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Multiple leading edge vortices of unexpected strength in freely flying hawkmoth

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L. Christoffer Johansson, Sophia Engel, Almut Kelber, Marco Klein Heerenbrink & Anders Hedenström

Department of Biology, Lund University, Ecology building, SE-223 62 Lund, Sweden.

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Correspondence and requests for materials should be addressed to L.C.J. (Christoffer.Johansson@biol.lu.se)

The Leading Edge Vortex (LEV) is a universal mechanism enhancing lift in flying organisms. LEVs, generally illustrated as a single vortex attached to the wing throughout the downstroke, have not been studied quantitatively in freely flying insects. Previous findings are either qualitative or from flappers and tethered insects. We measure the flow above the wing of freely flying hawkmoths and find multiple simultaneous LEVs of varying strength and structure along the wingspan. At the inner wing there is a single, attached LEV, while at mid wing there are multiple LEVs, and towards the wingtip flow separates. At mid wing the LEV circulation is ~40% higher than in the wake, implying that the circulation unrelated to the LEV may reduce lift. The strong and complex LEV suggests relatively high flight power in hawkmoths. The variable LEV structure may result in variable force production, influencing flight control in the animals.

Insect flight has long been considered a paradox, defeating the expectations of steady state aerodynamics. We now know that the main lift enhancing mechanism that enables insects to generate enough lift to stay airborne is the Leading Edge Vortex, LEV^{1–6}, which are also found in plant seeds⁷, birds^{8,9} and bats¹⁰. The LEV is generated by separation of the flow at the leading edge of the wing and enables the flow to reattach before the trailing edge. In flapping flight a single core LEV is generally found to stay attached to the top surface of the wing throughout the downstroke (e.g. ref. 11), although recent flapper studies and computational fluid dynamic (CFD) models have implicated a higher complexity with multiple cored vortices^{12–16}. Earlier studies have sometimes described a transient LEV structure with the formation of a second LEV during the shedding of the first LEV^{16,17}. However, this is different from the more recent studies, which indicate a multi-cored LEV that stays attached to the wing throughout the wingbeat^{12,13,15}. The multi-cored LEV structure is proposed to be a potentially general feature of insect flight when a combination of flow conditions are met (see below), although the exact circumstances are still debated^{13,15}. Although proposed as a general feature of insect flight, a multi-cored LEV has until now only been shown in accelerating butterflies¹⁸ and is yet to be demonstrated in steadily flying insects.

LEVs in insect flight have mainly been studied using flappers mimicking hawkmoths^{1,19,20} and other insects^{2,12–14,16,17,20}, and more recently CFD models have also been used to study vortex dynamics (e.g. refs. 21–23 regarding hawkmoths). LEVs have also been demonstrated in live insects using smoke visualizations^{3,5,18,20} or Particle Image Velocimetry (PIV)⁴. Although some of the previous studies are based on freely flying animals^{3,5,18}, a majority are based on tethered animals^{1,4,19–23} or in the case of flapper and CFD studies on simplified kinematics^{2,12,13,15}. Tethering may affect the deformability of the thorax, which is responsible for the wing motion in insects such as moths²⁴, or give exaggerated responses because the sensory feedback loop is disrupted²⁵, and it is yet to be shown that tethering generates results similar to free flight (but see³). Furthermore, the body and its motions are generally ignored or difficult to simulate in flappers and computational models (but see²⁶), as are wing mechanical properties, resulting in unrealistic aeroelastic interactions²³. To the best of our knowledge, no data exist from live, freely flying, insects that quantify the flow structure of the LEV, to be used as a baseline for comparing the results from tethered animals, mechanical flappers and CFD-models. Here we perform detailed, high-resolution PIV, measurements of the flow above the wing of hummingbird hawkmoths (*Macroglossum stellatarum*) flying steadily in front of small feeders in a wind tunnel, at flight speeds (U_∞) of 1 and 2 m/s to quantify the strength and structure of the LEV.

