

## (2,2-Bipyridyl)bis( $\eta^5$ -pentamethylcyclopentadienyl)strontium(II)

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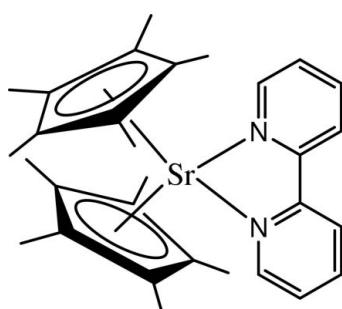
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Key indicators: single-crystal X-ray study;  $T = 168$  K; mean  $\sigma(\text{C}-\text{C}) = 0.005$  Å;  $R$  factor = 0.034;  $wR$  factor = 0.039; data-to-parameter ratio = 11.7.

In the title compound,  $[\text{Sr}(\text{C}_{10}\text{H}_{15})_2(\text{C}_{10}\text{H}_8\text{N}_2)]$ , the  $\text{Sr}-\text{N}$  distances are 2.624 (3) and 2.676 (3) Å, the  $\text{Sr}\cdots\text{Cp}$  ring centroid distances are 2.571 and 2.561 Å and the  $\text{N}-\text{C}-\text{C}-\text{N}$  torsion angle in the bipyridine ligand is  $-2.2$  (4)°. Interestingly, the bipyridine ligand is tilted. The angle between the plane defined by the Sr atom and the two bipyridyl N atoms and the plane defined by the 12 atoms of the bipyridine ligand is 10.7 (1)°.

### Related literature

For related literature, see: Allen (2002); Burns & Andersen (1987); Schultz *et al.* (2002).



### Experimental

#### Crystal data

$[\text{Sr}(\text{C}_{10}\text{H}_{15})_2(\text{C}_{10}\text{H}_8\text{N}_2)]$

$M_r = 514.26$

Orthorhombic,  $Pbca$   
 $a = 15.5489$  (9) Å  
 $b = 16.7821$  (9) Å  
 $c = 20.561$  (1) Å  
 $V = 5365.4$  (5) Å<sup>3</sup>

$Z = 8$   
Mo  $K\alpha$  radiation  
 $\mu = 2.03$  mm<sup>-1</sup>  
 $T = 168.2$  K  
 $0.10 \times 0.09 \times 0.03$  mm

#### Data collection

Bruker APEX CCD diffractometer  
Absorption correction: multi-scan  
(Blessing, 1995)  
 $T_{\min} = 0.772$ ,  $T_{\max} = 0.941$

30804 measured reflections  
5478 independent reflections  
3494 reflections with  $F^2 > 3\sigma(F^2)$   
 $R_{\text{int}} = 0.034$

#### Refinement

$R[F^2 > 2\sigma(F^2)] = 0.034$   
 $wR(F^2) = 0.038$   
 $S = 1.57$   
3494 reflections

298 parameters  
H-atom parameters constrained  
 $\Delta\rho_{\max} = 0.53$  e Å<sup>-3</sup>  
 $\Delta\rho_{\min} = -0.30$  e Å<sup>-3</sup>

**Table 1**  
Selected geometric parameters (Å, °).

|                        |           |                        |            |
|------------------------|-----------|------------------------|------------|
| Sr1–N1                 | 2.624 (3) | Sr1–Cg1                | 2.5711 (3) |
| Sr1–N2                 | 2.676 (3) | Sr1–Cg2                | 2.5608 (3) |
| C4···C27 <sup>i</sup>  | 3.540 (5) | C12···C24 <sup>i</sup> | 3.589 (5)  |
| C9···C22 <sup>ii</sup> | 3.538 (5) |                        |            |
| N1–C25–C26–N2          | −2.2 (4)  |                        |            |

Symmetry codes: (i)  $-x + 2, y - \frac{1}{2}, -z + \frac{1}{2}$ ; (ii)  $x - \frac{1}{2}, -y + \frac{1}{2}, -z$ . Cg1 and Cg2 are the centroids of the C1–C5 and C6–C10 rings, respectively.

Data collection: SMART (Bruker, 1999); cell refinement: SAINT (Bruker, 2002); data reduction: SAINT; program(s) used to solve structure: SIR97 (Altomare *et al.*, 1999); program(s) used to refine structure: TEXSAN (MSC/Rigaku, 1998); molecular graphics: TEXSAN; software used to prepare material for publication: TEXSAN.

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Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: WW2113).

### References

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## **supplementary materials**

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## (2,2-Bipyridyl)bis( $\eta^5$ -pentamethylcyclopentadienyl)strontium(II)

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### Comment

In  $Cp^*_2Sr(bipy)$  the  $Cp^*$  rings are completely staggered (see Fig. 1).  $Cg1$  and  $Cg2$  are the centroids of the rings defined by C1—C5 and C6—C10 respectively. The two pyridine rings in the bipyridine ligand are almost coplanar (the N—C—C—N torsion angle is 2.2 (4) $^\circ$ ). The least squares plane formed by the 12 atoms of the pyridine ring is tilted 10.7 $^\circ$  relative to the plane formed by Sr, N1, and N2. This is larger than the equivalent angle in any other  $Cp^*_2M(bipy)$  in the Cambridge Structural Database (Allen, 2002). The closest is 5.1 $^\circ$  in  $[Cp^*_2Yb(bipy)][Cp^*_2YbCl_2]$  (Schultz *et al.* 2002). The reason for this tilting is unclear as the Sr is d<sup>0</sup> and therefore electronic effects should be minor. At the same time it is unclear what steric reason could lead to this tilt.

### Experimental

$Cp^*_2Sr(bipy)$  was prepared according to literature procedures (Burns and Andersen, 1987)

### Refinement

All non-hydrogen atoms were refined anisotropically. Hydrogen atoms were fixed based on the expected geometry of the carbon atoms to which they were attached.

### Figures

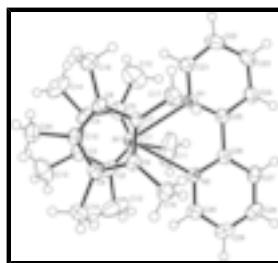


Fig. 1. View of the structure of  $(\eta^5\text{-C}_5\text{Me}_5)_2\text{Sr}(\text{bipy})$ , showing the staggering of the two  $Cp^*$  rings, with displacement ellipsoids drawn at the 50% probability level.

