Original Article

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Palatal *en-masse* retraction of segmented maxillary anterior teeth: A finite element study

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Key words: Segmented palatal *en-masse* retraction, Finite element study, Anchor screw, Lever arm

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INTRODUCTION

En-masse retraction of the maxillary anterior teeth is a critical procedure in orthodontic treatment of protruded anterior teeth. To accomplish this, various methods have been attempted using continuous or segmental approaches from the labial or palatal side.¹⁻¹³

In the past, the use of continuous archwire mechanics with posterior teeth as anchorage was the most common method for achieving *en-masse* retraction of the anterior teeth.^{1-3,5} With this method, some anchorage loss was inevitable since the retraction force is applied to both anterior and posterior teeth. If absolute preservation of anchorage is critical, anchorage loss can be prevented by using temporary skeletal anchorage devices such as anchor screws.^{4,6-13} However, even with a screw, an unexpected rotation of the whole dentition can occur if a retraction force is not applied in the appropriate manner.

A palatal approach was preferred as an esthetic alternative to the labial approach,^{2-5,8-13} but torque control of the anterior teeth was more difficult with the conventional palatal approach using continuous archwire than with the labial approach.⁴ This difficulty was overcome by using segmented archwires with lever arm mechanics.^{2,4,5,8,10,13} A longer lever arm and gingivally higher skeletal anchorage in the palatal approach makes it possible to attain a force system favorable to controlled retraction of maxillary anterior teeth due to the width and depth of the palate.

Several mechanical analyses have been performed to assess *en-masse* retraction of the anterior teeth.¹⁰⁻¹³ However, all of them were only limited to the initial tooth movement immediately after the force application. The movement pattern of the anterior teeth was discussed based on the assumption that the movement direction was equal to the force direction, but the relationship between the force application point and the center of resistance (CR) changed as the teeth moved, and thereby the movement pattern also changed. In addition, the movement direction was not always equal to the force direction.¹⁴ At present, the precise mechanics of *en-masse* retraction is not still fully understood.

The aim of this study was to clarify the mechanics of tooth movement for palatal *en-masse* retraction of the anterior teeth by using anchor screws and lever arms. To achieve this purpose, the finite element method was used to simulate the overall orthodontic tooth movements.

MATERIALS AND METHODS

A finite element software, ANSYS 11 (ANSYS, Inc., Canonsburg, PA, USA), was used for the present finite

element analysis. Figure 1 shows the finite element model for simulating extraction space closure with *enmasse* retraction of the segmented anterior teeth. Assuming bilateral symmetry of the arch, only the left side was modeled. Three-dimensional models of the teeth were made based on computed tomography (CT) images of a dental study model (i21D-400C; Nissin Dental Products, Kyoto, Japan).¹⁵ Each tooth was meshed with shell elements and defined as a rigid body. The term "rigid" means "undeformable" in the present article. The rigid body was defined by using the multipoint constraint approach provided in ANSYS 11.

The teeth and alveolar bone were assumed to be rigid bodies. The periodontal ligament (PDL) of 0.2 mm thickness was constructed on the root with solid elements.¹⁶⁻¹⁸ Nonlinear stress–strain relationship of the PDL was approximated with a piecewise linear curve. It was determined based on *in vivo* measurements of tooth mobility, as shown in Appendix 1.

The palatal wire and lever arm were made from 0.8-mm stainless steel square wire. Considering their elastic deformation, the palatal wire and lever arm were assumed to be elastic beams with a Young's modulus and Poisson's ratio of E = 200 and v = 0.3, respectively. Using rigid beams, the segmented archwire was firmly fixed to the crowns at the bracket positions. The symmetrical boundary condition was applied at the median end of the wire (Figure 1).

Figure 2 shows the combinations of anchor screw positions and lever arm height. One anchor screw was



Figure 1. Finite element model for simulating overall orthodontic tooth movement. The alveolar bone was assumed to be a rigid body; the wire was fixed to the crowns; and symmetrical boundary condition was applied.





