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Highly Strong and Elastic Graphene Fibres Prepared from Universal Graphene Oxide Precursors

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Graphene fibres are continuously prepared from universal graphene oxide precursors by a novel hydrogel-assisted spinning method. With assistance of a rolling process, meters of ribbon-like GFs, or GRs with improved conductivity, tensile strength, and a long-range ordered compact layer structure are successfully obtained. Furthermore, we refined our spinning process to obtained elastic GRs with a mixing microstructure and exceptional elasticity, which may provide a platform for electronic skins and wearable electronics, sensors, and energy devices.

raphene is a single-atom-thick two-dimensional (2D) material, comprised of a monolayer of hexagonally arranged sp²-hybridized C atoms. It has received much interest, because of its high electron mobility, thermal conductivity, elasticity, and stiffness¹⁻⁵. These properties make graphene attractive for application in nanoelectronic devices, sensors, functional composites, and energy storage. To maximize the practical application of graphene, it is important to integrate individual graphene nanosheets into ordered macroscopic materials. Nowadays, graphene sheets can be easily assembled into macroscopic papers and films⁶⁻⁸. The poor dispersibility of pristine graphene in common solvents and the variable layer-by-layer stacking of graphene sheets have also been overcome to prepare ordered graphene fibres (GFs)⁹⁻¹¹. Several methods have been reported to prepare ordered GFs, such as hydrothermal strategies and wet spinning of a concentrated graphene oxide (GO) liquid crystal solution. However, the electrical conductivity and mechanical strength of the as-obtained GFs are unsatisfactory for practical applications in lightweight chemical supercapacitors, sensors, stretchable electronics and other energy devices¹²⁻¹⁶. Size selection of GO sheets, Ag doping, and thermal treatment of GFs have been probed to prepare highly ordered and reduced GFs, in an attempt to improve GFs' electrical and mechanical properties¹⁷⁻²⁰. However, these methods are complex and costly. Additionally, the stretching properties of the asobtained GFs remain inferior to those of conventional organic fibers²¹⁻²³. Therefore, developing a straightforward and effective method for improving GFs' performance is still desirable.

In this study, we controlled the GFs microstructure without enhancers or selection of large graphene sheet sizes, and greatly improved the GFs properties. A self-assembly method was used to prepare the GFs. With assistance of a rolling machine, we further fabricated ribbon-like GFs, or graphene ribbons (GRs), with a long-range ordered compact layer structure. The electrical conductivity and tensile strength of GRs were both enhanced compared to those of GFs. Elastic GRs (EGRs) with high ultimate failure strain can also be obtained. Our processes provide a new approach to prepare pure graphene-based fibres with enhanced performance, and new opportunities for their applications in flexible and stretchable nanoelectronics, such as wearable electronics and energy devices.

To prepare GFs, GO fibres (GOFs) were firstly prepared by spinning a GO hydrogel, as shown schematically in Fig. 1a. GO suspensions (Supplementary Fig. S1a online) were mixed with sodium deoxycholate (NaDC). The obtained NaDC-functionalized GO sheets dispersed well in a NaDC-hydrated matrix and formed a spinnable supramolecular hydrogel (Supplementary Fig. S1b online). When the spun GO hydrogel was immersed in ethanol, NaDC dissolved and the GO sheets assembled to form a GOF due to van der Waals interactions. Spinning a 30 mg/mL aqueous GO suspension containing a desired ratio of NaDC (5–9%, weight-_{NaDC}/weight-_{water}) yielded continuous fibers. This spinning process is shown in Supplementary Movie S1 online. Meter lengths of



Figure 1 | (a) Schematic diagram of GOF fabrication. (b) Photograph of 3m-long GFs wound on a drum (diameter, 4 cm). (c) and (d) FE-SEM images of top and cross-section view of a GF, respectively. (e) High magnification FE-SEM image of cross-section view of a GF. Scale bars: 50 μ m, 20 μ m and 10 μ m, respectively. Figures were drawn by Guoji Huang.

GOFs with tunable diameters (10–60 μ m) were prepared using polytetrafluoroethylene (PTFE) pipelines with different diameters. Finally, GOFs were reduced to GFs after being treated with HI. Meters of GFs can be prepared through above processes (Fig. 1b). The Fourier transform infrared spectra, Raman spectra, and X-ray diffraction (XRD) patterns of NaDC, GO hydrogel, GOFs, and GFs are shown in Supplementary Fig. S2 online. Both dissolution of NaDC and reduction of GO could be confirmed by the spectroscopic results^{24–27}.