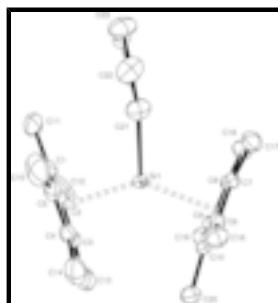


Fig. 2. Side view of the structure of  $(\eta^5\text{-C}_5\text{Me}_5)_2\text{Sr}(\text{bipy})$ , with displacement ellipsoids drawn at the 50% probability level. Hydrogen atoms have been omitted for clarity.

# supplementary materials

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## (2,2-Bipyridyl)bis( $\eta^5$ -pentamethylcyclopentadienyl)strontium(II)

### Crystal data

|  |   |
|--|---|
| [Sr(C <sub>10</sub> H <sub>15</sub> ) <sub>2</sub> (C <sub>10</sub> H <sub>8</sub> N <sub>2</sub> )] | $F_{000} = 2160.00$                       |
| $M_r = 514.26$   | $D_x = 1.273 \text{ Mg m}^{-3}$           |
| Orthorhombic, <i>Pbca</i>  | Mo $K\alpha$ radiation                    |
| Hall symbol: -P 2ac 2ab  | $\lambda = 0.7107 \text{ \AA}$            |
| $a = 15.5489 (9) \text{ \AA}$  | Cell parameters from 5093 reflections     |
| $b = 16.7821 (9) \text{ \AA}$  | $\theta = 2.4\text{--}25.2^\circ$         |
| $c = 20.561 (1) \text{ \AA}$   | $\mu = 2.03 \text{ mm}^{-1}$              |
| $V = 5365.4 (5) \text{ \AA}^3$   | $T = 168.2 \text{ K}$                     |
| $Z = 8$  | Plate, red                                |
|  | $0.10 \times 0.09 \times 0.03 \text{ mm}$ |

### Data collection

|   |  |
|---|--|
| Bruker APEX CCD diffractometer                      | 3494 reflections with $F^2 > 3\sigma(F^2)$ |
| $\omega$ scans                                      | $R_{\text{int}} = 0.034$                   |
| Absorption correction: multi-scan (Blessing, 1995)  | $\theta_{\text{max}} = 26.4^\circ$         |
| $T_{\text{min}} = 0.772$ , $T_{\text{max}} = 0.941$ | $h = 0\text{--}19$                         |
| 30804 measured reflections                          | $k = 0\text{--}20$                         |
| 5478 independent reflections                        | $l = 0\text{--}25$                         |

### Refinement

|                                 |  |
|---------------------------------|--|
| Refinement on $F$               | H-atom parameters constrained                        |
| $R[F^2 > 2\sigma(F^2)] = 0.034$ | $w = 1/[\sigma^2(F_0) + 0.00022 F_0 ^2]$             |
| $wR(F^2) = 0.039$               | $(\Delta/\sigma)_{\text{max}} = 0.002$               |
| $S = 1.57$                      | $\Delta\rho_{\text{max}} = 0.53 \text{ e \AA}^{-3}$  |
| 3494 reflections                | $\Delta\rho_{\text{min}} = -0.30 \text{ e \AA}^{-3}$ |
| 298 parameters                  | Extinction correction: none                          |

### Special details

**Refinement.** Refinement using reflections with  $F^2 > 3.0 \sigma(F^2)$ . The weighted *R*-factor (*wR*), goodness of fit (*S*) and *R*-factor (gt) are based on *F*, with *F* set to zero for negative *F*. The threshold expression of  $F^2 > 3.0 \sigma(F^2)$  is used only for calculating *R*-factor (gt).

### Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters ( $\text{\AA}^2$ )

|     | <i>x</i>    | <i>y</i>    | <i>z</i>    | $U_{\text{iso}}^*/U_{\text{eq}}$ |
|-----|-------------|-------------|-------------|----------------------------------|
| Sr1 | 0.88103 (2) | 0.21813 (2) | 0.12421 (1) | 0.02281 (7)                      |
| N1  | 0.9677 (2)  | 0.3503 (2)  | 0.1051 (1)  | 0.0311 (8)                       |
| N2  | 0.8425 (2)  | 0.3460 (1)  | 0.1963 (1)  | 0.0267 (8)                       |

