied. The galvanostatic electrolysis experiment showed that the average cell voltage of the Ti/ Ti<sub>4</sub>O<sub>7</sub> anode was 3.752 V, which was 163 mV lower than that of the Pb anode, the current efficiency increased by 3.22%, and the energy consumption decreased by 7.82%. The anode electrochemical oscillation disappeared and the nonpower energy consumption decreased. After continuous electrolysis of 8 h, the solution anode slime was reduced 90.42% and the plate anode slime 72.80%. This remarkably reduced the energy consumption of electrolysis and the generation of anode slime. The characterization test and electrochemical analysis showed that a uniform and dense  $\gamma$ -MnO<sub>2</sub> layer quickly formed at the initial stage of electrolysis. The  $\gamma$ -MnO<sub>2</sub> has a needle-like structure and more abundant Mn (III) in the lattice, which was beneficial to lower the cell voltage and OEP. The OEP of the Ti/Ti<sub>4</sub>O<sub>7</sub> anode was 324 mV lower than that of the Pb anode, and it maintained good catalytic OER activity during the electrolysis process, reversely inhibiting Mn<sup>2+</sup> oxidation and reducing the formation of anode slime. Dense MnO<sub>2</sub> layer, lower acidity anode solution, low charge-transfer resistance, and high diffusion resistance fully inhibit the diffusion of Mn<sup>3+</sup> to the solution to form solution anode slime. The application of the Ti/Ti<sub>4</sub>O<sub>7</sub> anode changes the structure and morphology of the anode MnO<sub>2</sub> layer, significantly reduces the amount of anode slime, avoids lead pollution, and improves the current efficiency. This provides a new way to achieve the clean production and sustainable development of electrolytic manganese metal industry.

#### ASSOCIATED CONTENT

#### Supporting Information

The Supporting Information is available free of charge at https://pubs.acs.org/doi/10.1021/acsomega.3c05273.

Preparation method of the  $Ti/Ti_4O_7$  anode, the XRD pattern of the  $Ti_4O_7$  powder, anodic potential-time curves for the  $Ti/Ti_4O_7$  anode and the Pb anode under HCC, SEM of anode slime particles under the  $Ti/Ti_4O_7$  and Pb anodes, table of relative content ratio of Mn(III) and Mn(IV) (PDF)

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#### **Author Contributions**

All the authors listed have approved the manuscript. **Notes** 

The authors declare no competing financial interest.

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