Results

We find that the LEV structure is complex, with multiple vortices present simultaneously. The structure of the LEVs vary along the wingspan. On the inner wing there is generally a single, attached, LEV (Fig. 1a,

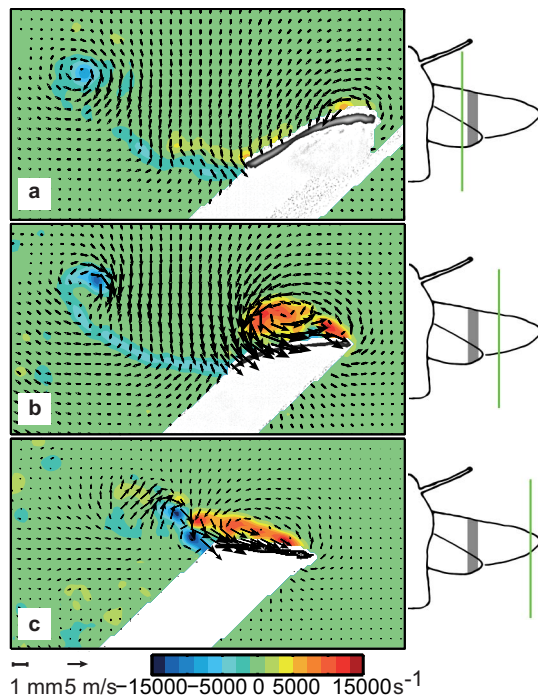


Figure 1 | Velocity fields (U_∞ subtracted), showing every third vector, and vorticity field, around the inner (a) (Moth 9), mid (b) (Moth 2) and distal (c) (Moth 2) part of a wing of a *M. stellatarum* flying at 2 m/s. Flight direction is to the right. a and b are at mid downstroke, and c at beginning of downstroke. Velocity is scaled according to the reference vector and vorticity according to the colorbar below the graphs. The velocity and vorticity fields are superimposed on the original images showing the wing profile as a gray area in the masked region (white). Cartoons to the right show the position of the laser along the span. The gray area shows the region where the structure and strength of the LEV changes along the wing length.

Supplementary Figs. S4–5, Supplementary Table S2–3), at mid wing there are multiple LEVs (Fig. 1b, Fig. 2, Fig. 3, Supplementary Table S2–3). At the distal part of the wing the flow is fully separated (Fig. 1c), most likely representing a cut through the wing tip vortex, rolling up on the wing. At mid-wing multiple LEVs are clearly visible when constructing the streamlines of the flow above the wing and using swirl strength to identify separate vortex structures (Fig. 2).

In order to better understand the flow conditions governing the LEV stability we determine a number of relevant parameters. During the downstroke the mean angle of attack (α), the angle between the wing chord line and the oncoming airflow, is higher at the lower speed $41.6 \pm 2.6^\circ$, mean \pm S.E.M., ($U_\infty = 1$ m/s) than at the higher speed, $32.2 \pm 2.4^\circ$ ($U_\infty = 2$ m/s). Amplitude normalized by mean chord²⁷, \bar{c} , is 0.68 ± 0.03 at $U_\infty = 1$ m/s and 0.81 ± 0.03 at $U_\infty = 2$ m/s and wavelength normalized by \bar{c} ²⁷ is 1.6 ± 0.04 at $U_\infty = 1$ m/s and 3.3 ± 0.12 at $U_\infty = 2$ m/s. Reynolds number¹⁰ (Re), a measure of the ratio of inertial and viscous forces, based on mean speed at mid-wing during the downstroke and \bar{c} is $1.0 \cdot 10^3$ ($U_\infty = 1$ m/s) and $1.4 \cdot 10^3$ ($U_\infty = 2$ m/s). The Reynolds number based on the wing tip velocity during mid downstroke and wing length (Re_s)¹⁵ is $5.7 \cdot 10^3$ ($U_\infty = 1$ m/s) and $6.3 \cdot 10^3$ ($U_\infty = 2$ m/s). The downstroke Strouhal number, St_{db} , an index related to flow unsteadiness, calculated on the basis of the wing tip motion²⁸ is 0.315 ± 0.018 at $U_\infty = 1$ m/s and 0.316 ± 0.012 at $U_\infty = 2$ m/s. Rossby number, Ro , a measure of the rotational acceleration initiating spanwise flow that mediate the growth of the LEV in flapping wings¹⁴, based on downstroke wingtip motion⁸, is 4.26 ± 0.17 at $U_\infty = 1$ m/s and 4.21 ± 0.12 at $U_\infty = 2$ m/s.

