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# Efficient Separation of Acetylene-Containing Mixtures Using ZIF-8 Membranes

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# separation is related to thermodynamic factors. It is worth noting that this is the first example of MOF membranes to successfully separate $C_2H_2$ from $CH_4$ and $CO_2$ .

# INTRODUCTION

As one of the most important chemical raw materials, acetylene is produced from natural gas by methane coupling at high temperatures<sup>1</sup> so that methane is inevitably mixed in acetylene. The purification of methane-containing acetylene gas in industry relies on the use liquid adsorbents, such as Nmethylpyrrolidone, in a multistage shower column.<sup>2,3</sup> It is a process that requires complex solvent circulation and additional flash vaporization to desorb the dissolved acetylene, which needs large-scale equipment and increases energy consumption.<sup>4</sup> In addition, owing to the same fluid properties of acetylene and CO<sub>2</sub>, the efficient separation of  $C_2H_2/CO_2$ mixtures is another technologically interesting issue. Therefore, a more efficient and rapid purification of acetylene gas is of great importance in optimizing the acetylene production process, increasing production efficiency, and reducing energy consumption and operating costs.

Recently, the emerging microporous metal-organic frameworks (MOFs)-based 5-10 physical adsorbents are promising as cost-effective and efficient materials for C2H2 mixture separation. Several MOFs have exhibited high separation capacities and selectivity for  $C_2H_2/CH_4^{11,12}$  and  $C_2H_2/$ CO<sub>2</sub><sup>11,13</sup> through dynamic column breakthrough. However, the regeneration process is inevitable due to the saturated adsorption of the column, in which the configuration and operating costs will increase, furthermore requiring extra energy input.<sup>14</sup> The gas separation membranes raise attention due to the advantages of continuous separation and characteristics without extra input energy for regeneration.<sup>15-17</sup> Although efficient separation of C2 mixtures has been achieved using inorganic molecular sieve membranes,<sup>18</sup> graphene membranes,<sup>19</sup> and polymer membranes,<sup>20</sup> their development have been limited due to the low designability of the materials themselves. MOF-based membranes show powerful designability. Several substrate-supported MOF membranes have been successfully prepared and exhibit high separation performance for binary mixtures with an obvious difference in kinetic diameter. For example, the high-efficiency separation of hydrogen from various mixtures was realized, including H<sub>2</sub>/  $N_2^{21} H_2^{2}/CO_2^{22} H_2^{2}/CH_4^{23}$  and  $H_2^{2}/C_3^{24} H_8^{24}$  For some gas mixtures with certain kinetic diameter differences, substratesupported MOF membranes can also realize effective separation. Sainath et al. grew ZIF-67 crystals on the lumen side of a graphene-modified hollow fiber membrane support using an in situ growth method, and the membranes achieved a  $CO_2$  permeance of 39.25  $\pm$  2.30 GPU (gas permeation unit) with a  $CO_2/CH_4$  selectivity of 44.94  $\pm$  3.0 at 1 bar feed pressure and 25 °C.<sup>25</sup> Alam et al. directly synthesized SAPO-34 membranes on tubular  $\alpha$ -alumina supports, and the

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membranes achieved a N<sub>2</sub> permeance of 399 GPU with a N<sub>2</sub>/ CH<sub>4</sub> selectivity of 4.38 at 100 kPa and 313 K.<sup>26</sup> Zhou et al. prepared ZIF-8 membranes on porous anodic aluminum oxide supports by a fast current-driven synthesis strategy, and the membranes achieved a C<sub>3</sub>H<sub>6</sub> permeance of 52.0 GPU with a C<sub>3</sub>H<sub>6</sub>/C<sub>3</sub>H<sub>8</sub> selectivity of 304.8 at 1 bar and room temperature.<sup>27</sup> However, using MOF membranes to separate gases with similar kinetic diameter is still a challenge, and no MOF membranes have been reported for C<sub>2</sub>H<sub>2</sub>/CH<sub>4</sub> or C<sub>2</sub>H<sub>2</sub>/CO<sub>2</sub> separation.

