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# Enhanced thermal properties of poly(lactic acid)/MoS<sub>2</sub>/carbon nanotubes composites

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In this work, few-layered molybdenum disulfide ( $MoS_2$ ) was functionalized with metal oxide ( $M_xO_y$ ) nanoparticles which served as a catalyst for carbon nanotubes (CNT) growth in the chemical vapour deposition (CVD) process. The resulting  $MoS_2/M_xO_y$ /CNT functionalized nanomaterials were used for flame retarding application in poly(lactic acid) (PLA). The composites were extruded with a twinscrew extruder with different wt% loading of the nanomaterial. Full morphology characterization was performed, as well as detailed analysis of fire performance of the obtained composites in relation to pristine PLA and PLA containing an addition of the composites. The samples containing the addition of  $MoS_2/M_xO_y$ /CNT displayed up to over 90% decrease in carbon oxide (CO) emission during pyrolysis in respect to pristine PLA. Microscale combustion calorimetry testing revealed reduction of key parameters in comparison to pristine PLA. Laser flash analysis revealed an increase in thermal conductivity of composite samples reaching up to 65% over pristine PLA. These results prove that few-layered 2D nanomaterials such as  $MoS_2$  functionalized with CNT can be effectively used as flame retardance of PLA.

Greater use of conventional petroleum based commodity resins in various applications have led to inevitable rise of its ecological footprint. Various new eco-friendly biodegradable polymers were developed in order to counteract this effect. With its biodegradability, low emission of greenhouse gas and low production energy PLA currently stands as one of popular alternatives for conventional polymer materials<sup>1</sup>. Due to its high degree of transparency, good mechanical properties, low toxicity and ability to process using equipment as well as relatively low cost and large production volume it shows high potential for packaging, household and biomedical applications. Nevertheless, other potential applications such as in electronics or automotive industry require PLA grades with high impact strength, better processing ability and improved flame retardant behaviour<sup>2</sup>. In order to meet that demand novel methods of modification need to be developed and applied.

A common way of improving flame retardancy of polymer is through combining its matrix with flame retardant filler. In the past improved flame resistance was achieved by introduction of halogenated flame retardants (HFR). Nowadays, it faces severe restrictions in Europe and North America due to the release of toxic substances and large amounts of smoke during combustion<sup>3</sup>. Instead, halogen-free flame retardant formulations function more commonly now as an environmentally friendly alternatives for HFR. These include intumescent flame retardants<sup>4,5</sup>, phosphorus- and nitrogen-containing micro- and nanoparticles<sup>6-8</sup>, inorganic substances and silica derivatives<sup>9</sup> which can be used either individually or in combination<sup>10</sup> to achieve optimal flame retardant performance.

Polymer/layered inorganic materials composites have high potential for improving thermal properties of polymers. Molybdenum disulfide is a member of a family of transition metal dichalcogenides (TDM). Structurally its crystals are characterized as hexagonal layered configurations. Atoms in the layer are bonded with strong covalent bonding, while layers are packed together to form a sandwich structure with weak Van der Waals forces similarly to graphite or boron nitride<sup>11</sup>. With their unique electrical, optical, thermal and mechanical properties  $MoS_2$  nanosheets can be potentially used for application as fillers for improving properties of polymers. Being a representative of layered inorganic materials  $MoS_2$  is expected to disperse and exfoliate in polymers, which results in the physical barrier effects that inhibits the diffusion of heat and gaseous decomposition products<sup>12,13</sup>. Molybdenum, a transition metal element, promotes the formation of charred layer during the combustion which

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acts as a physical barrier that slows down the heat and mass transfer<sup>11</sup>. In order to achieve high-performance homogenous dispersion of  $MoS_2$  nanosheets in the polymer hosts and proper interfacial interactions need to be established<sup>14</sup>. Similarly to metal oxide/graphene hybrid materials addition of metal oxide/ $MoS_2$  nanoparticles might prevent the aggregation of  $MoS_2$  flakes during preparation of polymer nanocomposites and result in improved flame retardant performance<sup>15,16</sup>. In addition they can also lead to improved char generation due to catalytic activity of metal oxide as well as suppressed smoke production and reduced toxicity due to catalytic conversion of carbon oxide  $(CO)^{17}$ .