Figure 2. The center of resistance (CR) of anterior teeth, locations of anchor screws, and lever-arm height. Lines of action of force are drawn with red lines. **A**, Midpalatal anchor screw. **B**, Palatal slope screw.

placed in the midpalatal area. Two anchor screws were placed in high or low positions on the palatal slope. The location of the anchor screws was measured from the bracket position. Forces of 2 N were applied from the anchor screw(s) to the lever arms extended at the canines. This amount of force was the same as the force used in several clinical cases.^{5,12,13} The lever arm height was 12 mm for the midpalatal screw, and varied by 6 mm, 8 mm, and 10 mm for the palatal slope screw.

The CR of the anterior teeth was determined in the cases where the anterior teeth moved bodily. For this purpose, the anterior teeth were defined as a rigid body.¹⁶

Orthodontic tooth movement was assumed to occur by accumulation of the initial movement produced by elastic deformation of the PDL.^{17,18} Long-term orthodontic movement was simulated by the following repeating calculations. First, the initial movement of each tooth was calculated based on the application of a force to the lever arm in the finite element model. In this calculation, nodes on the outer surface of the PDL were fixed, because the alveolar bone was assumed to be a rigid body. Second, the alveolar socket of each tooth, namely nodes on the outer surface of the PDL of each tooth, were moved as a rigid surface by the same translations and rotations as the initial movement. Alveolar bone was not a factor in these calculations. By repeating these two steps, the teeth moved step by step. The force system acting on the teeth was updated at each step. The movement pattern of the teeth changed as the teeth moved. The number of repeating calculations, N,

corresponds to the time elapsed after the force application.

RESULTS

Figure 2A and 2B show the location of the CR of the anterior teeth and the line of action of the force with respect to the initial tooth position. Five combinations of screw positions and lever arm height were used to change the force direction. The lines of action of the force passed apical and coronal to the CR in the two combinations of low palatal screws and 10-mm height and 6-mm height lever arms, respectively, and through the CR in the other three combinations.

In the three cases where the line of action of the force passed through the CR, Figure 3 shows the movement pattern of the anterior teeth at the number of repeating calculations N = 800. The computational time required for these calculations was about 80 minutes using a personal computer (Intel Core i3, 2.8 GHz, 4GB RAM). The posterior teeth, which were not included in the simulation model, were illustrated in the Figures for observing the relative position with the anterior teeth. Mean stress in the PDL was depicted on the roots with color contours. Red and blue colors indicate compressive and tensile stresses, respectively. The tipping angle of the central incisor is written in the Figures. The positive and negative angles indicate palatal and labial tipping respectively.

For all cases in Figure 3, the anterior teeth translated almost bodily. Compressive and tensile stresses were



Figure 3. Movement patterns at N = 800, when the line of action of the force passed through the center of resistance (CR) at the initial position. **A**, Midpalatal position (lever-arm height, 12 mm) and **B**, high position (lever-arm height, 10 mm); the anterior teeth translated upward. **C**, Low position (lever-arm height, 8 mm); the anterior teeth translated horizontally without upward movement.

distributed on the palatal and labial sides of the roots, respectively. In the case with the midpalatal screw, the anterior teeth translated upward (Figure 3A). When the high positioned screws were placed on the palatal slope, the anterior teeth translated with some intrusion although the line of action of the force was horizontal (Figure 3B). In the case of the low-positioned screw, the anterior teeth translated horizontally although the line of action of the force 3C).

Figure 4A shows the tooth movement pattern in the combination of the low-positioned screw and 10-mmhigh lever arms at N = 800. The anterior teeth tipped labially at first because the line of action of force passed apical to the CR, and then translated with the initially produced tipping. Figure 4B shows the case of a 6-mmhigh lever arm, where the line of action of the force



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Figure 4. Movement patterns at N = 800, when the line of action of force passed apical or coronal to the center of resistance (CR) at the initial position. **A**, Low position (lever-arm height, 10 mm); the anterior teeth tipped labially. **B**, Low position (lever-arm height, 6 mm); the anterior teeth tipped lingually.

passed coronal to the CR. The anterior teeth tipped palatally at first and then translated.

