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Magnetohydrodynamic nanofuid radiative thermal behavior by means of Darcy law inside a porous media

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Radiative nanomaterial thermal behavior within a permeable closed zone with elliptic hot source is simulated. Darcy law is selected for simulating permeable media in existence of magnetic forces. Contour plots for various buoyancy, Hartmann numbers and radiation parameter were illustrated. Carrier fuid is Al2O3-water with diferent shapes. Outputs prove that conduction mode augments with enhance of *Ha***.** *Nu* **augments with considering radiation source term.**

Transport processes of nanofuid through medium with porosity have been a challenging study in recent times because of its immense applications in geothermal operations, thermal insulations, food processing, and other petrochemical applications. Modeling of nanomaterial fow with imposing Lorentz forces was scrutinized by Yadav et al.^{[1](#page-9-0)} and buoyancy force was involved in governing PDEs. A survey present in the literature has shown that thermal properties of nanofuids are better than the usual fuids. Results available have shown that heating properties of solid is larger than liquid. The thermal conductivity engine oil and $H₂$ O are thousand times lower than that of copper (Cu). Some preliminary experiments on *Cu*−water suspended nanoparticles are performed by Eastman *et al.*^{[2](#page-9-1)}. In the augmentation of heat transmission, Khanafer *et al.*^{[3](#page-9-2)} obtained some interesting results by utilizing nanofluids. The problem studied by Qiang⁴ studied experimentally for copper based water nanofluid and obtained some interesting results. More detail on the investigation of heat transmission with nanofuids can be found in^{[5–](#page-9-4)10}. CuO-water based nanofluid inside absorptive medium in the actuality of magnetic force with Brownian motion is performed by Sheikholeslami¹¹. MHD fluid flow was portrayed by Raju *et al*.¹² over a cone. Kolsi *et al*. [13](#page-9-8) employed moved fn to control nanofuid migration through a channel. Diferent applications of Fe3O4-water nanofuid were categorized by Sheikholeslami and Rokni[14](#page-9-9). Haq *et al*. [15](#page-9-10) utilized carbon nanotubes with slip flow to improve convective heat transfer.

Nanomaterial fow has received considerable attention from many scientists due to its large uses in engineer ing ^{16–18}. Plasma studies and aerodynamics are some practical examples of such flows of radiation mechanism.

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Figure 1. Current porous zone under the impact of magnetic feld and sample element.

Radiation is ofen encountered in frequent engineering problems. Keeping in view its applications Sheikholeslami *et al*. [19](#page-9-13)[–23](#page-9-14) presented the application of nanomaterial in various domains. Some recent publications about heat transfer can be found in $24-32$ $24-32$. To preserve the conduction of about fluid low, nano liquids have been recommended in past ages. Infuence electric feld on ferrofuid inside a tank with dual adaptable surfaces was demonstrated by Sheikholeslami et al.^{[33](#page-9-17)}. The investigation of nanofluid with magnetic forces with physical effects and applica-tions can studied from^{[34](#page-9-18)–[36](#page-9-19)}. Turbulator effect on swirling nanofluid flow was examined by Sheikholeslami *et al.*³⁷. Utilizing such tools make the fow more complex. New model was introduced by Yadav *et al*. [38](#page-9-21) for thermal instability. Furthermore, instability of thermal treatment of nanomaterial within a penetrable zone was exemplifed by Yadav et al.³⁹. They considered variation of nanomaterial viscosity in their simulation. Viscous heating effect on nanomaterial radiative behavior in existence of electric feld was scrutinized by Daniel *et al*. [40](#page-10-0). In addition, they considered double stratifcation with magnetic feld. Nanomaterial free convection with double-difusive was scrutinized by Yadav *et al*. [41](#page-10-1) involving rotation system. Permeable plate with considering radiative impact was modeled by Daniel et al.⁴². They imposed Lorentz forces and utilized HAM to solve the problem. Nanomaterial exergy loss with implementation of innovative approach was established by Sheikholeslami⁴³. He is expert in this feld and shows the approach applications in appearance of magnetic feld. Entropy production during transient nanomaterial MHD flow was demonstrated by Daniel *et al.^{[44](#page-10-4)}*. They derived governing equations with considering electric feld efect. Developments on numerical approach for simulating treatment of nanomaterial were presented in different publications⁴⁵⁻⁵¹.