Results

The morphology and structure of GFs were analyzed by field emission-scanning electron microscopy (FE-SEM). In GFs, graphene sheets were densely stacked and largely aligned to the fiber axis, which is similar to previously reported graphene fibres^{9,28}. This is attributed to the flowing GO hydrogel and the effect of the PTFE pipeline or capillary-induced shear force induced in wet spinning. GFs did not break during their knotting into a loop (Supplementary Fig. S3 online), demonstrating an excellent flexibility compared to CNT fibers²⁹⁻³¹. The high-resolution cross-sectional FE-SEM image of GFs clearly shows that reduced GO sheets assembled randomly in GFs (Fig. 1c-e). The mean measured electrical conductivity of GFs reaches 3.08×10^4 S/m. A typical stress strain curve is shown in Fig. 2b. The mean experimentally determined tensile strength and elongation to break of the GF sample with best electrical properties are 238 MPa and 2%, respectively. The high tensile strength could be attributed to the directionally aligned structure and strong interactions between stacked reduced GO sheets. The tensile strength is

higher than that of neat wet-spun single-walled CNT fibers (50– 150 MPa) and GFs fabricated by other methods^{9–11,32,33}. The average density of GFs was measured as 1.7960 g/cm³, as a consequence, the specific strength and the average specific conductivity of the GFs is up to 132 kN·m/kg and 16 S·m²/kg, respectively.

Based on the supramolecular hydrogel-assisted spinning method, we next fabricated GRs, or ribbon-like GFs, with assistance of a double roller crusher. During this process, a geometric confinement was induced by rolling, which leaded to long-range ordered structures of GRs. A schematic of the fabrication process is shown in Fig. 2a.

The length of PTFE pipeline (internal/external diameter of 300/ 700 μ m) containing GO hydrogel was pressed in the double-roller crusher. GO hydrogel was subsequently released into a 95 wt% ethanol solution to dissolve the NaDC and yield a GOF with layered structure. After drying and reduction, 1.5 m-long GRs with a uniform spiral structure were obtained (Fig. 2c). The thickness of GRs could be turned (0.5–2.5 μ m) through adjusting the distance between the two rollers (300–400 μ m). Raman spectra and XRD patterns of the resulting GRs are shown in Supplementary Fig. S2 online.

FE-SEM was used to characterize fibre samples. Fig. 2d demonstrates good flexibility of GRs, which is comparable to that of GFs. Surface of GRs is much more smooth than that of GFs (Fig. 2e), which could be attributed to the ordered reduced GO layers in GRs. This structure is confirmed by cross-sectional images shown in Fig. 2f-h. These compact layers are mainly attributed to the shear flow of the GO hydrogel, which arose from the double-roller crusher. The mechanism can be explained as follows: The GO hydrogel was injected into the PTFE pipeline at a certain rate, and GO sheets with a lamellar structure were interconnected to form a partially ordered structure along the axial direction^{9,17,34-36}; subsequently, the PTFE pipeline containing GO hydrogel was pressed by the double-roller crusher, GO sheets were further rearranged as a result of the continuous compression force. Rounded fibers with a partially ordered structure (Fig. 1d) were then pressed into ribbon-like ones with a long-range ordered compact layer structure (Fig. 2f).

The GRs have a mean experimentally determined electronic conductivity of 5.7×10^4 S/m and a tensile strength of 404 MPa (Fig. 2b), which are about two times larger than those of our GFs, and are comparable to those of previously reported GFs (see Supplementary Table S1 online). In addition, the average density (1.8355 g/cm³), specific strength (220 kN·m/kg) and specific conductivity (32 S·m²/kg) of GRs are also higher than those of GFs. The above results indicate that ordered structure could remarkably improve the electrical and mechanical properties of GFs. However, their ultimate strain (2.25%) maintains at the same level as previous GFs, which is still the weakness of nowadays GF products.