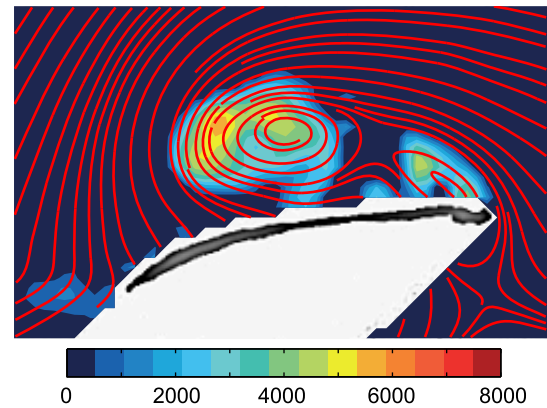


Figure 2 | A zoomed in view of Fig. 1b showing the streamlines on top of the swirling strength (a measure of rotation) color-coded according to the colorbar below. Free-stream flow not subtracted. The swirling strength indicates two distinct LEVs separated by areas of zero swirl.

In addition to determining the geometry of the vortex structure and the wing beat kinematics, we calculate the circulation (Γ) of the LEV (Γ_{LEV}) and the circulation in the wake (Γ_{TEV}) by integrating the vorticity above and behind the wing, respectively^{8,10}. The Γ_{LEV} , normalized by the local speed and chord, Γ_{LEV}^* , which is equal to half the local force coefficient, increases from inner to middle wing (Fig. 4), with a distinct increase at 33–47% of the wing length (Supplementary Fig. S6). The relative contribution of the LEV to lift production is determined by comparison with the circulation in the wake^{8,10}. The Γ_{TEV}^* is more constant along the wing than the Γ_{LEV}^* . The LEV is stronger than the TEV at mid-wing, where Γ_{LEV} is $132 \pm 13\%$ of the Γ_{TEV} at $U_\infty = 1$ m/s during mid downstroke, and $145 \pm 10\%$ at $U_\infty = 2$ m/s (Fig. 4). However, at the inner wing the LEV is weaker than the TEV during mid downstroke ($39 \pm 4\%$ at $U_\infty = 1$ m/s and $38 \pm 16\%$ at $U_\infty = 2$ m/s), suggesting that the LEV contributes $\sim 40\%$ of the lift generated at the inner wing (Fig. 4). The transition zone shows intermediate values in Γ_{LEV}^* and $\Gamma_{LEV}/\Gamma_{TEV}$ with a relatively high variation (Supplementary Fig. 6).

Discussion

A double LEV structure, similar to the one found here, has also been described in delta wings (e.g. ref. 29), in recent flapper studies (e.g. refs. 12, 13), CFD models¹⁵ and in free-flying butterflies during accelerated flight¹⁸ (suggesting large forces). In addition, secondary vortex structures, considered shear layer instabilities, have been described as a rare phenomenon in both tethered and freely flying dragonflies³. Contrary to the results in butterflies, our results show that multiple, simultaneous, LEVs are the normal feature during steady flight in our freely flying hawkmoths, which is consistent with the recent flapper studies^{12,13} and CFD models¹⁵ that suggest the complex LEV to be a general feature of insect flight. Not only does the flow show multiple LEVs, but the flow structure also varies between measurements (Fig. 3, Supplementary Figs. S1–3), which to some degree is explained by kinematic variation. However, the variation is partly also due to spanwise variation in LEV stability^{14,15}. Factors influencing the stability of LEVs in flapping flight is currently an active field of research^{2,8,12–15,23}, and a few diagnostic measures for LEV stability have been identified. The combination of Re and α used by the hawkmoths are above the critical values ($\alpha > 30^\circ$ and $Re > 640$) associated with the formation of multiple LEVs in a flapper¹³ and suggest the LEV may burst^{14,15}. A bursting LEV is turbulent, but force augmentation is maintained. This agrees with our observed variation in the LEV structure and associated high force coefficient of the LEV at mid wing (Fig. 4). However, although the LEV may burst, it does not necessarily shed prematurely from the wing^{14,15}. In fact, the downstroke Strouhal number, St_{db} , is within the range associated with