In current study, efects magnetic force and radiation on migration of nanofuid inside a porous medium was illustrated. CVFEM is considered as tool for showing roles of Rd, Ra, & Ha on performance.

Problem Explanation

The shape of enclosure and its boundary conditions have been demonstrated in Fig. [1](#page-1-0). Furthermore, example element was demonstrated. Uniform *q*″ was imposed on inner wall. Unchanging magnetic feld impact on nanomaterial flow style is surveyed. Porous domain has been full of H_2O based nanofluid.

Governing equations and CVFEM. Free convection and radiation impacts on migration of nanofluid inside a penetrable media were pretend under the efect of Lorentz forces. Considering Darcy model, fnal formulations can be written as:

Nu _{ave}	Mesh
2.923911	51×151
2.927703	61×181
2.931546	71×211
2.934301	81×241
2.938154	91×271

Table 1. Mesh study for case of *Ra*=600, *φ*=0.04 *Rd*=0.8, *Ha*=20.

Figure 2. Verification with Khanafer *et al.*^{[3](#page-9-2)} for ϕ = 0.1, *Gr* = 10⁴ and Pr = 6.2(*Cu* – *Water*).

$$
\frac{\partial P}{\partial x} = -\frac{\mu_{nf}}{K}u + B_0^2 \sigma_{nf} \left[-u(\sin \gamma)^2 + \frac{1}{(\sin \gamma)v(\cos \gamma)} \right]
$$
(1)

$$
\frac{\partial v}{\partial y} + \frac{\partial u}{\partial x} = 0 \tag{2}
$$

$$
\frac{\partial P}{\partial y} = -\frac{\mu_{rf}}{K}v + (T - T_c)g\rho_{rf}\beta_{rf} + B_0^2(\cos\gamma)[(\sin\gamma)u - v(\cos\gamma)]\sigma_{rf}
$$
\n(3)

$$
\left(v\frac{\partial T}{\partial y} + u\frac{\partial T}{\partial x}\right) = -\frac{1}{(\rho C_p)_{nf}} \frac{\partial q_r}{\partial y} + \left(\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2}\right) (\rho C_p)_{nf}^{-1} k_{nf},
$$
\n
$$
\left[T^4 \cong 4T_c^3 T - 3T_c^4, q_r = -\frac{4\sigma_e}{3\beta_R} \frac{\partial T^4}{\partial y}\right]
$$
\n(4)

Characteristics of nanofuid have following formulas:

$$
BB = \phi + (\rho \beta)_f (1 - \phi) / (\rho \beta)_s, BB = (\rho \beta)_{nf} / (\rho \beta)_s
$$

\n
$$
CC = \phi + (1 - \phi) (\rho C_p)_f / (\rho C_p)_s, CC = (\rho C_p)_{nf} / (\rho C_p)_s
$$

\n
$$
\rho_{nf} = \rho_s \phi + \rho_f (1 - \phi),
$$

\n
$$
\chi - 1 = \frac{3(A - 1)\phi}{(2 + A) + \phi(1 - A)}, A = \sigma_s / \sigma_f, \chi = \frac{\sigma_{nf}}{\sigma_f}
$$
 (5)

 μ_{nf} & k_{nf} are represented the Brownian motion forces functions and function of shape factor as mentioned in⁵²:

	Ha	
Shape	20	$\bf{0}$
Cylinder	2.887839	5.886044
Platelet	2.931546	5.9168
Spherical	2.800245	5.826297
Brick	2.834335	5.849228

Table 2. Impact of "*m*" on Nu_{ave} when $Ra = 600$, $\phi = 0.04$ $Rd = 0.8$.

streamlines

isotherms

Figure 3. Various of flow style with changing ϕ when $Ra = 600$, $Rd = 0.8$.