Another possible alternative to the use of conventional flame retardants are carbon nanotubes (CNT). These can be introduced into the polymer matrix in pristine form of a small diameter (1-2 nm) single-walled carbon nanotubes or a large diameter (10-100 nm) multi-walled carbon nanotubes (SWCNT and MWCNT, respectively)<sup>18-23</sup>. In addition to this functionalization of CNT can also be carried out in order to significantly improve the flame retardant performance<sup>17</sup>. This can be performed in three different ways. Surface modification by coupling agents allows for enhancement of dispersion state of CNT<sup>24-26</sup>. For example, addition of 9 wt% content of CNT functionalized with vinyltriethoxysilane into epoxy composite allowed for increase of limiting oxygen index (LOI) from 22 to 27% and improvement of UL-94 rating from V-1 to V-025. This also resulted in increase of char yield at 750 °C by 46.94%. Char yield can be also enhanced through covalent linkage of organic flame retardants to CNT<sup>27-30</sup> following surface treatment. Functionalization of CNT can facilitate their dispersion within the polymer matrix and enhance interfacial adhesion between the CNT and the polymer<sup>30</sup>. Formation of genuine composites can be confirmed by an increase in the Young's modulus and flame resistance of compositions containing pristine CNT<sup>28</sup>. Finally, hybridization of CNT by inorganic particles can allow for superior flame retardant properties<sup>31–33</sup>. In addition to that other key parameters, such as thermal stability and dielectric properties, can be also enhanced<sup>31</sup>. Generally speaking, flame retardant actions of CNT/polymer composites involve the condensed phase action. Char layer formed on the entire sample surface acts as insulation layer that reduces the amount of volatiles escaping to the flame. The formation of continuous layer is obtained by formation of three-dimensional network structure when the content of CNT reaches a threshold value<sup>17</sup>. Good quality char plays major role in reduction of peak heat release rate (pHRR)<sup>34,35</sup>.

During the scope of presented research few-layered  $MoS_2$  nanosheets functionalized with  $M_xO_y$  nanoparticles served as catalysts for growth of CNT in the CVD process were prepared. The obtained nanomaterials were used as flame retarding agents in PLA composites. Detailed description of synthesis, as well as full characteristics and analysis of properties of obtained PLA-based composites were provided. Additionally, a thorough analysis of thermal stability, fire performance and thermal conductivity of these materials was also performed and discussed in details.

### Methods

**Materials.** Bulk MoS<sub>2</sub> (powder), N-Methyl-2-pyrrolidone (NMP) (anhydrous, 99.5%), cobalt(II) acetate tetrahydrate (99%), iron(II) acetate (95%) and nickel(II) acetate tetrahydrate (98%) were purchased from Merck. PLA was obtained from Goodfellow. Hydrogen peroxide (30%) and ethanol (96%) were purchased from Chempur. Gaseous nitrogen and ethylene were purchased from Messer and Air Liquide, respectively.

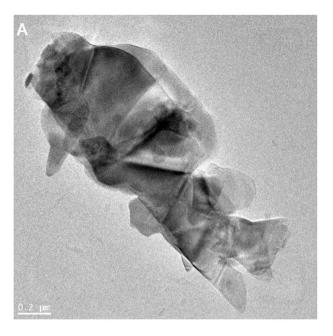
**Preparation of few-layered MoS\_2.** 1 g of bulk  $MoS_2$  powder was transferred into a 250 mL flat-bottomed beaker filled with solution of 95 mL of NMP and 5 mL of hydrogen peroxide. This was followed by 30 minutes of continuous sonication in an ultrasonic washer, after which solution was transferred to a 250 mL round bottomed flask, plugged to reflux and consciously stirred at 360 rpm and 35 °C for 24 h. Final dispersion was centrifuged four times at 10000 rpm for 20 minutes and washed with ethanol.

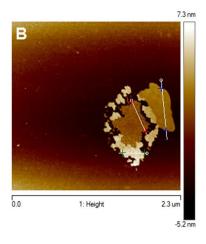
**Preparation of MoS**<sub>2</sub>/**M**<sub>x</sub>**O**<sub>y</sub>/**CNT.** In order to obtain MoS<sub>2</sub>/M<sub>x</sub>O<sub>y</sub>/CNT modified nanomaterials following procedure was applied. First, 150 mg of few-layered MoS<sub>2</sub> and 150 mg of respective source of metal oxide (cobalt(II) acetate tetrahydrate, iron(II) acetate or nickel(II) acetate tetrahydrate) were dispersed in ethanol and sonicated in an ultrasonic washer for 2 h. Next, dispersions were stirred for 48 h, after which they were dried under high vacuum at 440 °C for 3 h. This resulted respectively in MoS<sub>2</sub>/Co<sub>2</sub>O<sub>3</sub>, MoS<sub>2</sub>/Fe<sub>2</sub>O<sub>3</sub> and MoS<sub>2</sub>/Ni<sub>2</sub>O<sub>3</sub> modified nanomaterials. Next CVD was performed in tube furnace under constant 100 mLmin<sup>-1</sup> flow of nitrogen at 850 °C with a 15 minute long, 60 mLmin<sup>-1</sup> flow of ethylene as a source of carbon.