Substrate-supported ZIF-8 membranes have been widely studied because of their simple synthesis. Considering kinetic diameters of 3.3 Å for  $C_2H_2$  and 3.8 Å for  $CH_4$ , it is feasible to use the molecular sieving effect of ZIF-8 to achieve  $C_2H_2/CH_4$ separation. For the  $C_2H_2/CO_2$  mixture, the higher affinity for C<sub>2</sub>H<sub>2</sub> and ZIF-8 than CO<sub>2</sub> and ZIF-8 is therefore expected to be used for separating these two gases with the same kinetic diameters.<sup>28</sup> In this work, we prepared continuous and dense ZIF-8 membranes through an improved constant-current cathodic deposition method<sup>27,29–33</sup> at room temperature using PA filter membranes as substrates. The separation performance of the ZIF-8 membranes for a series of equimolar binary gas mixtures, including C<sub>2</sub>H<sub>2</sub>/CH<sub>4</sub>, C<sub>2</sub>H<sub>2</sub>/CO<sub>2</sub>, CO<sub>2</sub>/  $CH_4$ , and  $C_2H_2/C_2H_4$ , was tested under atmospheric pressure and room temperature permeation conditions. The results show that our ZIF-8 membranes have a maximum separation factor of 12.1 for the binary C2H2/CH4 gas mixture, corresponding to a permeance of 628.3 GPU for  $C_2H_2$ . The ZIF-8 membrane can also separate  $C_2H_2/CO_2$ , and the separation factor is 1.8. Cross-permeation tests of  $C_2H_2/$  $CH_4$ ,  $CO_2/CH_4$ , and  $C_2H_2/CO_2$  exhibit both a molecular sieve effect and thermodynamic potential. Preferential permeation induced by ZIF-8's higher affinity for C<sub>2</sub>H<sub>2</sub> plays an important role in  $C_2H_2/CH_4$  separation, while the  $C_2H_2/CO_2$  separation is related to thermodynamic factors.

#### RESULTS AND DISCUSSION

The experimental electrochemical deposition system is shown in Scheme 1. The structure and chemical properties of the

Scheme 1. Schematic Illustration of the Preparation of ZIF-8 on Polyamide Substrates Using Cathodic Deposition<sup>a</sup>



<sup>*a*</sup>The Au-coated PA substrate serves as a cathode and graphite plates of the same size as anodes in the electrochemcial deposition system.

prepared ZIF-8 membranes were characterized by powder Xray diffraction (PXRD) and scanning electron microscopy (SEM). The investigation was conducted at 15 min (ZIF-8 M-15), 30 min (ZIF-8 M-30), 45 min (ZIF-8 M-45), 60 min (ZIF-8 M-60), and 75 min (ZIF-8 M-75). PXRD suggests that both the original PA substrate and the Au-coated PA substrate exhibit diffraction broad peaks typical of polymers (Figure 1). The characteristic diffraction peak of the ZIF-8 membrane at



**Figure 1.** XRD patterns of the PA-supported ZIF-8 membranes at different growth times compared with the PA substrate, the Au-coated PA substrate, or the simulated ZIF-8.

different growth times matched well the simulated ZIF-8 diffraction peak, indicating the successful growth of the ZIF-8 phase on the Au-coated PA substrate. In the top-view SEM images of the membrane (Figure 2), it can be observed that the



Figure 2. Top-view images of the (a) PA substrate and PA-supported ZIF-8 membranes with different growth times: (b) ZIF-8 M-15, (c) ZIF-8 M-30, (d) ZIF-8 M-45, (e) ZIF-8 M-60, and (f) ZIF-8 M-75.