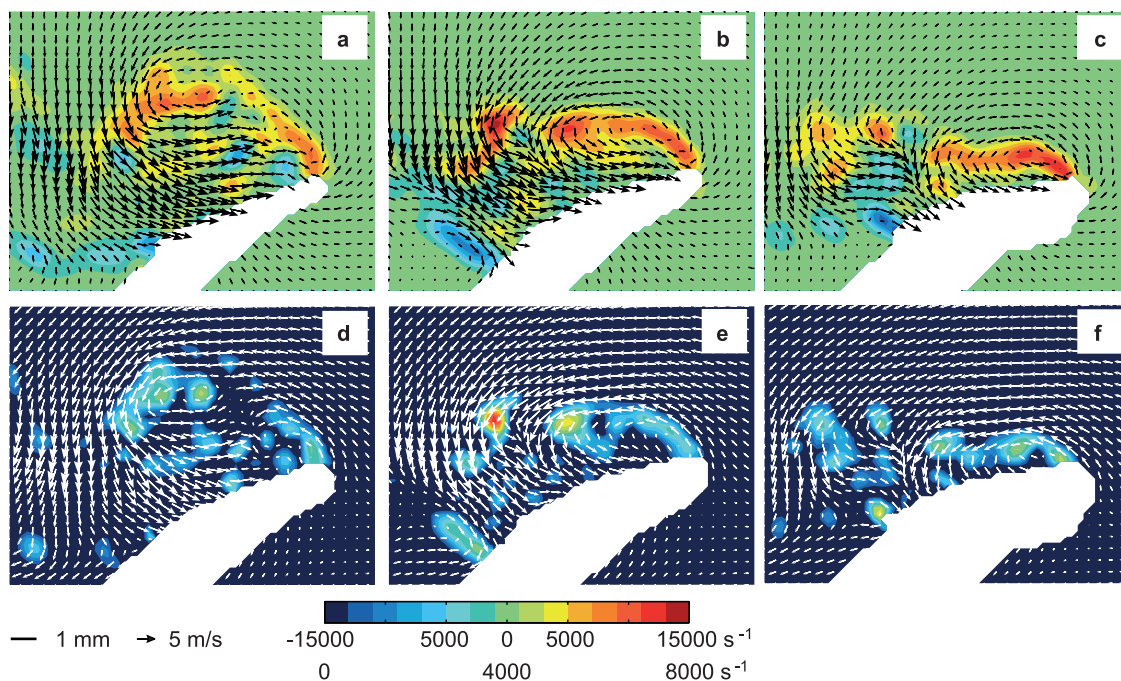


Figure 3 | Velocity and vorticity plots of the LEV structure at mid wing at mid downstroke at three additional wingbeats from the same flight sequence as Fig. 1b of Moth 2 showing the diversity of the flow structure. (a–c) show every second vector (free stream subtracted), scaled according to the vector below, on top of the vorticity, scaled according to the upper scale of the colorbar below the figure. (d–f) show the velocity, including the free stream flow, on top of the swirl strength scaled according to the lower scale of the colorbar below (zero swirl). Data from additional individuals and from further inwards on the wing are available in the Supplementary Figs. S1–S6.