**Extrusion of MoS**<sub>2</sub>/M<sub>x</sub>O<sub>y</sub>/CNT modified PLA composites. PLA was utilized as a polymer matrix. Four composites were prepared, containing addition of few-layered MoS<sub>2</sub>, MoS<sub>2</sub>/Co<sub>2</sub>O<sub>3</sub>/CNT, MoS<sub>2</sub>/Fe<sub>2</sub>O<sub>3</sub>/CNT or MoS<sub>2</sub>/Ni<sub>2</sub>O<sub>3</sub>/CNT, respectively. For each composite three samples containing different amounts of nanomaterials additives were prepared -0.5 wt%, 1 wt% and 2 wt%, respectively. Following 12 h of drying the nanomaterial ware blended with PLA using twin-screw extruder (Zamak Mercator EHP 2 × 12). For reference a sample of pristine PLA was also extruded.

**Characterization.** Morphology of nanomaterials obtained during each stage was analyzed using transmission electron microscopy (TEM) (Tecnai F20, FEI) with 200 kV accelerating voltage. Raman analysis was performed in microscope mode (InVia, Renishaw) with a 785 nm laser in ambient air. Number of layers in few-layered MoS<sub>2</sub> samples was determined using atomic force microscopy (AFM) (MultiMode 8, Bruker).

For the obtained composites and pristine PLA following analyses were performed. Thermogravimetric analysis (TGA) was performed using thermal analyzer (SDT Q600, TA Instruments) under airflow of 100 mLmin<sup>-1</sup>. In each case individual sample (ca. 5 mg in an alumina crucible) was heated from room temperature to 800 °C at a linear heating rate of 10 °Cmin<sup>-1</sup>. In addition to this, gaseous products from the heating process were analyzed *in situ* with a mass spectrometer (ThermoStar, Pfeiffer Vacuum) coupled with the TGA, under 100 mLmin<sup>-1</sup> argon flow. Microscale combustion calorimetry (MCC) was employed for measurement of flame retardancy using FAA





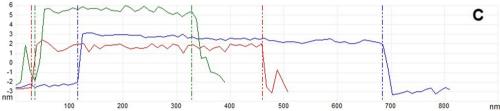


Figure 1. TEM (A), AFM (B) images of few-layered MoS<sub>2</sub> and analysis of height profile obtained from AFM (C).

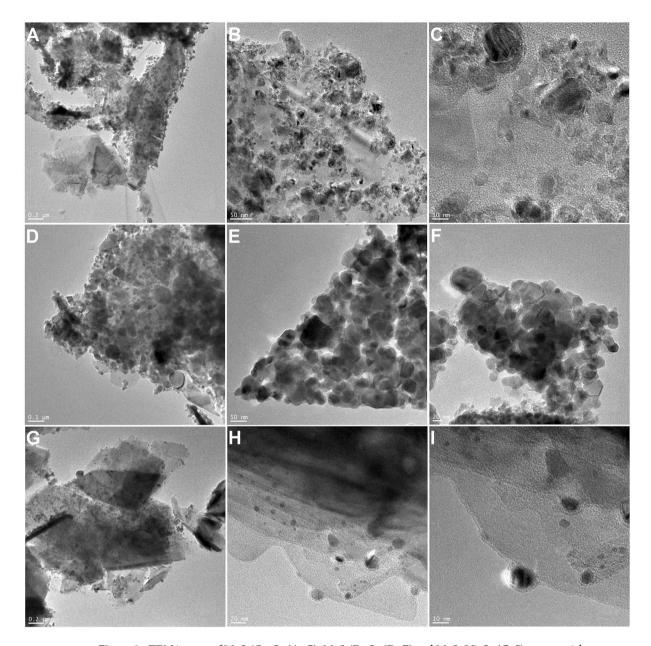
Micro Calorimeter, from FTT. This allowed for determination of pHHR, heat release capacity (HRC) and total heat release (THR) from 2 mg specimens. Thermal conductivity of the obtained samples was measured using laser flash apparatus (XFA 300, Linseis). Prior to this measurement the samples were spray coated with thin layer of graphite in order to facilitate the absorption of laser at the surface.