DISCUSSION

Mechanics of tooth movement

When applying an upward and backward force passing through the CR using one anchor screw placed in the midpalatal area, the anterior teeth translated in a more upward direction than horizontal due to the vertical component of force (Figure 3A). In the cases where two anchor screws were placed on the palatal slope in the high position, the force was horizontal and backward without the vertical component. However, even with a horizontal force passing through the CR, the anterior teeth translated with some intrusion (Figure 3B). This movement direction did not coincide with the force direction. This result seemed to be contrary to common orthodontic sense. Osipenko et al.¹⁴ have demonstrated that the tooth movement direction is not always equal to the force direction. Their theory is explained in Appendix 2. When applying this theory to the anterior teeth segment, the ratio of spring constants in the principal directions became $k_1/k_2 > 1$, and thereby the teeth translated upward by the horizontal force. This movement pattern was produced due to an inclination of the anterior teeth. If the horizontal force passing through



the CR of the anterior teeth is applied perpendicular to their long axis, the teeth must translate in a horizontal direction without vertical movement.

Tooth movement patterns can change depending on the spring constants of the tooth supported with the PDL, k_1 and k_2 , which will be different for each tooth. The movement patterns simulated here are not general pattern but represent specific teeth having the same stress-strain relationship as in Appendix 1.

With regard to the clinical settings, it should be noted that the movement direction is not always equal to the force direction. In a clinical report,⁴ a force parallel to the occlusal plane was applied to the CR of the six anterior teeth, and although they were guided to move parallel by an archwire, the anterior teeth moved bodily with an unexpected intrusion. To move the anterior teeth bodily without intrusion or extrusion, a downward and backward force passing through the CR was necessary (Figure 3C). This force direction, namely the combination of the anchor screw position and lever arm height, was determined by trial and error. Movement patterns of the anterior teeth could be controlled by changing the height of the lever arm for pure horizontal translation.

The anterior teeth tipped labially and palatally (Figure 4) depending on the line of action of the force that passed apical or coronal to the CR at the initial position (Figure 2B). In these cases, the force systems varied as the anterior teeth tipped, and thereby the line of action of the force passed through the CR after a while (N = 800) (Figure 4). It was difficult to predict these movement patterns using only the initial force systems.

As we demonstrated in this study, tooth movement direction was not always coincident with the force direction. To control movement patterns of the anterior teeth, knowledge of their CR and the relationship between force direction and CR is essential. However, estimation of tooth movement is still difficult because it also depends on each individual property of the PDL, namely the spring constants k_1 and k_2 in Appendix 2. For this reason, it would be difficult to set an optimal combination of anchor screw positions and lever arm heights to achieve a desired movement pattern. In clinical settings, the movement patterns should be modified if an undesirable movement of the anterior teeth occurs.

Clinical consideration

Palatal *en-masse* retraction of the maxillary anterior teeth using anchor screws is an alternative method for the correction of lip protrusion. There are various methods to apply retraction force to the anterior teeth.¹⁻¹³ Anchor screws are quite useful for the *en-masse* re-

traction and are superior to conventional orthodontic mechanics because they allow for maximum retraction without any anchorage loss or patient cooperation. Therefore, careful use of anchor screws together with an understanding of the involved mechanical principles can expand the boundaries and scope of conventional fixed appliance therapy. In this study, we investigated the mechanics of palatal *en-masse* retraction of the anterior teeth by using the finite element method based on the position of anchor screws and height of the lever arm in the palatal area.

Even when tipping movement occurred as shown in Figure 4, the line of action of the force passed through the CR of the anterior teeth after some retraction. This might mean that the anterior teeth could be retracted bodily with the same height of the lever arm or anchor screws after some tipping has occurred. This might be clinically important. If the anterior teeth are labially inclined before treatment, a short lever arm would be necessary to upright the anterior teeth and then the same lever arm height might be used for bodily retraction after achieving a normal inclination, and when the line of action of the force passed coronal to the CR, the anterior teeth tipped clockwise during retraction.