|     |            |            |             |             |
|-----|------------|------------|-------------|-------------|
| C1  | 1.0006 (3) | 0.1935 (2) | 0.2267 (2)  | 0.041 (1)   |
| C2  | 0.9339 (2) | 0.1399 (2) | 0.2383 (2)  | 0.040 (1)   |
| C3  | 0.9370 (2) | 0.0800 (2) | 0.1897 (2)  | 0.034 (1)   |
| C4  | 1.0066 (2) | 0.0990 (2) | 0.1483 (2)  | 0.034 (1)   |
| C5  | 1.0460 (2) | 0.1682 (2) | 0.1715 (2)  | 0.038 (1)   |
| C6  | 0.8290 (2) | 0.1915 (2) | -0.0059 (2) | 0.0266 (9)  |
| C7  | 0.7927 (2) | 0.2655 (2) | 0.0097 (2)  | 0.0239 (9)  |
| C8  | 0.7266 (2) | 0.2531 (2) | 0.0561 (2)  | 0.0255 (9)  |
| C9  | 0.7230 (2) | 0.1706 (2) | 0.0694 (2)  | 0.0266 (9)  |
| C10 | 0.7861 (2) | 0.1323 (2) | 0.0310 (2)  | 0.0254 (9)  |
| C11 | 1.0229 (4) | 0.2649 (3) | 0.2689 (2)  | 0.084 (2)   |
| C12 | 0.8676 (4) | 0.1433 (3) | 0.2921 (2)  | 0.087 (2)   |
| C13 | 0.8814 (3) | 0.0067 (3) | 0.1861 (2)  | 0.063 (1)   |
| C14 | 1.0366 (3) | 0.0512 (3) | 0.0904 (2)  | 0.060 (1)   |
| C15 | 1.1271 (3) | 0.2059 (3) | 0.1456 (3)  | 0.075 (2)   |
| C16 | 0.8986 (2) | 0.1763 (2) | -0.0554 (2) | 0.039 (1)   |
| C17 | 0.8158 (2) | 0.3448 (2) | -0.0202 (2) | 0.039 (1)   |
| C18 | 0.6675 (2) | 0.3164 (2) | 0.0822 (2)  | 0.038 (1)   |
| C19 | 0.6609 (2) | 0.1307 (2) | 0.1157 (2)  | 0.039 (1)   |
| C20 | 0.7986 (2) | 0.0439 (2) | 0.0234 (2)  | 0.038 (1)   |
| C21 | 1.0290 (2) | 0.3505 (2) | 0.0594 (2)  | 0.039 (1)   |
| C22 | 1.0872 (3) | 0.4116 (3) | 0.0512 (2)  | 0.046 (1)   |
| C23 | 1.0803 (3) | 0.4764 (2) | 0.0915 (2)  | 0.048 (1)   |
| C24 | 1.0177 (2) | 0.4781 (2) | 0.1389 (2)  | 0.037 (1)   |
| C25 | 0.9619 (2) | 0.4137 (2) | 0.1450 (2)  | 0.0266 (9)  |
| C26 | 0.8938 (2) | 0.4108 (2) | 0.1962 (2)  | 0.0252 (9)  |
| C27 | 0.8846 (2) | 0.4709 (2) | 0.2424 (2)  | 0.0328 (10) |
| C28 | 0.8216 (2) | 0.4643 (2) | 0.2889 (2)  | 0.041 (1)   |
| C29 | 0.7689 (2) | 0.3982 (2) | 0.2896 (2)  | 0.040 (1)   |
| C30 | 0.7819 (2) | 0.3412 (2) | 0.2421 (2)  | 0.035 (1)   |
| H1  | 0.9904     | 0.2628     | 0.3080      | 0.1013*     |
| H2  | 1.0825     | 0.2640     | 0.2789      | 0.1013*     |
| H3  | 1.0096     | 0.3126     | 0.2461      | 0.1013*     |
| H4  | 0.8535     | 0.0907     | 0.3054      | 0.1044*     |
| H5  | 0.8903     | 0.1720     | 0.3280      | 0.1044*     |
| H6  | 0.8173     | 0.1692     | 0.2766      | 0.1044*     |
| H7  | 0.8961     | -0.0285    | 0.2205      | 0.0757*     |
| H8  | 0.8227     | 0.0215     | 0.1899      | 0.0757*     |
| H9  | 0.8904     | -0.0193    | 0.1456      | 0.0757*     |
| H10 | 1.0396     | -0.0035    | 0.1019      | 0.0724*     |
| H11 | 0.9971     | 0.0578     | 0.0556      | 0.0724*     |
| H12 | 1.0919     | 0.0692     | 0.0773      | 0.0724*     |
| H13 | 1.1757     | 0.1814     | 0.1653      | 0.0898*     |
| H14 | 1.1270     | 0.2612     | 0.1555      | 0.0898*     |
| H15 | 1.1297     | 0.1988     | 0.0998      | 0.0898*     |
| H16 | 0.9326     | 0.1322     | -0.0419     | 0.0467*     |
| H17 | 0.8732     | 0.1649     | -0.0963     | 0.0467*     |
| H18 | 0.9340     | 0.2222     | -0.0591     | 0.0467*     |
| H19 | 0.8724     | 0.3422     | -0.0375     | 0.0463*     |

## supplementary materials

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|     |        |        |         |         |
|-----|--------|--------|---------|---------|
| H20 | 0.7764 | 0.3569 | -0.0541 | 0.0463* |
| H21 | 0.8132 | 0.3852 | 0.0121  | 0.0463* |
| H22 | 0.6148 | 0.2926 | 0.0954  | 0.0451* |
| H23 | 0.6937 | 0.3418 | 0.1184  | 0.0451* |
| H24 | 0.6565 | 0.3546 | 0.0492  | 0.0451* |
| H25 | 0.6716 | 0.1488 | 0.1587  | 0.0473* |
| H26 | 0.6036 | 0.1436 | 0.1036  | 0.0473* |
| H27 | 0.6686 | 0.0746 | 0.1138  | 0.0473* |
| H28 | 0.7707 | 0.0170 | 0.0582  | 0.0462* |
| H29 | 0.8583 | 0.0319 | 0.0241  | 0.0462* |
| H30 | 0.7746 | 0.0270 | -0.0168 | 0.0462* |
| H31 | 1.0326 | 0.3060 | 0.0310  | 0.0469* |
| H32 | 1.1306 | 0.4089 | 0.0188  | 0.0555* |
| H33 | 1.1186 | 0.5201 | 0.0867  | 0.0576* |
| H34 | 1.0127 | 0.5227 | 0.1671  | 0.0441* |
| H35 | 0.9215 | 0.5160 | 0.2417  | 0.0393* |
| H36 | 0.8143 | 0.5051 | 0.3205  | 0.0490* |
| H37 | 0.7252 | 0.3920 | 0.3215  | 0.0481* |
| H38 | 0.7454 | 0.2958 | 0.2420  | 0.0414* |