### **Results and Discussion**

Successful preparation of few-layered MoS<sub>2</sub> samples was confirmed using TEM and AFM (Fig. 1). Number of MoS<sub>2</sub> layers was determined through analysis of high profile with AFM (Fig. 1C). The flakes were typically 5 nm in height, which corresponded to approximately 7 layers of MoS<sub>2</sub> (assuming average thickness of single layer ca. 0.7 nm<sup>36</sup> (Dependence between lateral size and aspect ratio in Supplementary information)). This was verified later with Raman spectroscopy as the intensity of  $E_{2g}^1$  and  $A_{1g}$  peaks changes between bulk MoS<sub>2</sub> and few-layered MoS<sub>2</sub>. With the increased number of layers the frequency of  $E_{2g}^1$  (~382 cm<sup>-1</sup> for bulk MoS<sub>2</sub>) decreases while that of the  $A_{1g}$  (~407 cm<sup>-1</sup> for bulk MoS<sub>2</sub>) increases. This effect is caused by the interlayer van der Waals force in MoS<sub>2</sub> suppressing the atom vibration, which results in higher force constants<sup>36,37</sup>.

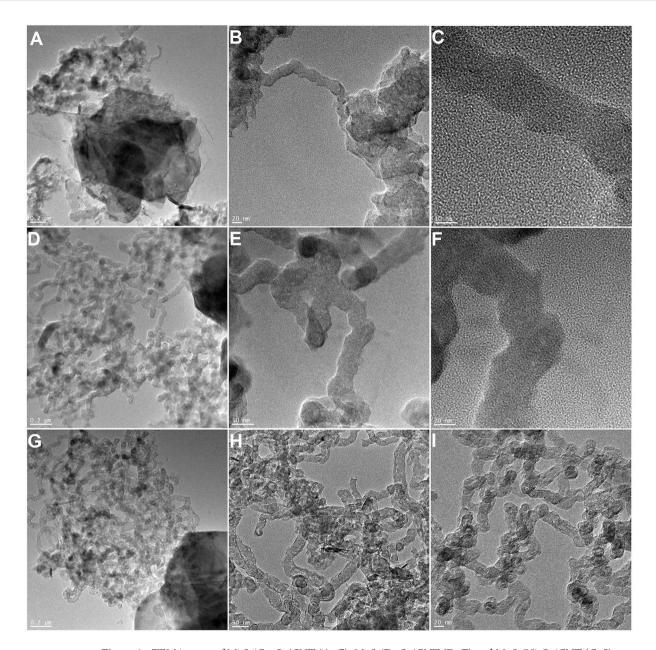
Dispersion of metal oxide nanoparticles on the surface of  $MoS_2$  was determined from collected high-resolution TEM images presented in Fig. 2. Metal oxide nanoparticles appeared to be well dispersed on the surface and deposited homogenously. The nanoparticles size was measured and ranged between 5 and 25 nm for all metal oxide nanoparticles. Presence of CNT on samples from the CVD process was confirmed with TEM (Fig. 3). As observed, internal diameter of nanotubes matched the diameter of specific metal oxide nanoparticles. Hallow core and an open end were visible and the surface appeared to be smooth.

**Thermal stability.** TGA measurements were performed in order to study the influence of  $MoS_2$  as well as  $MoS_2/M_xO_y/CNT$  nanomaterial on the thermal stability of PLA. Figure 4 presents the TGA curves for PLA/ $MoS_2$  and  $MoS_2/M_xO_y/CNT$  composites in comparison to pristine PLA. Based on accumulated data  $T_{10wt\%}$ ,  $T_{50wt\%}$  and  $T_{max}$  values (which represent temperatures at which 10%, 50% and maximum weight loss occur) were registered and displayed in Table 1. It can be observed that in case of PLA modified only by the addition of few-layered  $MoS_2$  (Fig. 4A) at loading of 0.5 wt% thermal decomposition proceeded at a slightly higher rate in comparison to pristine PLA, suggesting accelerated decomposition of polymer matrix as a result of flame retardant (FR) condensed phase action, which affected flow of the polymer  $^{38}$ . As recorded in this case  $T_{10wt\%}$  value was lowered and was equal to  $306\,^{\circ}\text{C}$ - it was  $18\,^{\circ}\text{C}$  below that of a pristine PLA. In addition to this, further reduction in  $T_{50wt\%}$  and  $T_{max}$  values in comparison to pristine PLA was also observed for this sample. In case of samples



**Figure 2.** TEM images of MoS<sub>2</sub>/Co<sub>2</sub>O<sub>3</sub> (**A-C**), MoS<sub>2</sub>/Fe<sub>2</sub>O<sub>3</sub> (**D-F**) and MoS<sub>2</sub>/Ni<sub>2</sub>O<sub>3</sub> (**G-I**) nanoparticles.