Figure 4. Outputs for various Ha at $Ra = 100$, $Rd = 0.8$.

$$
\mu_{hf} = \frac{k_{Brownian}}{Pr_f} \times \frac{\mu_f}{k_f} + \mu_f [1 - \phi]^{-2.5}, TT = Ln(T)
$$
\n
$$
k_{Brownian} = 10^4 \times g'(d_p, \phi, T) \times 5\rho_f \phi \sqrt{\frac{\kappa_b T}{\rho_p d_p}} c_{p,f}
$$
\n
$$
g'(d_p, \phi, T) = \left(a_7Ln(d_p) + a_9Ln(d_p)Ln(\phi) + a_8Ln(\phi) + a_{10}Ln(d_p)^2 + a_6\right)
$$
\n
$$
+ TT \begin{pmatrix} a_5Ln(d_p)^2 + a_3Ln(\phi) \\ + a_2Ln(d_p) + a_1 \\ + a_4Ln(d_p)Ln(\phi) \end{pmatrix}
$$
\n(6)

SCIENTIFIC REPORTS | *(2019) 9:12765* | https://d[oi.org/10.1038/s41598-019-49269-9](https://doi.org/10.1038/s41598-019-49269-9) 5 5 5 5 7 7 8 7 9 7 7 8 7 7 8 7 9 7 7 9 7 7 8 7 7 8 7 9 7 7 8 7 7 8 7 7 8 7 7 8 7 7 8 7 7 8 7 7 8 7 7 8 7 7 8 7 7 8 7 7 8 7 7 8 7 7 8 7 7

Figure 5. Outputs for various Ha at $Ra = 200$, $Rd = 0.8$.

$$
\kappa = (k_f - k_p),
$$

\n
$$
A_4 = \frac{k_f - m\kappa\phi + k_p - \phi\kappa + mk_f}{mk_f + k_p + \phi\kappa + k_f +},
$$
\n(7)

To get the properties of carrier fluid, we utilized alike model used in⁵². To estimate temperature dependent properties, Rokni *et al*. [53](#page-10-8),[54](#page-10-9) provide new formulation.

The following non dimensional variables by using of the stream function and, can be gained:

$$
v = -\frac{\partial \psi}{\partial x}, \Delta T = Lq''/k_f,
$$

(Y, X) = (yL⁻¹, xL⁻¹),

$$
\Psi = \psi/\alpha_{nf}, \theta = \frac{T - T_c}{\Delta T},
$$

$$
u = \frac{\partial \psi}{\partial y},
$$
 (8)

Thus, the last equations are:

Figure 6. Outputs for various *Ha* at $Ra = 600$, $Rd = 0.8$.

$$
\frac{\partial^2 \Psi}{\partial Y^2} + \frac{\partial^2 \Psi}{\partial X^2} = -Ha \frac{A_6}{A_5} \left[\frac{2(\sin \gamma) \Psi_{XY}(\cos \gamma) +}{(\cos^2 \gamma) \Psi_{XX} + \Psi_{YY}(\sin^2 \gamma)} \right] - \frac{A_3 A_2}{A_4 A_5} \frac{\partial \theta}{\partial X} Ra
$$
\n(9)

$$
\left(\frac{\partial^2 \theta}{\partial X^2}\right) + \left(1 + \frac{4}{3} \left(\frac{k_{nf}}{k_f}\right)^{-1} Rd\right) \frac{\partial^2 \theta}{\partial Y^2} = \frac{\partial \theta}{\partial X} \frac{\partial \Psi}{\partial Y} - \frac{\partial \Psi}{\partial X} \frac{\partial \theta}{\partial Y}
$$
(10)

Important variables can be introduced as:

$$
Rd = 4\sigma_e T_c^3 / (\beta_R k_f), A_5 = \frac{\mu_{hf}}{\mu_f},
$$

\n
$$
Ra = \frac{L(\rho \beta)_f Kg \Delta T}{\alpha_f \mu_f},
$$

\n
$$
A_3 = \frac{(\rho \beta)_{nf}}{(\rho \beta)_f}, \quad A_2 = \frac{(\rho C_p)_{nf}}{(\rho C_p)_f}, \quad A_6 = \frac{\sigma_{nf}}{\sigma_f},
$$

\n
$$
A_1 = \frac{\rho_{nf}}{\rho_f}, \quad A_4 = \frac{k_{nf}}{k_f},
$$

\n
$$
Ha = K \frac{\sigma_f B_0^2}{\mu_f},
$$

\n(11)