Atomic displacement parameters ( $\text{\AA}^2$ )

|     | $U^{11}$   | $U^{22}$   | $U^{33}$   | $U^{12}$    | $U^{13}$    | $U^{23}$    |
|-----|------------|------------|------------|-------------|-------------|-------------|
| Sr1 | 0.0253 (1) | 0.0195 (1) | 0.0236 (1) | -0.0008 (1) | -0.0028 (1) | -0.0020 (1) |
| N1  | 0.035 (2)  | 0.029 (2)  | 0.029 (2)  | -0.006 (1)  | 0.003 (1)   | -0.002 (1)  |
| N2  | 0.027 (1)  | 0.025 (1)  | 0.028 (2)  | 0.002 (1)   | 0.001 (1)   | -0.001 (1)  |
| C1  | 0.053 (3)  | 0.032 (2)  | 0.037 (2)  | 0.013 (2)   | -0.022 (2)  | -0.007 (2)  |
| C2  | 0.053 (3)  | 0.044 (2)  | 0.023 (2)  | 0.024 (2)   | 0.005 (2)   | 0.007 (2)   |
| C3  | 0.036 (2)  | 0.027 (2)  | 0.038 (2)  | 0.005 (2)   | -0.007 (2)  | 0.006 (2)   |
| C4  | 0.037 (2)  | 0.036 (2)  | 0.028 (2)  | 0.016 (2)   | -0.003 (2)  | -0.002 (2)  |
| C5  | 0.027 (2)  | 0.038 (2)  | 0.048 (2)  | 0.004 (2)   | -0.010 (2)  | 0.004 (2)   |
| C6  | 0.029 (2)  | 0.030 (2)  | 0.021 (2)  | 0.000 (1)   | -0.002 (1)  | -0.004 (1)  |
| C7  | 0.030 (2)  | 0.021 (2)  | 0.021 (2)  | -0.001 (1)  | -0.003 (1)  | 0.002 (1)   |
| C8  | 0.023 (2)  | 0.026 (2)  | 0.028 (2)  | 0.004 (1)   | -0.004 (2)  | -0.001 (1)  |
| C9  | 0.027 (2)  | 0.024 (2)  | 0.029 (2)  | -0.006 (1)  | -0.002 (1)  | 0.000 (1)   |
| C10 | 0.027 (2)  | 0.020 (2)  | 0.029 (2)  | -0.001 (1)  | -0.007 (1)  | -0.005 (1)  |
| C11 | 0.115 (5)  | 0.061 (3)  | 0.077 (4)  | 0.033 (3)   | -0.066 (3)  | -0.032 (3)  |
| C12 | 0.115 (4)  | 0.097 (4)  | 0.049 (3)  | 0.066 (3)   | 0.038 (3)   | 0.037 (3)   |
| C13 | 0.064 (3)  | 0.043 (3)  | 0.082 (3)  | -0.005 (2)  | -0.012 (3)  | 0.024 (2)   |
| C14 | 0.063 (3)  | 0.074 (3)  | 0.044 (3)  | 0.035 (2)   | -0.007 (2)  | -0.015 (2)  |
| C15 | 0.030 (2)  | 0.081 (4)  | 0.114 (4)  | 0.002 (2)   | -0.011 (2)  | 0.024 (3)   |
| C16 | 0.043 (3)  | 0.040 (2)  | 0.034 (2)  | -0.001 (2)  | 0.003 (2)   | -0.006 (2)  |
| C17 | 0.048 (2)  | 0.032 (2)  | 0.036 (2)  | 0.002 (2)   | 0.000 (2)   | 0.006 (2)   |
| C18 | 0.036 (2)  | 0.034 (2)  | 0.043 (2)  | 0.008 (2)   | 0.003 (2)   | 0.000 (2)   |
| C19 | 0.037 (2)  | 0.037 (2)  | 0.044 (2)  | -0.008 (2)  | 0.005 (2)   | 0.004 (2)   |
| C20 | 0.039 (2)  | 0.031 (2)  | 0.045 (2)  | -0.002 (2)  | -0.005 (2)  | -0.006 (2)  |
| C21 | 0.044 (2)  | 0.040 (2)  | 0.033 (2)  | -0.004 (2)  | 0.009 (2)   | -0.006 (2)  |
| C22 | 0.046 (2)  | 0.060 (3)  | 0.033 (2)  | -0.017 (2)  | 0.011 (2)   | 0.001 (2)   |

|     |           |           |           |            |            |            |
|-----|-----------|-----------|-----------|------------|------------|------------|
| C23 | 0.053 (3) | 0.041 (3) | 0.050 (3) | -0.022 (2) | 0.008 (2)  | 0.001 (2)  |
| C24 | 0.043 (2) | 0.028 (2) | 0.040 (2) | -0.007 (2) | 0.001 (2)  | -0.002 (2) |
| C25 | 0.028 (2) | 0.023 (2) | 0.029 (2) | -0.001 (1) | -0.004 (1) | 0.002 (1)  |
| C26 | 0.026 (2) | 0.024 (2) | 0.025 (2) | 0.001 (1)  | -0.006 (1) | 0.002 (1)  |
| C27 | 0.034 (2) | 0.029 (2) | 0.036 (2) | -0.002 (2) | -0.006 (2) | -0.006 (1) |
| C28 | 0.041 (2) | 0.046 (2) | 0.035 (2) | 0.009 (2)  | -0.003 (2) | -0.013 (2) |
| C29 | 0.034 (2) | 0.052 (2) | 0.035 (2) | 0.008 (2)  | 0.006 (2)  | -0.004 (2) |
| C30 | 0.033 (2) | 0.033 (2) | 0.038 (2) | -0.001 (2) | 0.005 (2)  | 0.002 (2)  |