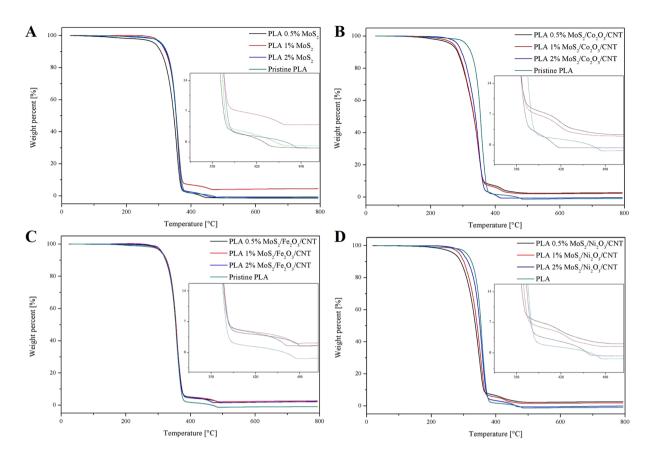
containing 1 wt% and 2 wt% of loading of few-layered MoS2 only Tmax was strongly affected which suggested that in both cases decomposition of polymer matrix proceeded at a normal rate in initial stages and stopped at a lower temperature. Therefore, it appears that addition of few-layered MoS2 nanoparticles has resulted in disruption of heat and gas diffusion. This effect was dependant on the FR load, as well as quality of dispersion in the polymer matrix. Combined with barrier effect, which limited access to fuel, it has caused the combustion process to finish at lower temperature. For samples containing addition of MoS<sub>2</sub>/Co<sub>2</sub>O<sub>3</sub>/CNT (Fig. 4B) a significant decrease in every recorded value was observed.  $T_{10wt\%}$  values were lowered by up to 40 °C for sample containing 0.5 wt% load of FR. T<sub>50wt%</sub> values were as much as 20 °C below that of pristine PLA for samples containing 0.5 wt% and 1 wt% FR load. Highest reduction in T<sub>max</sub> value was observed for sample containing 2 wt% load of FR and was 65 °C below that of pristine PLA. It appears that accelerated decomposition of the PLA matrix was caused by condensed action of the MoS<sub>2</sub>/Co<sub>2</sub>O<sub>3</sub>/CNT<sup>38</sup>. This resulted in pronounced flow of the polymer and its withdrawal from the sphere of influence. Change in melt-flow properties was confirmed during the preparation of samples for thermal conductivity testing. Composite samples needed to be preheated to glass transition temperature (about 150 °C) to form tablets using a table press. In case of PLA containing addition of MoS<sub>2</sub>/Co<sub>2</sub>O<sub>3</sub>/CNT the glass transition temperature appeared to be significantly lower (equal to about 110 °C) in comparison to another samples. In literature it was reported that poly(lactic acid) and poly(methyl methacrylate) (PMMA) blends containing addition of isopropylated triaryl phosphate ester flame retardant displayed accelerated breakdown of polymer during the TGA testing, combined with accelerated melt dripping during the UL-94 rating testing, favouring the melt-flow



**Figure 3.** TEM images of  $MoS_2/Co_2O_3/CNT$  (**A–C**),  $MoS_2/Fe_2O_3/CNT$  (**D–F**) and  $MoS_2/Ni_2O_3/CNT$  (**G–I**) nanoparticles.

drip mode of extinguishment³. As result of this, PLA/PMMA/FR blends have achieved V-0 classification in the UL-94 test³. In case of  $MoS_2/Fe_2O_3/CNT$  (Fig. 4C) only a significant reduction in  $T_{max}$  value was observed, which was highest (14 °C) for sample containing 2 wt% of nanomaterial, while the largest amount of charred reside was observed with sample containing 1 wt%. Recorded  $T_{10wt\%}$  and  $T_{50wt\%}$  values remained within the range of temperatures observed for pristine PLA. The composite samples containing addition of  $MoS_2/Ni_2O_3/CNT$  (Fig. 4D) placed between those derived from  $Co_2O_3$  and  $Fe_2O_3$  nanoparticles – at lower FR loads polymer decomposition was accelerated but the stability of matrix increased with wt% of FR. In summary, obtained results suggest improved fire resistant performance due to disruption of heat and gas transfer within the composites, as well as barrier effect introduced through the addition of  $MoS_2$  and CNT.