CONCLUSION

By using an overall finite element simulation, the mechanics of palatal *en-masse* retraction of segmented maxillary anterior teeth were clarified. The following conclusions were obtained:

- 1. The tooth movement pattern changed depending on a combination of lever arm height and anchor screw position.
- 2. The maxillary anterior teeth tipped labially or palatally and translated when the line of action of the force passed apical or coronal to the CR.
- 3. The maxillary anterior teeth translated when the line of action of the force passed through the CR.
- 4. The maxillary anterior teeth moved bodily with an unexpected vertical movement when the line of the action was not perpendicular to the long axis of the anterior teeth even though the force direction was horizontal and passed through the CR.
- 5. The tooth movement pattern may be unpredictable in a clinical setting because it is not necessarily the same as the force direction.

CONFLICTS OF INTEREST

No potential conflict of interest relevant to this article was reported.

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REFERENCES

- Gjessing P. Controlled retraction of maxillary incisors. Am J Orthod Dentofacial Orthop 1992;101: 120-31.
- 2. Park YC, Choy K, Lee JS, Kim TK. Lever-arm mechanics in lingual orthodontics. J Clin Orthod 2000; 34:601-5.
- 3. Chung KR, Oh MY, Ko SJ. Corticotomy-assisted orthodontics. J Clin Orthod 2001;35:331-9.
- 4. Hong RK, Heo JM, Ha YK. Lever-arm and miniimplant system for anterior torque control during retraction in lingual orthodontic treatment. Angle Orthod 2005;75:129-41.
- 5. Kim SH, Park YG, Chung K. Severe Class II anterior deep bite malocclusion treated with a C-lingual re-tractor. Angle Orthod 2004;74:280-5.
- 6. Park YC, Chu JH, Choi YJ, Choi NC. Extraction space closure with vacuum-formed splints and miniscrew anchorage. J Clin Orthod 2005;39:76-9.
- Chung KR, Cho JH, Kim SH, Kook YA, Cozzani M. Unusual extraction treatment in Class II division 1 using C-orthodontic mini-implants. Angle Orthod 2007;77:155-66.
- 8. Park YC, Choi YJ, Choi NC, Lee JS. Esthetic segmental retraction of maxillary anterior teeth with a palatal appliance and orthodontic mini-implants. Am J Orthod Dentofacial Orthop 2007;131:537-44.
- 9. Chung KR, Kook YA, Kim SH, Mo SS, Jung JA. Class II malocclusion treated by combining a lingual retractor and a palatal plate. Am J Orthod Dentofacial Orthop 2008;133:112-23.

- 10. Jang HJ, Roh WJ, Joo BH, Park KH, Kim SJ, Park YG. Locating the center of resistance of maxillary anterior teeth retracted by Double J Retractor with palatal miniscrews. Angle Orthod 2010;80:1023-8.
- 11. Lee EH, Yu HS, Lee KJ, Park YC. Three dimensional finite element analysis of continuous and segmented arches with use of orthodontic miniscrews. Korean J Orthod 2011;41:237-54.
- Park JH, Tai K, Takagi M, Miyajima K, Kojima Y, Joo BH. Esthetic orthodontic treatment with a double J retractor and temporary anchorage devices. Am J Orthod Dentofacial Orthop 2012;141:796-805.
- 13. Mo SS, Kim SH, Sung SJ, Chung KR, Chun YS, Kook YA, et al. Torque control during lingual anterior retraction without posterior appliances. Korean J Orthod 2013;43:3-14.
- 14. Osipenko MA, Nyashin NY, Nyashin YI. Center of resistance and center of rotation of a tooth: the definitions, conditions of existence, properties. Russ J Biomech 1999;1:5-15.
- 15. Kojima Y, Kawamura J, Fukui H. Finite element analysis of the effect of force directions on tooth movement in extraction space closure with miniscrew sliding mechanics. Am J Orthod Dentofacial Orthop 2012;142:501-8.
- 16. Kojima Y, Fukui H. A finite element simulation of initial movement, orthodontic movement, and the centre of resistance of the maxillary teeth connected with an archwire. Eur J Orthod 2014;36:255-61.
- 17. Kojima Y, Fukui H. Numerical simulations of canine retraction with T-loop springs based on the updated moment-to-force ratio. Eur J Orthod 2012;34:10-8.
- 18. Kim MJ, Park JH, Kojima Y, Tai K, Chae JM. A finite element analysis of the optimal bending angles in a running loop for mesial translation of a mandibular molar using indirect skeletal anchorage. Orthod Craniofac Res 2018;21:63-70.