Next, we refined the GR manufacturing process to obtain elastic GRs. During the synthesis of GRs, after rolling, we reduced the ribbon-like GOFs before drying. Water molecules in wet GOFs gave space for movement of GO sheets to unregularly restack in the reduction reaction. Partially disordered structure was thus randomly formed. Fig. 3a shows the deformation of EGRs with an original length of about 10 cm. The elastic fibre could be stretched to about 18 cm without breakage. After relaxation, it retracted immediately. Supplementary Movie S2 online shows this process. In the video, it is clearly seen that the EGRs behaved like a spring. We believe that the key factor which makes GRs elastic is the partially disordered "defects" induced in their ordered layer structure. They could lead to non-uniform shrink in the thickness direction of the fibre during drying, which twisted the GRs (see Fig. 3b and 3c). With mixing microstructures of GFs and GRs (Fig. 3d and 3e), EGRs had similar spectroscopic features to them (Supplementary Fig. S2 online). The mean measured tensile strength and conductivity of EGRs reaches 102 MPa (Fig. 4a) and 3.55×10^4 S/m (Fig. 4b inset, black line),



Figure 2 | (a) Schematic showing the fabrication of GRs and EGRs. Process (1) involves drying followed by reduction of the layered GOF structure to GRs, and (2) involves the reduction of the layered GOF structure, and then drying to yield EGRs. (b) Stress-strain curves of the GFs (black) and GRs (red). (c) Photograph of 1.5-m-long GRs wound on a drum (diameter, 4 cm). FE-SEM images of (d) a tightened knot, (e) surface morphology, and (f) cross-sectional morphology of GRs. (g) and (h) are high-magnification images of (c). Scare bars: 1 mm, 50 μ m, 2 μ m and 500 nm, respectively. Figures were drawn by Guoji Huang.

respectively. The average density of EGRs is 1.5420 g/cm³. The low density could be attributed to the partially disordered "defects" structure, which leads to a relatively lower specific strength (66 kN·m/kg) and specific conductivity (22 S·m²/kg) compared to those of GRs. We further investigated the electrical resistance (R) during stretching. As shown in Fig. 4b, the electrical resistance of our EGR remained stable during the stretching and recovery process. Typical I–V curves of the EGR before (black) and after (red) stretching were overlapped (Fig. 4b inset). This differs from traditional materials whose resistances are greatly influenced by their shape.

Furthermore, it is worth noting that the ultimate strain of EGRs is as high as 85%, more than 6 times larger than the best result ever reported³⁷. Fig. 4c presents cyclic stress–strain curves for the overall elastic property of the EGR. The fibre was stretched by the two ends with different predefined tensile strain from 10% to 70% for this measurement. The EGR shows a typical elastomeric behavior at $\varepsilon \leq$ 50%. Residual strain appears at higher strains ($\varepsilon \geq$ 60%). These results are similar to those of the elastomeric fibre mat reported in ref. 38. Additionally, we further studied its elastic property by stretching it to a predefined strain ($\varepsilon =$ 50%) for 1, 50 and 100 loading and



Figure 3 | (a) Stretching of EGRs from their initial length to a maximum and releasing to free state. FE-SEM images of (b) surface and (c) fracture dregion of an EGR, respectively. (d) and (e) High-magnification images of (c). Scare bars: 200 μ m, 50 μ m, 5 μ m and 2 μ m, respectively.



Figure 4 | (a) The stress-strain curve of an EGR. (b) Relative resistance changes ($\Delta R/R_0$) of a 4-cm-long EGR during stretching process (black) and recovery process (red), inset shows typical I–V curves of the EGR before (black) and after (red) stretching, they are overlapped. (c) Cyclic stress–strain curves of the EGRs within different strain of 10%–70%. (d) Elastic stretching of the EGR within a strain of 50% (selected cycle 1th, 50th, and 100th are plotted).

unloading cycles. The corresponding cyclic stress-strain curves were showed in Fig. 4d. The result indicates that the elastic stretching remained stable and showed a negligible variation after 100 cycles. The good elastic property of the EGR at room temperature could be attributed to the mixing of disordered "defects" and ordered layer structure, and might be further improved by optimization of the fabrication process. The EGRs exhibited high electronic conductivity, tensile strength, and ultimate strain. Therefore we suppose that they may provide a platform for electronic skins and wearable electronics, sensors, and energy devices.