CO content analysis performed with use of mass spectrometry during the TGA pyrolysis cycle in argon atmosphere revealed promising results. In each case the amount of CO released was lower in comparison to that observed for pristine PLA (Fig. 5). For PLA modified only with addition of few-layered MoS $_2$  (Fig. 5A) the reduction in CO release ranged from 38 up to 70%, with the highest value recorded for sample containing 1 wt% of nanomaterials which also corresponded to the largest recorded charred residue value. Previously we observed that introduction of few-layered MoS $_2$  into the poly(vinyl alcohol) (PVA) composite resulted in significant decrease (up to 94%) in permeability of hydrogen gas in comparison to pristine PVA $^{39}$ . This effect was attributed to the incorporation of impermeable MoS $_2$  nanosheets with high aspect ratio. As a result a high number



**Figure 4.** TGA curves of PLA composites in comparison to pristine PLA.

	FR load [wt%]	T <sub>10wt%</sub> [°C]	T <sub>50wt%</sub> [°C]	T <sub>max</sub> [°C]
PLA	-	324	354	485
FLA	0.5	306	346	445
	1	320	351	459
PLA MoS <sub>2</sub>	2	322	353	465
	0.5	284	334	496
PLA MoS <sub>2</sub> /Co <sub>2</sub> O <sub>3</sub> /CNT	1	286	334	488
	2	295	339	420
	0.5	326	354	491
	1	326	356	483
PLA MoS <sub>2</sub> /Fe <sub>2</sub> O <sub>3</sub> /CNT	2	323	354	469
	0.5	291	337	493
PLA MoS <sub>2</sub> /Ni <sub>2</sub> O <sub>3</sub> /CNT	1	301	342	480
I LA WOO2/ NI <sub>2</sub> O <sub>3</sub> / CN I	2	314	351	468

Table 1. Summary of TGA results for PLA and PLA composites.

of tortuous pathways was created which restricted the diffusion of penetrants, such as  $H_2$  or  $CO^{39,40}$ . Reduction of CO emission during pyrolysis was further enhanced in case of  $MoS_2/M_xO_y/CNT$  composites. Highest reduction of CO emission in respect to pristine PLA was observed for all samples containing  $MoS_2/Fe_2O_3/CNT$  (Fig. 5C), and it was always above 90%. This was attributed to a well developed and thermally stable char barrier, which protected the molten zone from the burning zone, as reported by Attia *et al.*<sup>41</sup> in case of polystyrene composites containing addition of MWCNT.

**Flammability studies.** Fire performance testing was conducted using MCC, which allowed for laboratory evaluation of fire resistant properties of composites. Examples of heat release rate curves of prepared composites were presented in Fig. 6. Average values for key parameters - pHRR, HRC and THR were calculated from three measurements for each sample and presented in Table 2. All of these values were lowered for samples containing the addition of FR in comparison to pristine PLA. The samples containing an addition of MoS<sub>2</sub> (Fig. 6A) showed

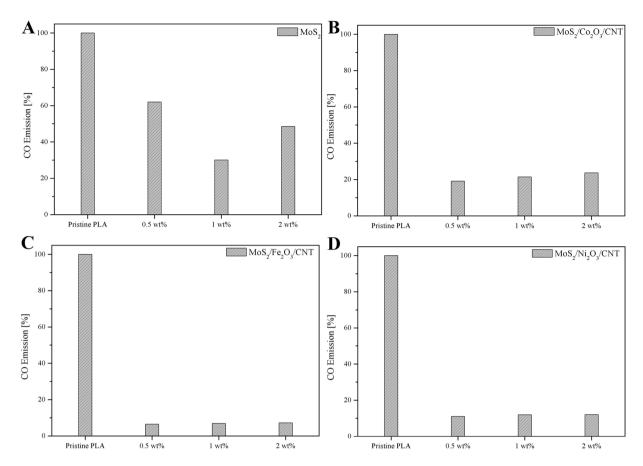


Figure 5. CO emission of PLA composites in comparison to pristine PLA.