Appendix 1

The stress–strain relationship of the periodontal ligament (PDL) was assumed to be piecewise linear and was identified based on the mobility of the upper right first premolar measured *in vivo*. It was determined by trial and error in such a way that mobilities calculated using the stress–strain relationship of the PDL were consistent with those measured *in vivo* (Appendix Figure 1).¹

Appendix 2

Osipenko et al.² have provided the exact mathematical definition of the center of resistance (CR) and clarified the "principal" direction in the two-dimensional tooth movement produced by elastic deformation of the periodontal ligament (PDL). They defined the "principal" direction in the following sense: when a force is applied to the CR in the "principal" direction, the tooth translates in the same direction as the "principal" direction.

Based on the principal directions, tooth movement direction can be explained as shown in Appendix Figure 2. One of the principal directions is roughly the same as the tooth axis. The other principal direction is perpendicular to the tooth axis. When applying a transverse force F_1 to the CR in the principal direction, the tooth translates by δ_1 in the same direction of the force. This relationship is denoted as $F_1 = k_1 \delta_1$, where k_1 is the spring constant of the tooth supported with the PDL. In the same manner, a relationship between axial force F_2 and axial movement δ_2 is denoted as $F_2 = k_2 \delta_2$. The spring constants k_1 and k_2 in the principal directions depend on the elastic properties of the PDL.

When applying an arbitrary directional force F whose axial and transverse components are F_1 and F_2 , the tooth translates in the direction of $\delta_2/\delta_1 = (k_1/k_2)$ (F_2/F_1). In general, movement direction δ_2/δ_1 is not always equal to the force direction F_2/F_1 . It changes depending on the k_1/k_2 . If $k_1/k_2 = 1$, the movement direction becomes the same as the force direction, namely, $\delta_2/\delta_1 = F_2/F_1$.

When a horizontal force acts on the CR, the tooth translates horizontally at $k_1/k_2 = 1$, and an upward or downward translation occurs depending on whether $k_1/k_2 > 1$ or $k_1/k_2 < 1$, respectively.

REFERENCES

- 1. Goto T. [Experimental study in the physiological mobility of the tooth]. Shikwa Gakuho 1971;71:1415-44. Japanese.
- 2. Osipenko MA, Nyashin NY, Nyashin YI. Center of resistance and center of rotation of a tooth: the definitions, conditions of existence, properties. Russ J Biomech 1999;1:5-15.



Appendix Figure 1. Identification of stress–strain relation of the periodontal ligament (PDL). **A**, Piecewise linear stress–strain relation of the PDL. **B**, Finite element model of the maxillary right first premolar. **C**, Comparison of the initial tooth mobilities of the first premolar calculated using the piecewise linear relation by the finite element model with those measure *in vivo*. The red and blue circles indicate tooth movements in the bucco-lingual and axial direction, respectively. Data from the article of Goto. (Shikwa Gakuho 1971;71:1415-44).¹



Appendix Figure 2. Translational direction of tooth produced by a force acting on the center of resistance (CR). **A**, Translational movements in the principal directions. **B**, Movement direction $\delta_2/\delta_1 = (k_1/k_2) (F_2/F_1)$ produced by a force in arbitrary direction. **C**, Three types of translational movement produced by a horizontal force.

 δ , Displacement; F, force; k, spring constant, Suffix 1 and 2 indicate transverse and axial directions.