*Geometric parameters ( $\text{\AA}$ ,  $^\circ$ )*

|         |            |         |           |
|---------|------------|---------|-----------|
| SR1—N1  | 2.624 (3)  | C21—C22 | 1.378 (5) |
| SR1—N2  | 2.676 (3)  | C22—C23 | 1.370 (5) |
| SR1—C1  | 2.841 (3)  | C23—C24 | 1.378 (5) |
| SR1—C2  | 2.812 (3)  | C24—C25 | 1.392 (4) |
| SR1—C3  | 2.819 (3)  | C25—C26 | 1.495 (4) |
| SR1—C4  | 2.838 (3)  | C26—C27 | 1.393 (4) |
| SR1—C5  | 2.869 (3)  | C27—C28 | 1.374 (5) |
| SR1—C6  | 2.830 (3)  | C28—C29 | 1.380 (5) |
| SR1—C7  | 2.840 (3)  | C29—C30 | 1.382 (5) |
| SR1—C8  | 2.841 (3)  | C11—H1  | 0.950     |
| SR1—C9  | 2.818 (3)  | C11—H2  | 0.950     |
| SR1—C10 | 2.815 (3)  | C11—H3  | 0.950     |
| SR1—Cg1 | 2.5711 (3) | C12—H4  | 0.950     |
| SR1—Cg2 | 2.5608 (3) | C12—H5  | 0.950     |
| N1—C21  | 1.339 (4)  | C12—H6  | 0.950     |
| N1—C25  | 1.346 (4)  | C13—H7  | 0.950     |
| N2—C26  | 1.349 (4)  | C13—H8  | 0.950     |
| N2—C30  | 1.334 (4)  | C13—H9  | 0.950     |
| C1—C2   | 1.394 (5)  | C14—H10 | 0.950     |
| C1—C5   | 1.402 (5)  | C14—H11 | 0.950     |
| C1—C11  | 1.520 (5)  | C14—H12 | 0.950     |
| C1—Cg1  | 1.189 (4)  | C15—H13 | 0.950     |
| C2—C3   | 1.419 (5)  | C15—H14 | 0.950     |
| C2—C12  | 1.512 (5)  | C15—H15 | 0.950     |
| C2—Cg1  | 1.199 (4)  | C16—H16 | 0.950     |
| C3—C4   | 1.412 (5)  | C16—H17 | 0.950     |
| C3—C13  | 1.506 (5)  | C16—H18 | 0.950     |
| C3—Cg1  | 1.207 (4)  | C17—H19 | 0.950     |
| C4—C5   | 1.396 (5)  | C17—H20 | 0.950     |
| C4—C14  | 1.510 (5)  | C17—H21 | 0.950     |
| C4—Cg1  | 1.189 (3)  | C18—H22 | 0.950     |
| C5—C15  | 1.508 (6)  | C18—H23 | 0.950     |
| C5—Cg1  | 1.190 (4)  | C18—H24 | 0.950     |
| C6—C7   | 1.402 (4)  | C19—H25 | 0.950     |
| C6—C10  | 1.416 (4)  | C19—H26 | 0.950     |
| C6—C16  | 1.508 (5)  | C19—H27 | 0.950     |
| C6—Cg2  | 1.199 (3)  | C20—H28 | 0.950     |
| C7—C8   | 1.418 (4)  | C20—H29 | 0.950     |

## supplementary materials

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| C7—C17     | 1.509 (5)   | C20—H30                | 0.950     |
| C7—Cg2     | 1.197 (3)   | C21—H31                | 0.950     |
| C8—C9      | 1.412 (4)   | C22—H32                | 0.950     |
| C8—C18     | 1.503 (4)   | C23—H33                | 0.950     |
| C8—Cg2     | 1.206 (3)   | C24—H34                | 0.950     |
| C9—C10     | 1.413 (4)   | C27—H35                | 0.950     |
| C9—C19     | 1.513 (4)   | C28—H36                | 0.950     |
| C9—Cg2     | 1.203 (3)   | C29—H37                | 0.950     |
| C10—C20    | 1.505 (4)   | C30—H38                | 0.950     |
| C10—Cg2    | 1.201 (3)   |                        |           |
| SR1···N1   | 2.624 (3)   | SR1···C3               | 2.819 (3) |
| SR1···N2   | 2.676 (3)   | SR1···C6               | 2.830 (3) |
| SR1···C1   | 2.841 (3)   | SR1···C4               | 2.838 (3) |
| SR1···C2   | 2.812 (3)   | SR1···C7               | 2.840 (3) |
| SR1···C3   | 2.819 (3)   | SR1···C8               | 2.841 (3) |
| SR1···C4   | 2.838 (3)   | SR1···C1               | 2.841 (3) |
| SR1···C5   | 2.869 (3)   | SR1···C5               | 2.869 (3) |
| SR1···C6   | 2.830 (3)   | SR1···C21              | 3.465 (4) |
| SR1···C7   | 2.840 (3)   | SR1···C30              | 3.537 (4) |
| SR1···C8   | 2.841 (3)   | SR1···C25              | 3.540 (3) |
| SR1···C9   | 2.818 (3)   | SR1···C26              | 3.562 (3) |
| SR1···C10  | 2.815 (3)   | N1···C17               | 3.497 (4) |
| SR1···Cg1  | 2.5711 (3)  | N1···C5                | 3.562 (4) |
| SR1···Cg2  | 2.5608 (3)  | N1···C15               | 3.565 (5) |
| SR1···Cg2  | 2.5608 (3)  | N2···C11               | 3.455 (5) |
| SR1···Cg1  | 2.5711 (3)  | C4···C27 <sup>i</sup>  | 3.540 (5) |
| SR1···N1   | 2.624 (3)   | C9···C22 <sup>ii</sup> | 3.538 (5) |
| SR1···N2   | 2.676 (3)   | C11···C26              | 3.500 (5) |
| SR1···C2   | 2.812 (3)   | C12···C24 <sup>i</sup> | 3.589 (5) |
| SR1···C10  | 2.815 (3)   | C15···C21              | 3.371 (6) |
| SR1···C9   | 2.818 (3)   |                        |           |
| N1—SR1—N2  | 61.32 (8)   | SR1—C7—C17             | 118.0 (2) |
| N1—SR1—C1  | 84.1 (1)    | SR1—C7—Cg2             | 64.4 (1)  |
| N1—SR1—C2  | 111.7 (1)   | C6—C7—C8               | 108.4 (3) |
| N1—SR1—C3  | 127.42 (9)  | C6—C7—C17              | 126.3 (3) |
| N1—SR1—C4  | 105.55 (10) | C6—C7—Cg2              | 54.3 (2)  |
| N1—SR1—C5  | 80.72 (9)   | C8—C7—C17              | 125.2 (3) |
| N1—SR1—C6  | 97.99 (9)   | C8—C7—Cg2              | 54.1 (2)  |
| N1—SR1—C7  | 83.55 (9)   | C17—C7—Cg2             | 177.6 (3) |
| N1—SR1—C8  | 100.70 (9)  | SR1—C8—C7              | 75.5 (2)  |
| N1—SR1—C9  | 128.80 (9)  | SR1—C8—C9              | 74.7 (2)  |
| N1—SR1—C10 | 126.83 (9)  | SR1—C8—C18             | 119.2 (2) |
| N1—SR1—Cg1 | 102.33 (6)  | SR1—C8—Cg2             | 64.3 (1)  |
| N1—SR1—Cg2 | 108.44 (6)  | C7—C8—C9               | 107.6 (3) |
| N2—SR1—C1  | 81.48 (9)   | C7—C8—C18              | 125.4 (3) |
| N2—SR1—C2  | 88.69 (9)   | C7—C8—Cg2              | 53.5 (2)  |
| N2—SR1—C3  | 117.64 (9)  | C9—C8—C18              | 126.9 (3) |
| N2—SR1—C4  | 128.44 (9)  | C9—C8—Cg2              | 54.0 (2)  |