ZIF-8 upper surface has protruding forms similar to the Aucoated PA substrate at the shorter 15 min growth time since the growth of ZIF-8 is directly related to the electroreduction of ligand dissociated protons<sup>27</sup> and ZIF-8 preferentially grows at locations with higher conductivity.<sup>30</sup> In addition, we note that the size of grains on the membrane surface becomes significantly larger with growth time. This is probably due to the crystallization of Zn<sup>2+</sup> and ligands in solution, which reduces the concentration of free  $Zn^{2+}$  and ligands and then enlarges the grain size. The mother solution changed from clear to turbid with an increase in time, indicating the spontaneous crystallization of the mother solution (Figure S1). The membrane cross-sectional SEM image (Figure 3) shows the increase in thickness of the membrane with growth time. We plot the membrane thickness as a function of growth time. As shown in Figure S2, the membrane thickness increases linearly from 500 to 820 nm, while the growth time increased from 15 to 45 min. While the growth time increased up to 60 and 75 min, the membrane thickness increases slowly to 890



**Figure 3.** Cross-sectional image of the (a) PA substrate and PAsupported ZIF-8 membranes with different growth times: (b) ZIF-8 M-15, (c) ZIF-8 M-30, (d) ZIF-8 M-45, (e) ZIF-8 M-60, and (f) ZIF-8 M-75.

and 920 nm, respectively, indicating a significant decrease in the rate of the deposition reaction compared to the previous one. The slowing down of the membrane growth rate over time is related to the poor conductivity of ZIF-8, which prevents the substrate to contact the mother liquid directly.<sup>30</sup> In addition, the presence of the ultrathin ZIF-8 layer results in a significant thin-film interference phenomenon on the film surface (Figure S3).

Subsequently, we used the Wicke-Kallenbach-type gas separation measurement system (Figures S4 and S5) to measure the separation of four kinds of equimolar mixtures by ZIF-8 membranes prepared under different growth times. As expected, the separation for  $C_2H_2/CH_4$  mixtures can be efficiently achieved using ZIF-8 membranes. The selectivity factors for  $C_2H_2/CH_4$  increase with the increasing growth time, reaching a maximum of 12.1 at a growth time of 60 min (relevant calculation methods are presented in the Supporting Information). The selectivity factor has a slight decrease of 11.2, while the growth time reaches 75 min, which may be attributed to the further depletion of protons late in the electrodeposition reaction, resulting in excessive concentrations near the cathode, corroding the membrane, leading to membrane defects.<sup>29</sup> The permeances of C<sub>2</sub>H<sub>2</sub> and CH<sub>4</sub> show a U-shaped curve with increasing growth time, and both obtained minimum values of 628.3 and 51.9 GPU, respectively, at a growth time of 60 min. Compared to kinetic diameters of  $C_2H_2$  (3.3 Å) and  $CH_4$  (3.8 Å) with a window size of ZIF-8 (3.4 Å), the molecular sieving effect of ZIF-8 works here. We further measure the separation performance of the ZIF-8 membranes for equimolar  $C_2H_2/CO_2$ . As shown in Figure 4b, the  $C_2H_2/CO_2$  mixture can also be separated with a selectivity factor of about 1.8, even though the two gases have the same kinetic diameter, indicating that the thermodynamic potential for preferential permeation induced by ZIF-8's higher affinity for  $C_2H_2$  plays an important role in  $C_2H_2/CO_2$  separation. To further confirm this view, we measured the separation performance for  $CO_2/CH_4$  using the ZIF-8 membranes above. As shown in Figure 4c, the change in the selectivity factor is similar to Figure 4a but with an obviously low  $CO_2/$ CH₄ separation factor of 6.7 for ZIF-8 M-60, which can be attributed to the lower adsorption enthalpy for CO<sub>2</sub> than C<sub>2</sub>H<sub>2</sub>. Last, we further test the separation performance of ZIF-8 membranes for equimolar  $C_2H_2/C_2H_4$  (Figure 4d) and also found that ZIF-8 M-60 exhibits the highest selectivity.