optimal vortex shedding^{30,31}, i.e. vortices are shed at the start and end of the downstroke. The Ro is relatively high, indicating a potentially unstable LEV, but local Ro is lower towards the base of the wing, predicting a stable LEV-structure there. This is in general agreement with our findings. Although the on-wing LEV may indicate detachment from the wing surface during the downstroke (Fig. 3, Supplementary Figs. S1–3), images showing the entire wake of the downstroke do not display any clear signs of a shed LEV. This suggests that the LEVs contribute to the lift production until the end of

the downstroke. Alternatively, the variation in the LEV structure may be caused by a chaotic interaction with the wake of the previous wingbeat as suggested by the combination of normalized amplitude and normalized wavelength²⁷. However, if taking into account an inclined stroke plane, the wave length of the outer wing should be relatively higher than for the inner wing during the downstroke, reducing the relative risk of interactions at the outer wing. This is opposite to the higher variation at the outer wing than at the inner wing that we find here. The spanwise transition between the single LEV on the inner wing and the more complex structure at mid wing occurs at approximately a relative position 0.35–0.4 of the wing length from the root. This is close to the transition (~ 0.45) predicted by the Re_s of approximately 6×10^3 found here¹⁵. Although the prediction applies to hovering flight¹⁵ the close agreement with our results for forward flight calls for further studies of the factors determining LEV transition. Worth noting is that the transition point seems to coincide with the position of the wing tip of the hindwing. This may suggest a possible active control mechanism for the inner wing by the hind wing. Regardless of the cause of the variation in LEV structure the varying position of the LEV along the chord affects the pressure distribution⁶ and thus the pitching moments controlling wing twist and consequently the local angle of attack. These factors combine to a complex system affecting force generation that may influence flight control.

The increase in Γ_{LEV}^* is associated with the transition from a single to multiple LEVs, suggesting that the increased LEV complexity results in an increased local force coefficient of the LEV. The $\Gamma_{LEV}/\Gamma_{TEV}$ above unity at the mid wing, where most of the lift is generated, suggests that the LEV is solely responsible for the lift generation at this part of the wing. In fact, the $\Gamma_{LEV}/\Gamma_{TEV}$ significantly above unity suggests that the LEV not only complements the bound circulation, Γ_B , but instead requires the bound circulation to reverse at mid wing, because according to Kelvin's circulation theorem, the net change in circulation in a closed system is zero³². This means that the circulation moving with the wing ($\Gamma_B + \Gamma_{LEV}$) should

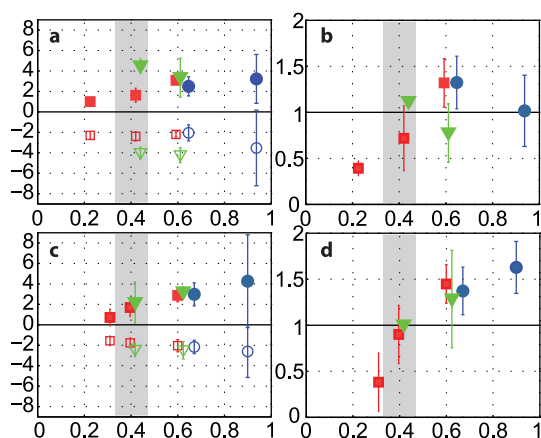


Figure 4 | Circulation normalized by the local speed and chord of the LEV (closed) and TEV (open) along the length of the wing (0 at base, 1 at tip) at 1 m/s (a) and 2 m/s (c) flight speed. $\Gamma_{LEV}/\Gamma_{TEV}$ along the length of the wing at 1 m/s (b) and 2 m/s (d) flight speed. A ratio above one suggests that the LEV is stronger than the circulation found in the wake. The gray area indicates the location along the wing where we find an increase in Γ_{LEV} and $\Gamma_{LEV}/\Gamma_{TEV}$. Values are means ± 2 *SEM. Colors are beginning of downstroke (blue), mid downstroke (red) and end of downstroke (green).



be equal, but of opposite spin, to the circulation shed into the wake (Γ_{TEV}). Since the decay of circulation is negligible within the time frame of a downstroke³³, the bound circulation of the wing (Γ_B), which we cannot estimate directly, is required to be of opposite spin to Γ_{LEV} . Our results thus show that the LEV is the main lift-generating mechanism in freely flying hummingbird hawkmoths, and that the LEV is stronger than expected since a weaker LEV, where $\Gamma_B \geq 0$, may produce the same lift while adding less kinetic energy to the air.