|            |             |             |           |
|------------|-------------|-------------|-----------|
| N2—SR1—C5  | 104.27 (9)  | C18—C8—Cg2  | 176.3 (3) |
| N2—SR1—C6  | 125.91 (9)  | SR1—C9—C8   | 76.4 (2)  |
| N2—SR1—C7  | 97.29 (8)   | SR1—C9—C10  | 75.4 (2)  |
| N2—SR1—C8  | 85.32 (8)   | SR1—C9—C19  | 115.5 (2) |
| N2—SR1—C9  | 104.69 (9)  | SR1—C9—Cg2  | 65.3 (1)  |
| N2—SR1—C10 | 132.08 (8)  | C8—C9—C10   | 108.1 (3) |
| N2—SR1—Cg1 | 104.87 (6)  | C8—C9—C19   | 125.5 (3) |
| N2—SR1—Cg2 | 110.07 (6)  | C8—C9—Cg2   | 54.2 (2)  |
| C1—SR1—C2  | 28.5 (1)    | C10—C9—C19  | 126.4 (3) |
| C1—SR1—C3  | 47.4 (1)    | C10—C9—Cg2  | 53.9 (2)  |
| C1—SR1—C4  | 46.96 (10)  | C19—C9—Cg2  | 179.2 (3) |
| C1—SR1—C5  | 28.4 (1)    | SR1—C10—C6  | 76.0 (2)  |
| C1—SR1—C6  | 149.9 (1)   | SR1—C10—C9  | 75.6 (2)  |
| C1—SR1—C7  | 166.5 (1)   | SR1—C10—C20 | 120.5 (2) |
| C1—SR1—C8  | 161.6 (1)   | SR1—C10—Cg2 | 65.4 (1)  |
| C1—SR1—C9  | 145.7 (1)   | C6—C10—C9   | 107.9 (3) |
| C1—SR1—C10 | 140.70 (10) | C6—C10—C20  | 125.2 (3) |
| C1—SR1—Cg1 | 24.75 (7)   | C6—C10—Cg2  | 53.8 (2)  |
| C1—SR1—Cg2 | 165.79 (7)  | C9—C10—C20  | 126.5 (3) |
| C2—SR1—C3  | 29.20 (10)  | C9—C10—Cg2  | 54.1 (2)  |
| C2—SR1—C4  | 47.49 (10)  | C20—C10—Cg2 | 174.0 (3) |
| C2—SR1—C5  | 47.1 (1)    | N1—C21—C22  | 123.8 (3) |
| C2—SR1—C6  | 143.0 (1)   | C21—C22—C23 | 117.7 (3) |
| C2—SR1—C7  | 164.6 (1)   | C22—C23—C24 | 120.0 (3) |
| C2—SR1—C8  | 139.0 (1)   | C23—C24—C25 | 119.2 (3) |
| C2—SR1—C9  | 117.2 (1)   | N1—C25—C24  | 121.2 (3) |
| C2—SR1—C10 | 118.9 (1)   | N1—C25—C26  | 116.8 (3) |
| C2—SR1—Cg1 | 25.23 (7)   | C24—C25—C26 | 122.0 (3) |
| C2—SR1—Cg2 | 139.88 (9)  | N2—C26—C25  | 116.5 (3) |
| C3—SR1—C4  | 28.92 (10)  | N2—C26—C27  | 121.5 (3) |
| C3—SR1—C5  | 47.25 (10)  | C25—C26—C27 | 122.0 (3) |
| C3—SR1—C6  | 114.19 (10) | C26—C27—C28 | 119.3 (3) |
| C3—SR1—C7  | 140.88 (10) | C27—C28—C29 | 119.7 (3) |
| C3—SR1—C8  | 131.80 (10) | C28—C29—C30 | 117.6 (3) |
| C3—SR1—C9  | 103.18 (9)  | N2—C30—C29  | 124.1 (3) |
| C3—SR1—C10 | 93.82 (10)  | SR1—Cg1—C1  | 90.4 (2)  |
| C3—SR1—Cg1 | 25.35 (7)   | SR1—Cg1—C2  | 88.7 (2)  |
| C3—SR1—Cg2 | 118.38 (7)  | SR1—Cg1—C3  | 88.9 (2)  |
| C4—SR1—C5  | 28.31 (10)  | SR1—Cg1—C4  | 90.3 (2)  |
| C4—SR1—C6  | 104.51 (10) | SR1—Cg1—C5  | 91.9 (2)  |
| C4—SR1—C7  | 132.45 (9)  | C1—Cg1—C2   | 71.4 (3)  |
| C4—SR1—C8  | 144.42 (10) | C1—Cg1—C3   | 143.7 (3) |
| C4—SR1—C9  | 118.07 (10) | C1—Cg1—C4   | 144.1 (3) |
| C4—SR1—C10 | 96.86 (9)   | C1—Cg1—C5   | 72.2 (3)  |
| C4—SR1—Cg1 | 24.78 (7)   | C2—Cg1—C3   | 72.3 (3)  |
| C4—SR1—Cg2 | 120.99 (7)  | C2—Cg1—C4   | 144.5 (3) |
| C5—SR1—C6  | 122.0 (1)   | C2—Cg1—C5   | 143.6 (3) |
| C5—SR1—C7  | 142.7 (1)   | C3—Cg1—C4   | 72.2 (2)  |
| C5—SR1—C8  | 169.5 (1)   | C3—Cg1—C5   | 144.1 (2) |