Inner and outer surfaces have following conditions:

$$
\theta = 0 \text{ exterior surfaces}
$$

\n
$$
\frac{\partial \theta}{\partial n} = 1 \text{ internal surface}
$$

\n
$$
\Psi = 0 \text{ over inner and outer walls}
$$
 (12)

Nu_{ave} and *Nu_{loc}* have been calculated as:

$$
Nu_{ave} = \frac{1}{S} \int_0^s Nu_{loc} ds
$$
\n(13)

$$
Nu_{loc} = \left(\frac{k_{nf}}{k_f}\right) \frac{1}{\theta} \left(1 + \frac{4}{3}Rd\left(\frac{k_{nf}}{k_f}\right)^{-1}\right) \tag{14}
$$

Simulation technique, grid and verifcation. Combine of two infuential approaches has been assem-bled in CVFEM. As explained in ref.³³ and shown in Fig. [1\(b\),](#page-1-0) such grid is applied in CVFEM. Final equations have attainment to values of *θ*, Ψ by using of Gauss-Seidel technique. Table [1](#page-2-0) exhibits the sample for grid management. This procedure should be done because last result should be immaterial of grid size. Verifications of current code for nanofluid convective flow are displayed in Fig. $2³$ $2³$ $2³$ $2³$. These observations show nice accuracy of CVFEM code.

Outcome and Discussion

Radiative nanofuid heat transmission through a penetrable enclosure by means of Darcy law was displayed. Efects of Brownian motion and shape factor on nanomaterial behavior were examined. CVFEM was applied to display the variations of Rayleigh number (*R a* = 100 to 600), radiation (*Rd* = 0 \rightarrow 0.08), Concentration of Alumina (ϕ = 0 to 0.04) and magnetic forces (*Ha* = 0 to 20). Deviations of Nu respect to *m* are represented in Table [2.](#page-3-0) Higher value of Nu is described for Platelet shape. Tus, it is designated for more simulations. Role of scattering Al₂O₃ in H₂O have exemplified in Fig. [3.](#page-3-1) It is observed that $|\psi_{\text{max}}|$ and Nu enhances by diffusing Al₂O₃. Since Lorentz force acting, the impact of *φ* on isotherms is not important. Impacts of substantial parameters on isotherms and streamlines are displayed in Figs [4,](#page-4-0) [5](#page-5-0) and [6.](#page-6-0) $|\psi_{\rm max}|$ rises with increase of buoyancy effect while it diminishes with escalation of *Ha*. Simulations for higher Ra leads to complex shape of isotherm with imposing greater buoyancy forces and thermal plume appears. Imposing Lorentz forces make suppress the plume and isotherms force to being parallel to each other's. For better description, below formula was derived and Fig. [7](#page-8-0) was displayed.

$$
Nu_{ave} = 3.05 + 0.85Rd + 0.49Ra - 0.7Ha + 0.14Rd Ra - 0.18Rd Ha
$$

-0.47RaHa - 0.1Ra² (15)

Greater values of radiation parameter and Ra lead to thinner boundary layer which indicates greater *Nuave*. Slender thickness of boundary layer was seen with reduce of Hartmann number which proves reduction efect of Hartmann number on Nu_{ave} .

Conclusions

Imposing Lorenz forces infuence on nanomaterial fow by means of Darcy law inside a porous enclosure is reported. Shape factor role was involved to predict nanomaterial properties as well as Brownian motion. CVFEM modeling was done to fnd the variations of Lorentz and buoyancy forces and radiation parameter on nanofuid thermal characteristic were demonstrated. The concluded points are given as

Figure 7. Changes in *Nuave* for various *Rd*, *Ra*, *Ha*.

- • Outputs depict that *Nu* improves with improve of buoyancy force but it decrease with augment of *Ha*.
- Higher value of Nu is described for Platelet shape.
- Nu augments with considering radiation source term.
- • As *Ha* enhances, the velocity of working fuid decreases.

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Author Contributions

M.S. and Z.S. modeled and solved the problem. Z.S. and T.T.N. wrote the manuscript. P.K. contributed in the numerical compuattuions and plotting the graphical results. T.T.N. and A.S. edited the manuscript grammatically and thoroughly checked the mathematical modeling and English corrections. All the corresponding authors finalized the manuscript after its internal evaluation.

Additional Information

Competing Interests: The authors declare no competing interests.

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