Hovering specialist vertebrates, i.e. hummingbirds⁹, flycatchers⁸ and bats¹⁰, also use LEVs at low flight speeds. However, the LEVs in these animals have not displayed the complexity found here and the LEVs are closer to the wing surface despite the higher Re of bird and bat flight. Flexibility of the wings may stabilize the LEV^{8,23}, and one explanation for the differences between insects and vertebrates may be a difference in mechanical properties of the wings^{34,35}. Alternatively, the ability of active control of the wing during a wing-beat, in response to sensory information³⁶, may be more likely to occur in vertebrates as a consequence of lower wingbeat frequency and ability to morph the wings. Our results thus indicate differences in flow control related to phylogenetic history, with the potential to impose limitations to animal flight performance.

Methods

Six moths (*Macroglossum stellatarum*), Table S1, were flying freely in front of a feeder at speeds (U_∞) 1 and 2 m/s in a wind tunnel.

2D velocity fields were determined using PIV in a vertical plane, $37 \times 37 \text{ mm}^2$ parallel to U_∞ [x, z] around the wing. Images of fog particles ($\sim 1 \text{ }\mu\text{m}$) were captured in the plane illuminated by a laser (Litron LPY732 series, 532 nm, 200 Hz). Images were captured (HighSpeedStar3; 1024×1024 pixels, Zeiss Makro-Planar T, 100 mm, filter $532 \pm 5 \text{ nm}$) and analyzed using Davis 7.4 (LaVision, Germany) after calibration (plate type 22, and “self-calibration”). 127 frames were analysed (box size 12×12 , 50% overlap) after masking the wing and shadow. After removing erroneous vectors, vector fields were smoothed once (3×3 box size).

Two synchronized cameras (500 Hz) filmed side- and top views for 3D kinematics²⁸. Nine sequences (3–5 wing beats), all individuals contributed at least one sequence, at each speed were analysed. Mean speed at mid wing during the downstroke (U_{dm}), wing beat frequency ($f = 82.4 \pm 1.3 \text{ Hz}$ [mean \pm S.E.M.] at $U_\infty = 1 \text{ m/s}$ and $79.7 \pm 2.2 \text{ Hz}$ at $U_\infty = 2 \text{ m/s}$), and amplitude ($\theta = 72.3 \pm 4.1^\circ$ at $U_\infty = 1 \text{ m/s}$ and $70.8 \pm 5.4^\circ$ at $U_\infty = 2 \text{ m/s}$), were determined.

The presences of multiple LEVs were confirmed by patches of positive swirling strength³⁷ separated by zero swirl. Circulation (Γ) was determined for the LEV and for the vortices shed into the wake at the trailing edge, including the start vortex (TEV), by integrating spanwise vorticity (ω_y) within an area of interest. The position of vector fields were determined from the laser position along the wing length, grouped into four groups (0–33%, 34–47%, 48–80% and 81–100%) and given a time stamp as beginning of downstroke (bd), mid downstroke (md) and end of downstroke (ed).

We estimated the wing speed (U_{eff}) along the wing length during each phase (bd, md, ed) by fitting a sine function with a period of 2*downstroke ratio to the wing speed during a normalized downstroke. The downstroke was subdivided into three equal periods and the mean speed of each period was calculated by integrating the sine function over the period and divide by the normalized time of the period. The chord distribution along the wing was measured from photos of the animals. For each combination of individual and phase we then calculated Uc for each measurement, based on the spanwise location, which was used to normalize the circulation. The normalized circulation is half the lift coefficient $C_L = 2\Gamma/Uc$. We estimated means and SEM of the normalized circulation ($\Gamma^* = \Gamma/Uc$) and $\Gamma_{LEV}/\Gamma_{TEV}$ as the intercept (equal to the mean of the individual means) and SEM in a mixed model in JMP (SAS Institute) with individual as a random variable.

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Author contributions

Experiments were planned and conducted by L.C.J., S.E., A.H. and A.K. Analysis was performed by L.C.J. and S.E. Interpretation of the results were done by L.C.J., M.K.H. and A.H. All authors contributed to the writing of the paper.

Additional information

Supplementary information accompanies this paper at <http://www.nature.com/scientificreports>

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