## supplementary materials

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| C5—SR1—C9   | 146.35 (10) | C4—Cg1—C5   | 71.8 (2)  |
| C5—SR1—C10  | 123.37 (10) | SR1—Cg2—C6  | 90.1 (1)  |
| C5—SR1—Cg1  | 24.49 (7)   | SR1—Cg2—C7  | 90.7 (1)  |
| C5—SR1—Cg2  | 144.63 (8)  | SR1—Cg2—C8  | 90.5 (2)  |
| C6—SR1—C7   | 28.63 (9)   | SR1—Cg2—C9  | 89.4 (1)  |
| C6—SR1—C8   | 47.57 (9)   | SR1—Cg2—C10 | 89.3 (1)  |
| C6—SR1—C9   | 47.77 (9)   | C6—Cg2—C7   | 71.6 (2)  |
| C6—SR1—C10  | 29.05 (9)   | C6—Cg2—C8   | 144.0 (2) |
| C6—SR1—Cg1  | 128.95 (7)  | C6—Cg2—C9   | 144.3 (2) |
| C6—SR1—Cg2  | 25.08 (6)   | C6—Cg2—C10  | 72.3 (2)  |
| C7—SR1—C8   | 28.92 (9)   | C7—Cg2—C8   | 72.4 (2)  |
| C7—SR1—C9   | 47.60 (9)   | C7—Cg2—C9   | 144.1 (2) |
| C7—SR1—C10  | 47.55 (9)   | C7—Cg2—C10  | 143.9 (2) |
| C7—SR1—Cg1  | 157.22 (7)  | C8—Cg2—C9   | 71.7 (2)  |
| C7—SR1—Cg2  | 24.93 (6)   | C8—Cg2—C10  | 143.8 (2) |
| C8—SR1—C9   | 28.89 (9)   | C9—Cg2—C10  | 72.0 (2)  |
| C8—SR1—C10  | 47.71 (9)   | C1—C11—H1   | 109.470   |
| C8—SR1—Cg1  | 156.95 (7)  | C1—C11—H2   | 109.470   |
| C8—SR1—Cg2  | 25.12 (7)   | C1—C11—H3   | 109.470   |
| C9—SR1—C10  | 29.06 (9)   | H1—C11—H2   | 109.472   |
| C9—SR1—Cg1  | 128.52 (6)  | H1—C11—H3   | 109.472   |
| C9—SR1—Cg2  | 25.27 (6)   | H2—C11—H3   | 109.473   |
| C10—SR1—Cg1 | 116.13 (6)  | C2—C12—H4   | 109.470   |
| C10—SR1—Cg2 | 25.25 (6)   | C2—C12—H5   | 109.470   |
| Cg1—SR1—Cg2 | 141.38 (1)  | C2—C12—H6   | 109.470   |
| SR1—N1—C21  | 118.3 (2)   | H4—C12—H5   | 109.472   |
| SR1—N1—C25  | 122.9 (2)   | H4—C12—H6   | 109.472   |
| C21—N1—C25  | 118.2 (3)   | H5—C12—H6   | 109.473   |
| SR1—N2—C26  | 120.9 (2)   | C3—C13—H7   | 109.470   |
| SR1—N2—C30  | 120.1 (2)   | C3—C13—H8   | 109.470   |
| C26—N2—C30  | 117.8 (3)   | C3—C13—H9   | 109.471   |
| SR1—C1—C2   | 74.6 (2)    | H7—C13—H8   | 109.472   |
| SR1—C1—C5   | 76.9 (2)    | H7—C13—H9   | 109.473   |
| SR1—C1—C11  | 117.2 (2)   | H8—C13—H9   | 109.472   |
| SR1—C1—Cg1  | 64.8 (1)    | C4—C14—H10  | 109.469   |
| C2—C1—C5    | 108.5 (3)   | C4—C14—H11  | 109.470   |
| C2—C1—C11   | 125.5 (4)   | C4—C14—H12  | 109.470   |
| C2—C1—Cg1   | 54.6 (2)    | H10—C14—H11 | 109.474   |
| C5—C1—C11   | 125.9 (4)   | H10—C14—H12 | 109.471   |
| C5—C1—Cg1   | 53.9 (2)    | H11—C14—H12 | 109.473   |
| C11—C1—Cg1  | 177.9 (3)   | C5—C15—H13  | 109.470   |
| SR1—C2—C1   | 76.9 (2)    | C5—C15—H14  | 109.470   |
| SR1—C2—C3   | 75.7 (2)    | C5—C15—H15  | 109.469   |
| SR1—C2—C12  | 113.1 (2)   | H13—C15—H14 | 109.473   |
| SR1—C2—Cg1  | 66.1 (1)    | H13—C15—H15 | 109.473   |
| C1—C2—C3    | 108.1 (3)   | H14—C15—H15 | 109.473   |
| C1—C2—C12   | 127.5 (4)   | C6—C16—H16  | 109.470   |
| C1—C2—Cg1   | 54.0 (2)    | C6—C16—H17  | 109.471   |
| C3—C2—C12   | 124.4 (4)   | C6—C16—H18  | 109.470   |