Figure 4. Binary mixture gas separation performance of the PA-supported ZIF-8 membranes with different growth times from 15 to 75 min: (a)  $C_2H_2/CH_4$ ; (b)  $C_2H_2/CO_2$ ; (c)  $CO_2/CH_4$ ; and (d)  $C_2H_2/C_2H_4$ .

mixture gas	adsorption enthalpy (kJ/mol)	kinetic diameter (Å)	permeance (GPU)	separation factor	AE diff	KD diff
$C_2H_2/CH_4$	$17.3/12^{34}$	3.30/3.80	628.3/51.7	12.1	5.3	-0.5
$CO_2/CH_4$	$14.9^{35}/12$	3.30/3.80	340.4/50.4	6.4	2.9	-0.5
$C_2H_2/CO_2$	17.3 <sup>35</sup> /14.9	3.30/3.30	600.5/319.1	1.8	2.4	0
$C_2 H_2 / C_2 H_4$	$17.3/16.2^{36}$	3.30/4.16	633.6/151.2	4.2	1.1	-0.86

Table 1. Data Related to Separation for ZIF-8 M-60 Membranes<sup>a</sup>

"AE diff: adsorption enthalpy differences. KD diff: kinetic diameter differences. AE diff values and KD diff values are obtained by former molecular' data minus the latter molecular' data.

To further understand the separation behavior in ZIF-8 membranes, ZIF-8 M-60 with the best separation effect in our experiment was selected as an example and we present its related data about gas separation in Table 1. Interestingly, we noticed that the permeances for all gases that we measured have shown only small differences, no matter how the composition of the gas mixture changes, indicating that the interactions between the gases can be almost ignored, and the separation process is dominated by the molecular sieving effect and the interactions between gases and ZIF-8's framework. Thus, the difference of adsorption enthalpy (denoted as AE diff) and kinetic diameter (denoted as KD diff) is introduced. We find that the selectivity factor is positively correlated with the AE diff and KD diff. As shown in Table1, ZIF-8 M-60 has the lowest selectivity factor of 1.8 for  $C_2H_2/CO_2$ , corresponding to the low AE diff (2.4 kJ/mol) and KD diff (0 Å). For C<sub>2</sub>H<sub>2</sub>/C<sub>2</sub>H<sub>4</sub>, ZIF-8 M-60 shows an incremental selectivity factor of 4.2, which may be due to the relatively high KD diff of -0.86. For C<sub>2</sub>H<sub>2</sub>/CH<sub>4</sub>, the largest separation factor of 12.1 in all the gases that we tested can be observed, which may be benefited from the highest AE diff of 5.3 kJ/mol between  $C_2H_2$ and CH<sub>4</sub> and an obvious kinetic diameter difference of 0.5 Å. Compared to C<sub>2</sub>H<sub>2</sub>/CH<sub>4</sub>, ZIF-8 M-60 only has half the separation factor (6.4) for  $CO_2/CH_4$ , even though  $CO_2$  has the same kinetic diameter as  $C_2H_2$  (KD diff = 0). We notice that the AE diff in  $CO_2/CH_4$  is 2.9 kJ/mol, lower than the 5.3 kJ/mol in  $C_2H_2/CH_4$ . Thus, we speculate that the AE diff may be responsible for the higher selectivity factor in  $C_2H_2/CH_4$ than  $CO_2/CH_4$ . We also provide the related data in Table S1 about the gas separation of other samples, including ZIF-8 M-15, ZIF-8 M-30, ZIF-8 M-45, and ZIF-8 M-75, which show similar results to ZIF-8 M-60. Based on the results above, the high separation factor of ZIF-8 membranes for  $C_2H_2/CH_4$  can be attributed to the molecular sieve effect and thermodynamic potential for preferential permeation induced by ZIF-8's higher affinity for  $C_2H_2$ , while the separation for  $C_2H_2/CO_2$  can be attributed to only thermodynamic factors. In addition, the hygrothermal stability of the ZIF-8 M-60 sample was investigated (Figure S6). The results showed that there was no significant degradation in the separation performance of the ZIF-8 M-60 sample for the four kinds of gas mixtures, even though ZIF-8 M-60 was exposed to 95 °C and 90% RH for 4 h. Also, the structure of ZIF-8 was retained after the hygrothermal stability test, which can be confirmed by PXRD (Figure S7). The above results indicated the good hygrothermal stability of the ZIF-8 M-60 sample.