Discussion

The electrical and mechanical properties of the GFs, GRs, and EGRs could potentially be further improved by optimizing the initial GO/

NaDC ratio in hydrogel precursors. The effects of NaDC content (5–9%) on tensile strength, ultimate failure strain, and electrical conductivity of our graphene-based fibres are shown in Fig. 5 a–c. The most strong and conductive samples were found to be GRs with 8% and 7% initial NaDC content, respectively. EGRs exhibited best elasticity (ultimate strain ~90%) at 9% initial NaDC content. Based on above results, we believe that there are still rooms for improvement in elastic behaviors of graphene-based fibres. The next grant challenge could be assembly of GO sheets into complex and control-lable structures.

In conclusion, we reported a hydrogel-assisted spinning method for fabricating GFs with favorable electrical and mechanical properties. A double-roller crusher was further used to create GRs and EGRs with a long-range ordered structure, to improve the electrical



Figure 5 | Effects of NaDC content on (a) tensile strength, (b) failure strain, and (c) electrical conductivity of GFs (black), GRs (red), and EGRs (blue). Error bars are the s.d. calculated from repeated measurements.

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and mechanical properties. The rigidity and elasticity of these ribbons could be tuned by controlling the microscopic structure in preparation. EGRs with high elasticity and elastic recovery, as well as enhanced electrical properties were prepared. The electrical resistance of the EGRs does not change during stretching. The GFs, GRs, and EGRs have great potential in flexible/wearable sensors and energy devices.

Methods

Synthesis of GO and GO hydrogel. GO was synthesized using the Hummers' method. Typically, natural flake graphite powder (3 g) was added to 0°C 98% sulfuric acid (69 mL) in a 500-mL flask. KMnO₄ (9 g) was gradually added while cooling and stirring in an ice bath. The mixture was stirred at 35°C for 2 h. Distilled water (138 mL) was slowly added, and the temperature was maintained at <100°C for 15 min. The mixture was then poured slowly into 30% H₂O₂ solution (520 mL). The product was filtered with 10% aqueous HCl (750 mL) to remove metal ions, and was thoroughly diluted with distilled water during filtering. The brown-yellow powder of GO was dried for hybrid preparation. GO hydrogel was synthesized by mixing an aqueous 30 mg/mL GO suspension and NaDC, in the desired ratio in water (5–9%). The mixture was magnetically stirred for 24 h, during which time the gel formed.

Fabrication of GOFs, GFs, GRs, and EGRs. GO hydrogel was loaded into a plastic syringe and injected into ethanol at a rate of 20 mL/h, to remove NaDC. After washing with ethanol, GOFs were collected onto the drum, and dried at 60°C for 12 h. Dried GOFs were immersed in aqueous 40% HI for 2 h at room-temperature, followed by washing with ethanol and water, and vacuum drying at 80°C for 12 h to obtain GFs. The GO hydrogel was injected into the PTFE pipeline (inner/external diameter of 300/700 μ m). Then the pipeline was pressed in a double-roller crusher and GO hydrogel was squeezed out into ethanol. The layered GOF structure was obtained. It was subsequently either dried and chemically reduced, or chemically reduced and then dried. Finally, the GRs and EGRs were obtained and collected on drums.

Characterizations and measurements. The morphologies of the as-prepared products were determined at 5.0 kV using a JSM-6700F field emission scanning electron microscopy (FESEM). The electrical resistance of the as-prepared products was measured using a two-probe method by a Zahner electrochemical workstation (Zennium CIMPS-1). Conductivity was calculated based on the length L, area A and resistance R using the formula, conductivity = $L/(R^*A)$. Area, A (calculated by the grid method) of each sample was an average based on the measurements at 3-5 different locations along the fiber's long axis direction. Mechanical property tests of as-prepared products were conducted with an Instron material testing system (Instron 5969) at a strain rate of 1 and 40 mm/min. The densities of as-prepared products were measured as follow: Tetrabromoethane (Br2CHCHBr2) and carbon tetrachloride (CCl₄) were mixed in a certain proportion to ensure that the as-prepared samples suspended uniformly in the mixture for at least 4 h at 20°C. The density of the mixture, and hence the sample density, was measured using a PZ-B-5 liquid specific gravity balance. Unless otherwise stated, all values were determined from samples with 8% NaDC content.

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Author contributions

Y.L. and H.W. designed and directed the study. G.H., C.H. and M.Z. performed the experiments. G.H., C.H., Y.S., M.Z. and H.W. wrote the main manuscript text. M.Z., Q.Z. and Y.L. prepared figures. All authors reviewed the manuscript.

Additional information

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