|            |           |             |         |
|------------|-----------|-------------|---------|
| C3—C2—Cg1  | 54.1 (2)  | H16—C16—H17 | 109.471 |
| C12—C2—Cg1 | 178.3 (4) | H16—C16—H18 | 109.472 |
| SR1—C3—C2  | 75.1 (2)  | H17—C16—H18 | 109.473 |
| SR1—C3—C4  | 76.3 (2)  | C7—C17—H19  | 109.470 |
| SR1—C3—C13 | 118.1 (2) | C7—C17—H20  | 109.470 |
| SR1—C3—Cg1 | 65.8 (1)  | C7—C17—H21  | 109.470 |
| C2—C3—C4   | 106.9 (3) | H19—C17—H20 | 109.472 |
| C2—C3—C13  | 126.4 (4) | H19—C17—H21 | 109.473 |
| C2—C3—Cg1  | 53.6 (2)  | H20—C17—H21 | 109.471 |
| C4—C3—C13  | 126.5 (4) | C8—C18—H22  | 109.470 |
| C4—C3—Cg1  | 53.3 (2)  | C8—C18—H23  | 109.469 |
| C13—C3—Cg1 | 176.1 (3) | C8—C18—H24  | 109.470 |
| SR1—C4—C3  | 74.8 (2)  | H22—C18—H23 | 109.472 |
| SR1—C4—C5  | 77.1 (2)  | H22—C18—H24 | 109.473 |
| SR1—C4—C14 | 116.7 (2) | H23—C18—H24 | 109.473 |
| SR1—C4—Cg1 | 65.0 (1)  | C9—C19—H25  | 109.471 |
| C3—C4—C5   | 108.6 (3) | C9—C19—H26  | 109.470 |
| C3—C4—C14  | 126.2 (4) | C9—C19—H27  | 109.471 |
| C3—C4—Cg1  | 54.5 (2)  | H25—C19—H26 | 109.472 |
| C5—C4—C14  | 125.2 (4) | H25—C19—H27 | 109.472 |
| C5—C4—Cg1  | 54.1 (2)  | H26—C19—H27 | 109.472 |
| C14—C4—Cg1 | 178.2 (3) | C10—C20—H28 | 109.470 |
| SR1—C5—C1  | 74.7 (2)  | C10—C20—H29 | 109.469 |
| SR1—C5—C4  | 74.6 (2)  | C10—C20—H30 | 109.470 |
| SR1—C5—C15 | 120.4 (3) | H28—C20—H29 | 109.473 |
| SR1—C5—Cg1 | 63.6 (1)  | H28—C20—H30 | 109.473 |
| C1—C5—C4   | 107.9 (3) | H29—C20—H30 | 109.473 |
| C1—C5—C15  | 125.4 (4) | N1—C21—H31  | 118.110 |
| C1—C5—Cg1  | 53.9 (2)  | C22—C21—H31 | 118.110 |
| C4—C5—C15  | 126.5 (4) | C21—C22—H32 | 121.146 |
| C4—C5—Cg1  | 54.1 (2)  | C23—C22—H32 | 121.146 |
| C15—C5—Cg1 | 176.0 (3) | C22—C23—H33 | 120.023 |
| SR1—C6—C7  | 76.1 (2)  | C24—C23—H33 | 120.023 |
| SR1—C6—C10 | 74.9 (2)  | C23—C24—H34 | 120.398 |
| SR1—C6—C16 | 117.4 (2) | C25—C24—H34 | 120.399 |
| SR1—C6—Cg2 | 64.8 (1)  | C26—C27—H35 | 120.349 |
| C7—C6—C10  | 108.0 (3) | C28—C27—H35 | 120.348 |
| C7—C6—C16  | 126.4 (3) | C27—C28—H36 | 120.163 |
| C7—C6—Cg2  | 54.1 (2)  | C29—C28—H36 | 120.164 |
| C10—C6—C16 | 125.6 (3) | C28—C29—H37 | 121.225 |
| C10—C6—Cg2 | 53.9 (2)  | C30—C29—H37 | 121.224 |
| C16—C6—Cg2 | 177.7 (3) | N2—C30—H38  | 117.935 |
| SR1—C7—C6  | 75.3 (2)  | C29—C30—H38 | 117.936 |
| SR1—C7—C8  | 75.6 (2)  |             |         |

Symmetry codes: (i)  $-x+2, y-1/2, -z+1/2$ ; (ii)  $x-1/2, -y+1/2, -z$ .

## supplementary materials

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Fig. 1

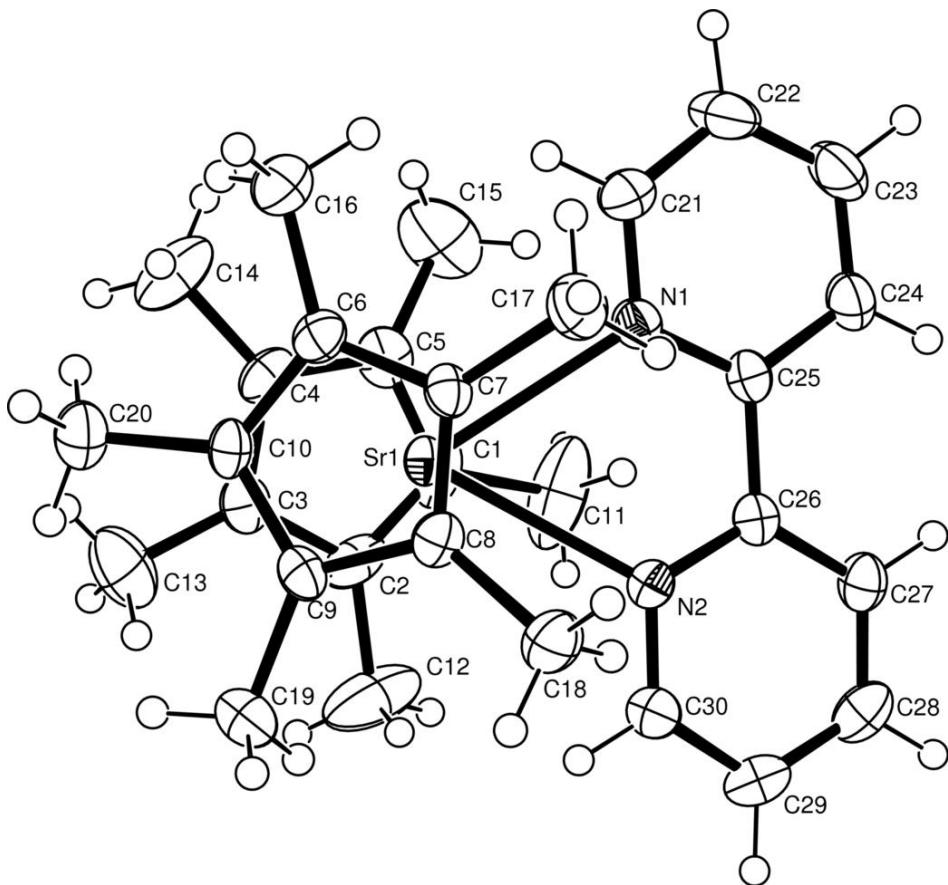


Fig. 2