satisfying FR performance with significant decrease of pHRR and THR values in comparison to pristine PLA. Therefore, it was evident that the addition of MoS<sub>2</sub> into the PLA matrix introduced the barrier effect which effectively impeded oxygen filtration, heat and mass transmission and the release of combustible gases produced during the combustion process, as previously reported for PVA, polystyrene (PS) and PMMA<sup>11,42,43</sup>. Formation of this barrier prevented underlying material from further combustion. For composite samples containing addition of MoS<sub>2</sub>/M<sub>x</sub>O<sub>y</sub>/CNT FR best results were observed for 2 wt% load. This effect could be attributed to strong barrier effect due to formation of an enhanced char layer thanks to the presence of CNT<sup>21,44</sup>. In case of samples containing addition of MoS<sub>2</sub>/Co<sub>2</sub>O<sub>3</sub>/CNT (Fig. 6B) and MoS<sub>2</sub>/Ni<sub>2</sub>O<sub>3</sub>/CNT (Fig. 6D) there was a visible shoulder within the temperature range of 250-350 °C. This suggested occurrence of an overlapping stage, preceding main combustion of PLA. This may be attributed to the release of FR additive via vaporisation or cleavage. In addition, a secondary peak was also observed for those samples within the temperature range of 425-515 °C which could be attributed to the increase in volume of sample due to intumescence. The intensity of this peak decreased with increase in FR loading, which suggests that rigidity of the barrier was directly tied to the FR contents and it is optimal at 2 wt%. While both of the effects could be also observed for samples containing addition of MoS<sub>2</sub> as well as MoS<sub>2</sub>/Fe<sub>2</sub>O<sub>3</sub>/CNT (Fig. 6C), the size of the before mentioned shoulder as well as intensity of the secondary peak were much lower.

**Thermal conductivity.** In order to verify thermal conductivity of obtained composites samples with a diameter of 12.7 mm were prepared using tablet press. For each composite a batch of 3 tablets were prepared. Thickness of each tablet was measured and recorded. In order to facilitate laser adsorption at the surface all tablets were covered with a thin layer of graphite prior to measurement. Tests were carried out at room temperature, which was measured at 25.4 °C. Obtained data (average out of 3 tablets for each composite) was presented in Table 3. In case of samples prepared with addition of only few-layered MoS<sub>2</sub> highest level of thermal conductivity – 0.502 Wm<sup>-1</sup>K<sup>-1</sup> was observed for sample containing addition of 2 wt% of FR and it was 54% higher than that of a pristine PLA sample. Similar effects were reported in literature for epoxy samples containing addition of nanomaterial such as graphene oxide or graphene nanosheets<sup>45</sup>. For samples containing CNT based structures thermal conductivity increased with increase in loading, resulting in up to 0.538 Wm<sup>-1</sup>K<sup>-1</sup> or a 65% increase over pristine PLA in case of a sample containing 2 wt% of MoS<sub>2</sub>/Fe<sub>2</sub>O<sub>3</sub>/CNT. It is however worth noting that even in case of 0.5 wt% of MoS<sub>2</sub>/Ni<sub>2</sub>O<sub>3</sub>/CNT a 50.9% increase in thermal conductivity was observed. Kashiwagi *et al.* also observed similar increase in thermal conductivity in case of polypropylene composites containing addition of carbon nanotubes which suggests that further enhancement of thermal conductivity of CNT based composites could be attributed to their presence<sup>46</sup>.

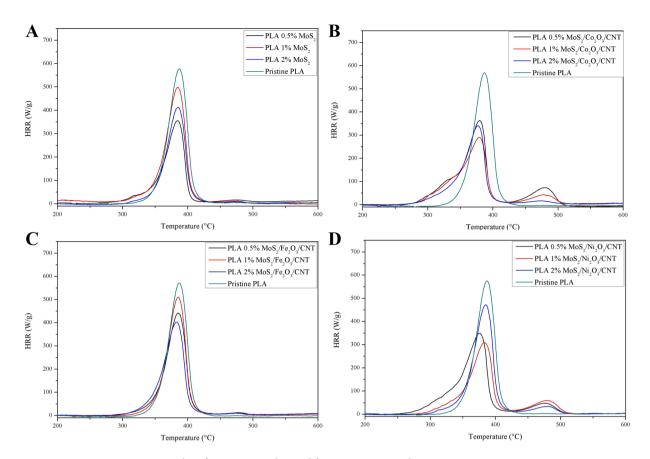


Figure 6. Examples of HRR curves obtained for pristine PLA and PLA composites.