#### CONCLUSIONS

We have observed continuous and dense ZIF-8 membranes using PA filter membranes as substrates and demonstrated that ZIF-8 membranes can efficiently separate  $C_2H_2/CH_4$  and  $C_2H_2/CO_2$  for the first time. The high affinity of the ZIF-8 framework for  $C_2H_2$  and the small kinetic diameter of  $C_2H_2$  are the reasons for the ability of ZIF-8 to separate  $C_2H_2$  mixtures. It is expected that extensive research endeavors on MOF membranes will facilitate the discoveries of better  $C_2H_2$  separation materials.

#### EXPERIMENTAL SECTION

**Materials.** All reagents and solvents were used as received from commercial suppliers without further purification. Polyamide (PA) microporous filter membranes (0.5um) were purchased from Zhejiang Haining Yibo Filter Material Co. A DPS-305BF DC power (0–30 V) was from Guangdong HongShengFeng Co. Aluminum rings with an outer diameter of 50 mm, an inner diameter of 42 mm, and a thickness of 1.5 mm was from Hebei PangShi Aluminum Co. An ISC-150-type ion sputtering instrument was from SuProInstruments. A XK-CTS80Z-type constant temperature and humidity control chamber was used. Any reagents used should be kept dry, and moist reagents that adsorb free water will result in an accelerated rate of crystallization of the mother solution for the synthesis of ZIF-8 membranes.

**Preparation of the Mother Solution for the Synthesis of ZIF-8 Membranes.** A total of 45 mL of methanol was used to dissolve 0.827 g of zinc acetate anhydrous and another 45 mL of methanol to dissolve 0.738 g of 2-methylimidazole. The two solutions were mixed at room temperature and used for the electrodeposition reaction immediately.

Fabrication of ZIF-8 Membranes by Cathodic Deposition with Constant Current. Sputtering of Au atoms on one side of a 50 mm diameter PA filter membrane was implemented by using an ion sputterer at an absolute pressure of 8 Pa and a power of 10 W for 150 s. The Au-coated PA membrane was then fixed with two aluminum rings and connected to the negative terminal of the DC power supply. A graphite plate of 50 mm diameter and 1 mm thickness is connected to the positive side of the DC power supply and used as the anode. Two electrodes were immersed in the precursor solution, and the distance between the two electrodes was kept at 10 mm. A current of 10 mA was applied to a cathode for a period of time to produce the ZIF-8 layer. The prepared membrane was rinsed several times in methanol and dried in air.

**Characterization Methods.** X-ray powder diffraction (XRD) patterns were measured with a PANalytical X'pert<sup>3</sup> powder diffractometer at 40 kV and 40 mA. The morphology and thickness of the ZIF-8 film were imaged with a Phenom nano (Thermo Fisher Scientific) field emission scanning electron microscope at 15 kV with a secondary electron signal.

# ASSOCIATED CONTENT

#### **Supporting Information**

The Supporting Information is available free of charge at https://pubs.acs.org/doi/10.1021/acsomega.1c05126.

Details of the gas separation test method and hygrothermal stability test method; photographs of the mother solution (Figure S1); curves of membrane thickness with growth time (Figure S2); photograph of the ZIF-8 membrane with thin-film interference phenomenon (Figure S3); schematic illustration of the Wicke-Kallenbach-type gas separation measurement system and details of the permeation cell (Figures S4 and S5); gas separation performance and XRD patterns of the ZIF-8 membrane after the hygrothermal stability test (Figures S6 and S7); and data related to separation for ZIF-8 membranes at different growth times (Table S1) (PDF)

Raw data and corresponding calculation methods (XLSX)

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#### Notes

The authors declare no competing financial interest.

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