	FR load [wt%]	HRC [Jg <sup>-1</sup> K <sup>-1</sup> ]	pHRR [Wg <sup>-1</sup> ]	THR [kJg <sup>-1</sup> ]
PLA	_	703.6	558.3	22.1
PLA	0.5	555.2 395.9	16.6	
	1	618.9	476.3	18.8
PLA MoS <sub>2</sub>	2	602.6	468.6	17.9
	0.5	560.2	337.1	21.6
PLA MoS <sub>2</sub> /Co <sub>2</sub> O <sub>3</sub> /CNT	1	571.3	332.1	20.4
	2	565.4	318.7	19.1
	0.5	621.6	483.7	19.6
PLA MoS <sub>2</sub> /Fe <sub>2</sub> O <sub>3</sub> /CNT	1	607.2	471.6	18.7
	2	595.9	449.5	17.9
	0.5	550.2	375.2	21.1
DI A M C DI O IONTE	1	548.2	363.3	20.2
PLA MoS <sub>2</sub> /Ni <sub>2</sub> O <sub>3</sub> /CNT	2	543.3	330.8	19.8

**Table 2.** MCC combustion data of PLA and PLA composites.

### **Conclusions**

In this work, in order to improve fire performance of PLA, few-layered MoS $_2$  and MoS $_2$ /M $_x$ O $_y$ /CNT nanomaterials were prepared and introduced into the PLA composites through twin-screw extrusion blending process. TGA analysis revealed 40 °C and 65 °C decrease of  $T_{max}$  value for samples containing 0.5 wt% of few-layered MoS $_2$  and 2 wt% of MoS $_2$ /Co $_2$ O $_3$ /CNT, respectively. Thanks to the addition of few-layered MoS $_2$  a formation of charred residue layer was observed which allowed for up to nearly 70% decrease in CO emission during burning in case of a sample containing 1 wt% of MoS $_2$ . Over 90% of reduction in CO emission was achieved through introduction of MoS $_2$ /Fe $_2$ O $_3$ /CNT into the PLA matrix. MCC analysis showed best performance of few-layered MoS $_2$  and MoS $_2$ /Fe $_2$ O $_3$ /CNT composites, while MoS $_2$ /Co $_2$ O $_3$ /CNT and MoS $_2$ /Ni $_2$ O $_3$ /CNT composites displayed strong effects of secondary stage preceding the main combustion of PLA as well as instability of barrier at 0.5 wt% and 1 wt% of FR. Thermal conductivity of all of the composites was increased in comparison to pristine PLA, up to 65% in

	FR load [wt%]	Thermal conductivity [W m <sup>-1</sup> K <sup>-1</sup> ]	Increase from pristine PLA [%]
PLA	_	0.326	
FLA	0.5	0.365	12.0
PLA MoS <sub>2</sub>	1	0.421	29.1
	2	0.502	54.0
	0.5	0.341	4.6
PLA MoS <sub>2</sub> /Co <sub>2</sub> O <sub>3</sub> /CNT	1	0.392	20.2
	2	0.465	42.6
	0.5	0.466	42.9
PLA MoS <sub>2</sub> /Fe <sub>2</sub> O <sub>3</sub> /CNT	1	0.487	49.4
	2	0.538	65.0
	0.5	0.492	50.9
PLA MoS <sub>2</sub> /Ni <sub>2</sub> O <sub>3</sub> /CNT	1	0.500	53.4
	2	0.510	56.4

**Table 3.** Thermal conductivity of PLA and PLA composites.

case of a composite containing addition of 2 wt% of  $MoS_2/Fe_2O_3/CNT$  due to the presence of CNT. In conclusion, introduction of few-layered  $MoS_2$  and CNT functionalized  $MoS_2$  nanomaterials shows good potential for reduction of fire hazard of the PLA, which could prove beneficial for academic research and practical applications.

# Data availability

The datasets used and/or analysed during the current study are available from the corresponding author on reasonable request.

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# **Author contributions**

P.H. prepared all of the samples, gathered, analyzed and interpreted the data and was a major contributor in writing the manuscript. E.M. helped with interpretation of data and writing of the manuscript. K.W. prepared TEM images, TGA, XRD and Raman spectroscopy data. All authors read and approved the final manuscript.

### Competing interests

The authors declare no competing interests.

## Additional information

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